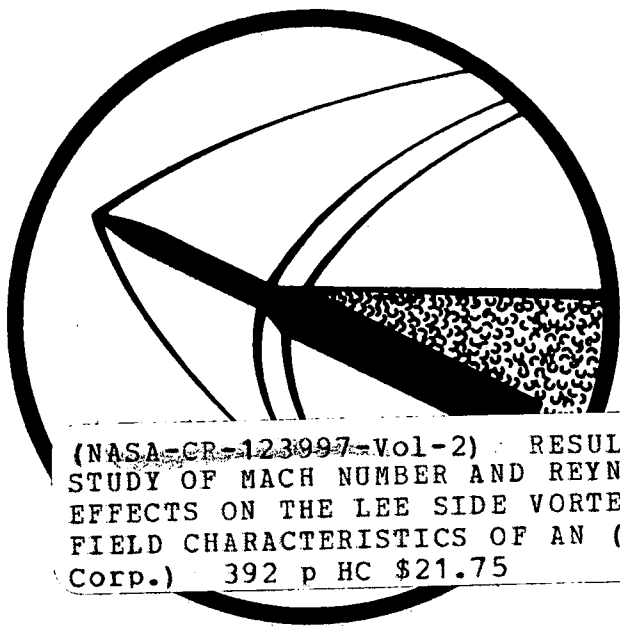


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(NASA-CR-123097-Vol-2) RESULTS OF A
STUDY OF MACH NUMBER AND REYNOLDS NUMBER
EFFECTS ON THE LEE SIDE VORTEX FLOW
FIELD CHARACTERISTICS OF AN (Chrysler
Corp.) 392 p HC \$21.75

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Volume II - APPENDIX

RESULTS OF A STUDY OF MACH NUMBER AND REYNOLDS NUMBER EFFECTS ON THE LEE SIDE VORTEX FLOW FIELD CHARACTERISTICS OF AN OGIVE-CYLINDER-FRUSTUM-CYLINDER AT ANGLES OF ATTACK TO 25 DEGREES

by J. E. Foley

NASA Contract NAS8-24391

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SPACE DIVISION



CHRYSLER
CORPORATION

410R



APPENDIX

Description

This appendix contains a complete listing of the data reduction computer program output for the TWT 535 test data. Each page lists a computed local flow property for the r/D , θ flow field location array at a specific body station and freestream condition. Local flow properties presented are; local Mach number (M); local angle of attack (α); local crossflow direction (θ_{vc}); local pressure coefficient (C_p); local total pressure ratio ($P_t/P_{t\infty}$); local velocity components (V_x , V_r , V_θ); crossflow velocity ratio ($V_c/V_\infty \sin \alpha_\infty$); local vorticity ($\omega D/4V_\infty$); and local circulation strength ($\Gamma/\pi D V_\infty$). The local vorticity and circulation strength values are those defined for each cell by the four adjacent flow survey points, and the r/D , θ values listed correspond to the midpoints of the cells. Also shown on the listing with the local circulation strengths are the sums of the local circulation strengths in the radial and circumferential directions; i.e. with $\Gamma_{i,j}$ the circulation strength of a cell at r_i , θ_j ,

$$R_{SUMj} = \sum_{r_i = r_{min}}^{r_i = r_{max}} (\Gamma_{i,j}/\pi D V_\infty)_{\theta = \theta_j}$$

$$\text{and } T_{HSUMi} = \sum_{\theta_j = \theta = 90^\circ}^{\theta_j = \theta = 180^\circ} (\Gamma_{i,j}/\pi D V_\infty)_{r = r_i}$$

These sums are shown in the bottom row and right hand columns respectively of each listing with the sum in the lower right hand corner as the total circulation strength summed over all cells.



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<u>SECTION</u>	<u>CONDITIONS</u>	<u>PAGE</u>
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<u>SECTION</u>	<u>CONDITIONS</u>	<u>PAGE</u>
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	Crossflow Direction, θ_{VC} (THETA VC)	VI-11
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<u>SECTION</u>	<u>CONDITIONS</u>	<u>PAGE</u>
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	Local Mach Number, M (M)	VII-1
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	Local Pressure Coefficient, C_p (CP)	VII-16
	Local Total Pressure Ratio, $P_t/P_{t\infty}$ (PT/PTINF)	VII-21
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	Local Mach Number, M (M)	VIII-1
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SECTION I

$M_{\infty}=0.8$, $\alpha=20.1^{\circ}$, $Re=4.4 \times 10^6 \text{ ft}^{-1}$,

$X/D = 3.5, 4.1, 4.8, 6.5$

LOCAL FLOW FIELD DATA

MACH = .798 RE = 4.37x10⁺⁶ FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 123 0	.801	.809	.816	.813	.822	.815	.718	.580	.541	.643	.791	.804	.797
.395 127 1	.822	.839	.818	.732	.703	.736	.734	.719	.777	.777	.778	.776	.772
.438 123 0	.806	.817	.776	.697	.763	.794	.804	.810	.800	.790	.784	.779	.777
.495 127 1	.776	.785	.782	.780	.764	.804	.813	.802	.796	.793	.792	.792	.789
.566 151 0	.754	.753	.770	.796	.796	.785	.777	.782	.783	.780	.780	.781	.777
.703 153 0	.753	.755	.759	.764	.771	.776	.776	.777	.780	.779	.778	.777	.773
.839 167 0	.764	.759	.757	.762	.769	.769	.767	.774	.779	.779	.778	.776	.776
.966 169 0	.786	.786	.776	.771	.774	.772	.773	.779	.785	.786	.786	.786	.784
1.047 169 0	.770	.776	.773	.775	.781	.785	.786	.783	.780	.777	.774	.773	.771
1.170 167 0	.773	.782	.777	.778	.781	.784	.786	.785	.783	.779	.776	.775	.774
1.297 153 0	.784	.789	.788	.786	.788	.790	.791	.791	.788	.785	.784	.784	.780
1.439 151 0	.784	.786	.785	.785	.786	.788	.787	.784	.781	.777	.774	.771	.769

LOCAL FLOW FIELD DATA

*6 -1

MACH = .797 RE = 4.36x10 FT ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 143 0	.708	.730	.760	.778	.760	.696	.581	.557	.655	.716	.715	.712	.703
.438 139 0	.770	.769	.769	.782	.819	.800	.687	.716	.769	.767	.759	.746	.735
.495 143 0	.837	.803	.705	.706	.796	.750	.771	.810	.803	.796	.790	.785	.774
.566 149 0	.825	.812	.777	.790	.808	.805	.816	.814	.798	.785	.774	.761	.748
.703 155 0	.790	.799	.802	.822	.836	.832	.821	.810	.802	.798	.789	.778	.765
.839 165 0	.809	.802	.803	.808	.813	.814	.811	.806	.799	.800	.796	.787	.778
.966 171 0	.833	.832	.829	.825	.827	.829	.824	.813	.813	.814	.809	.802	.794
1.047 171 0	.814	.814	.815	.819	.824	.822	.818	.814	.807	.801	.794	.785	.777
1.170 165 0	.813	.814	.814	.815	.819	.821	.820	.816	.810	.802	.796	.788	.782
1.297 155 0	.807	.813	.809	.812	.813	.816	.815	.811	.806	.801	.793	.787	.785
1.439 149 0	.815	.812	.812	.813	.813	.814	.813	.810	.805	.800	.793	.787	.783

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.41x10 FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 147 0	1.321	1.333	.908	.524	.293	.467	.709	.592	.557	1.033	1.394	1.348	1.234
.641 205 0	1.195	1.160	1.210	1.172	.905	1.120	1.170	1.189	1.236	1.199	1.154	1.130	1.116
.703 157 1	1.125	1.068	1.011	1.101	1.219	.961	.977	1.078	1.079	1.073	1.067	1.063	1.046
.839 163 0	1.018	1.014	1.033	1.041	1.014	1.023	1.021	1.015	1.008	1.007	1.006	1.003	1.001
.966 173 0	.921	.925	.965	.949	.928	.911	.879	.918	.940	.938	.939	.944	.937
1.047 173 0	.864	.882	.901	.904	.907	.907	.901	.890	.885	.881	.876	.876	.874
1.170 163 0	.858	.855	.862	.866	.868	.872	.869	.867	.866	.861	.855	.856	.855
1.297 157 1	.842	.842	.846	.848	.849	.852	.855	.851	.850	.848	.843	.841	.842
1.439 147 0	.824	.831	.829	.834	.835	.833	.834	.834	.835	.832	.826	.823	.822

LOCAL FLOW FIELD DATA

*6 -1

MACH = .804 RE = 4.40x10 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THEYA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 145 1	.712	.704	.679	.657	.641	.595	.641	.780	.862	.900	.943	.970	.980
.641 207 0	.726	.702	.665	.668	.753	.814	.845	.851	.861	.881	.917	.944	.959
.703 159 0	.698	.649	.625	.691	.766	.807	.827	.837	.845	.853	.861	.864	.865
.839 161 0	.805	.740	.644	.659	.748	.805	.818	.825	.833	.840	.847	.849	.844
.966 175 0	.829	.704	.587	.621	.736	.810	.826	.828	.834	.840	.847	.848	.845
1.047 175 0	.649	.544	.528	.655	.781	.816	.817	.818	.819	.823	.829	.833	.840
1.170 161 0	.819	.657	.544	.668	.792	.808	.807	.809	.812	.813	.816	.820	.825
1.297 159 0	.787	.769	.689	.774	.810	.810	.810	.811	.813	.816	.820	.822	.824
1.439 145 1	.785	.796	.798	.802	.804	.805	.806	.808	.808	.809	.809	.811	.817

LOCAL FLOW FIELD DATA

MACH = .798 RE = 4.37x10⁺⁸ -1 ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

LOCAL ANGLE OF ATTACK		-- (ALPHA) --		DEC.										
THETA		180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.														
.315	123 0	8.586	8.402	12.764	17.102	18.227	15.822	9.238	1.595	16.809	30.079	26.442	27.892	28.657
.395	127 1	14.448	15.822	17.821	14.290	20.011	25.566	23.003	26.288	27.845	28.335	28.217	27.858	27.612
.438	123 0	12.853	15.784	14.640	10.875	25.347	29.746	28.869	27.849	27.878	27.881	27.628	27.450	26.736
.493	127 1	2.993	8.012	15.497	22.652	29.778	32.006	30.493	28.897	27.791	26.997	26.099	25.363	24.815
.566	131 0	2.702	6.698	14.776	22.161	26.674	27.180	27.322	26.542	25.857	25.826	25.594	25.066	24.615
.703	153 0	12.101	13.293	16.584	20.478	23.816	25.632	26.184	26.166	25.481	24.969	24.723	23.947	23.316
.839	167 0	16.290	17.200	19.648	22.092	23.809	24.991	25.948	25.114	24.392	24.203	24.001	23.320	22.561
.966	169 0	17.533	17.552	19.276	21.516	23.155	24.649	25.308	24.762	23.839	23.225	22.966	22.295	21.576
1.047	169 0	19.116	18.712	19.683	20.642	21.488	22.022	22.554	23.179	23.329	23.287	23.317	23.092	22.586
1.170	167 0	19.966	19.581	20.231	20.790	21.269	21.777	22.137	22.433	22.663	22.794	22.768	22.439	21.947
1.297	153 0	20.059	19.876	20.097	20.585	21.005	21.434	21.737	21.931	22.010	22.037	21.986	21.703	21.352
1.439	151 0	20.700	20.943	20.994	21.237	21.635	22.082	22.396	22.608	22.733	22.796	22.918	22.840	22.278

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.36x10 FT ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 143 0	.458	12.710	20.030	25.882	24.473	20.106	20.379	28.808	32.375	33.426	34.005	34.517	35.074
.438 139 0	1.543	8.106	20.853	29.179	31.260	28.288	31.379	34.131	34.701	35.044	35.193	35.654	35.975
.495 143 0	7.921	9.232	10.436	32.715	37.065	37.515	36.986	35.218	34.073	32.979	32.121	31.304	30.488
.566 149 0	5.132	7.569	13.218	27.121	34.372	35.394	34.611	33.148	31.836	31.071	30.604	30.325	29.883
.703 155 0	8.409	12.377	21.232	27.485	30.558	31.343	30.678	29.895	29.323	28.476	27.910	27.336	26.734
.839 165 0	18.197	19.274	22.207	24.208	25.090	26.299	27.369	27.954	28.453	27.259	25.869	25.323	24.924
.966 171 0	19.849	19.871	20.728	22.758	24.393	25.160	25.858	26.767	26.288	24.932	24.210	23.794	23.073
1.047 171 0	19.941	19.962	21.365	22.296	23.331	24.133	24.830	24.913	24.927	24.717	24.321	23.895	23.433
1.170 165 0	20.432	21.038	21.304	21.690	22.461	23.026	23.251	23.322	23.358	23.309	23.329	23.123	22.534
1.297 155 0	20.408	20.349	21.058	21.452	22.169	22.684	23.077	23.383	23.385	23.183	23.046	22.693	22.195
1.439 149 0	20.374	20.703	20.783	21.332	21.980	22.526	22.862	23.109	23.251	23.194	23.198	23.001	22.414

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.41X10 FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

LOCAL ANGLE OF ATTACK		-- (ALPHA) -- DEG.												
THETA		180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D	RUN NO.													
.566	147 0	6.295	7.749	14.852	31.726	22.264	19.249	11.974	18.080	28.701	21.920	22.877	26.508	29.840
.641	205 0	1.621	5.513	13.860	18.906	11.243	8.213	10.081	13.547	16.306	18.869	21.070	22.813	24.161
.703	157 1	3.779	4.949	9.411	24.804	24.401	18.980	18.449	18.598	18.658	19.735	20.846	21.820	23.239
.839	163 0	1.317	5.268	14.172	22.757	26.216	24.862	22.826	21.027	20.881	21.091	21.385	21.569	21.675
.966	173 0	9.138	11.163	16.084	22.143	24.323	24.129	24.573	22.335	21.514	21.773	21.832	21.418	21.060
1.047	173 0	12.311	14.132	17.586	21.013	22.201	22.244	21.887	21.947	22.101	22.184	22.385	22.285	22.047
1.170	163 0	14.344	16.040	18.022	20.102	21.410	21.725	21.923	22.002	21.989	22.324	22.629	21.971	21.860
1.297	157 1	16.040	16.742	18.035	19.667	20.712	21.123	21.451	21.787	21.827	21.845	21.987	21.812	21.531
1.439	147 0	17.777	17.614	18.721	19.638	20.675	21.598	22.019	22.311	22.397	22.417	22.629	22.521	22.302

LOCAL FLOW FIELD DATA

+6 -1

MACH = .804 RE = 4.40X10 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 145 1 4.451	4.259	3.763	.925	4.303	10.739	21.704	25.715	26.428	27.964	29.898	31.476	32.421	
.641 207 0 5.212	3.601	3.121	11.418	16.807	20.286	22.514	23.656	24.659	25.429	26.313	26.947	27.331	
.703 159 0 6.419	2.936	7.885	16.124	19.021	20.555	22.371	23.774	24.709	25.402	26.245	27.293	28.110	
.839 161 0 4.597	2.348	8.611	18.275	19.922	20.258	21.722	22.812	23.669	24.250	24.673	25.086	26.078	
.966 175 0 3.211	.928	13.142	22.783	22.260	21.413	21.836	22.387	22.832	23.297	23.371	23.503	23.678	
1.047 175 0 .973	10.317	22.220	22.842	21.146	20.963	21.897	22.664	23.337	23.781	24.085	24.038	24.017	
1.170 161 0 3.739	6.885	21.826	22.858	21.698	21.551	21.898	22.250	22.610	23.082	23.376	23.304	23.134	
1.297 159 0 8.934	10.393	16.962	20.471	21.183	20.950	21.403	21.784	22.122	22.405	22.618	22.603	22.455	
1.439 145 1 12.881	14.377	17.778	20.693	21.594	21.801	21.979	22.120	22.373	22.757	23.196	23.171	22.697	

LOCAL FLOW FIELD DATA

MACH = .798 RE = 4.37X10 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

CROSSFLOW DIRECTION (THETAVC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 123 0	180.0	-147.8	-112.2	-85.3	-59.5	-44.6	-50.7	-17.9	57.8	69.1	76.9	80.3	83.8
.395 127 1	180.0	-151.0	-136.3	-90.1	-14.2	18.2	39.3	60.7	64.3	68.0	72.6	78.1	83.4
.438 123 0	-180.0	172.7	167.2	73.7	36.3	33.0	40.1	47.0	54.0	60.8	66.8	72.8	78.6
.495 127 1	-180.0	115.3	99.8	77.6	55.4	46.6	45.5	48.6	54.5	60.4	65.6	70.8	76.7
.566 151 0	.0	65.2	75.8	72.3	59.9	52.7	54.8	58.2	62.4	67.2	72.8	78.3	83.7
.703 153 0	.0	21.5	38.1	45.9	49.4	51.1	53.0	56.5	60.8	65.2	70.5	76.5	82.7
.839 167 0	.0	13.7	26.8	35.1	41.4	46.2	51.0	54.3	59.0	64.5	70.0	76.1	82.6
.966 169 0	.0	6.3	20.6	31.0	39.1	45.5	50.1	54.0	58.4	63.6	69.4	75.8	82.6
1.047 169 0	.0	16.5	23.4	31.6	38.6	44.8	50.2	55.3	60.6	66.0	71.9	78.6	84.5
1.170 167 0	.0	13.8	20.7	28.7	35.7	42.3	48.2	54.0	59.7	65.7	72.0	78.8	84.5
1.297 153 0	.0	13.4	19.8	27.7	34.9	42.1	48.0	54.2	60.2	65.9	72.2	79.3	85.4
1.439 151 0	.0	14.0	19.5	27.0	33.7	40.6	46.5	52.2	58.4	64.3	70.6	77.1	83.1

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.36X10 FT ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 143 0	180.0	-69.4	-53.6	-37.5	-24.0	-11.1	11.3	44.5	56.3	56.4	61.3	66.1	67.2
.438 139 0	180.0	-66.2	-59.9	-36.1	-14.7	-2.2	16.8	36.0	41.2	44.4	50.4	56.0	60.5
.495 143 0	180.0	-154.8	-41.3	1.3	11.2	21.1	31.5	35.8	39.2	43.7	48.8	54.2	59.3
.566 149 0	-180.0	144.6	81.4	44.3	30.4	32.9	36.2	38.4	43.6	49.0	54.9	60.1	64.8
.703 155 0	.0	45.4	53.1	46.9	41.0	38.5	39.4	42.7	47.2	51.9	57.6	62.8	67.9
.839 165 0	.0	10.7	23.7	29.3	34.3	39.7	43.9	47.5	51.8	55.8	61.2	66.9	72.0
.966 171 0	.0	6.1	17.8	27.7	33.5	38.7	43.6	48.3	52.3	56.9	62.3	67.3	73.0
1.047 171 0	.0	16.7	22.5	30.3	37.0	41.5	45.2	49.6	54.0	59.4	64.8	70.1	77.0
1.170 165 0	.0	14.3	20.3	28.7	34.9	40.6	45.4	50.4	55.6	61.0	66.5	72.8	79.3
1.297 155 0	.0	13.7	20.6	28.3	34.6	40.7	45.8	50.5	55.7	61.4	67.1	73.2	79.7
1.439 149 0	.0	13.8	19.6	27.1	33.5	40.0	45.0	50.1	55.8	61.5	67.1	73.2	80.0

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.41x10 FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 147 0	180.0	-147.9	-121.7	-110.8	164.0	157.7	-170.7	178.6	158.8	119.8	106.7	106.1	103.2
.641 205 0	-180.0	-107.9	-66.9	-58.8	-60.7	-24.7	22.1	57.8	71.0	78.1	82.8	86.0	88.5
.703 157 1	180.0	-158.3	-79.7	-25.7	-11.8	.3	28.4	45.0	58.5	68.9	76.8	82.5	86.2
.839 163 0	.0	81.3	74.9	46.5	31.9	33.5	39.0	46.2	56.4	64.7	71.8	77.9	83.3
.966 173 0	.0	30.5	46.5	47.2	43.8	44.1	49.0	52.3	58.0	64.7	70.7	76.5	82.3
1.047 173 0	.0	31.2	38.0	39.5	40.8	43.8	48.1	53.2	58.7	64.2	69.9	76.0	82.3
1.170 163 0	.0	24.8	31.0	36.7	40.3	44.2	48.4	53.5	59.2	65.4	71.6	77.0	83.1
1.297 157 1	.0	20.1	26.9	34.1	39.6	44.5	49.3	54.5	59.9	65.8	71.6	77.6	83.6
1.439 147 0	.0	18.2	24.4	32.3	38.3	43.4	48.0	53.5	59.1	64.8	70.3	76.2	82.1

LOCAL FLOW FIELD DATA

MACH = .604 RE = 4.40x10 FT ALPHA = 20.080 X/D = 5.500 TEST NO. = 35

CROSSFLOW DIRECTION (THETA) MODEL RADIAL L.

THEYA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 145 1	180.0	-142.9	-111.1	-110.1	101.5	87.3	77.7	79.4	83.0	85.8	87.3	88.2	89.2
.641 207 0	180.0	-136.4	35.3	54.9	66.2	69.7	68.6	68.7	71.6	76.0	80.1	83.4	86.0
.703 159 0	180.0	176.2	36.9	49.2	58.3	62.4	65.0	68.3	72.9	77.5	81.9	85.1	87.8
.639 161 0	180.0	-139.2	1.2	27.0	42.3	50.7	57.4	63.7	69.2	74.4	79.4	83.9	87.5
.966 175 0	180.0	-99.6	11.2	30.6	41.5	46.6	52.6	59.3	65.5	71.4	77.8	82.8	87.1
1.047 175 0	.0	15.2	34.7	42.9	46.0	50.5	56.1	61.7	67.0	72.9	78.9	84.2	90.0
1.170 161 0	.0	43.9	39.6	40.2	42.0	46.9	53.5	59.9	65.6	71.7	77.6	83.2	89.5
1.297 159 0	.0	40.1	41.1	40.5	42.3	48.2	54.2	59.9	65.4	71.3	77.5	83.4	89.2
1.439 145 1	.0	32.9	37.5	38.3	40.9	45.7	51.4	57.8	63.5	69.5	75.5	81.1	87.3

LOCAL FLOW FIELD DATA

MACH = .796 RE = 4.37X10 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 123 0	.000	-.028	-.049	-.056	-.072	-.056	.033	.099	.164	.162	-.009	-.022	.005
.395 127 1	-.049	-.097	-.167	-.224	-.154	-.000	.069	.085	.028	.040	.044	.043	.053
.438 123 0	.005	-.043	-.169	-.228	-.184	-.064	-.041	-.043	-.005	.022	.038	.049	.043
.495 127 1	.056	.040	-.026	-.083	-.061	-.048	-.024	.006	.019	.022	.019	.019	.029
.566 151 0	.104	.105	.062	-.011	.014	.054	.079	.047	.029	.039	.035	.027	.032
.703 153 0	.091	.093	.087	.081	.076	.066	.074	.065	.039	.035	.040	.033	.039
.839 167 0	.071	.084	.097	.095	.084	.092	.105	.066	.042	.039	.044	.042	.039
.966 169 0	.030	.025	.052	.076	.081	.097	.102	.071	.036	.025	.025	.021	.019
1.047 169 0	.075	.060	.068	.061	.050	.043	.042	.052	.055	.056	.066	.073	.068
1.170 167 0	.073	.050	.062	.058	.054	.051	.047	.050	.056	.067	.074	.069	.068
1.297 153 0	.040	.025	.028	.030	.029	.028	.028	.029	.032	.036	.037	.036	.037
1.439 151 0	.045	.041	.043	.043	.043	.044	.051	.057	.059	.065	.073	.079	.080

LOCAL FLOW FIELD DATA

*6 -1

MACH = .707 RE = 4.36x10 FT ALPHA = 20.080 X/D = 4.100 TEST NO. = 95

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 143 0	.194	.165	.111	.073	.081	.090	.146	.184	.165	.159	.150	.140	.166
.438 139 0	.079	.077	.016	-.034	-.035	-.050	.058	.051	.046	.076	.090	.124	.161
.495 143 0	-.082	-.126	-.231	-.165	-.083	.010	.005	-.010	.015	.023	.033	.044	.063
.566 149 0	-.048	-.087	-.211	-.239	-.149	-.074	-.057	-.028	.004	.034	.061	.090	.118
.703 155 0	.010	-.013	-.048	-.102	-.113	-.086	-.063	-.038	-.011	-.006	.013	.038	.069
.839 165 0	-.036	-.018	-.017	-.023	-.034	-.035	-.022	-.001	.029	.006	-.004	.019	.039
.966 171 0	-.063	-.066	-.064	-.042	-.042	-.046	-.031	.011	.004	-.015	-.019	-.006	.011
1.047 171 0	-.021	-.024	-.023	-.026	-.034	-.033	-.018	-.010	.007	.019	.032	.052	.075
1.170 165 0	-.022	-.028	-.029	-.032	-.036	-.037	-.035	-.027	-.011	.006	.019	.038	.049
1.297 155 0	-.014	-.032	-.024	-.033	-.030	-.034	-.025	-.012	-.006	.002	.016	.026	.034
1.439 149 0	-.022	-.019	-.023	-.023	-.020	-.016	-.015	-.006	.007	.016	.026	.043	.046

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.41x10⁶ FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 147 0	-1.055	-1.099	-.662	-.597	-.656	-.539	-.582	-.532	-.455	-.728	-1.134	-1.032	-.845
.641 205 0	-.820	-.785	-.924	-1.009	-.830	-.849	-.814	-.829	-.878	-.821	-.738	-.693	-.667
.703 157 1	-.683	-.632	-.710	-.841	-.911	-.488	-.483	-.614	-.611	-.602	-.593	-.586	-.341
.839 163 0	-.458	-.476	-.581	-.616	-.537	-.497	-.471	-.464	-.454	-.451	-.452	-.451	-.447
.966 173 0	-.270	-.277	-.367	-.320	-.270	-.225	-.140	-.256	-.318	-.309	-.311	-.330	-.322
1.047 173 0	-.142	-.177	-.217	-.224	-.233	-.230	-.216	-.189	-.182	-.174	-.161	-.158	-.157
1.170 163 0	-.114	-.116	-.122	-.133	-.139	-.143	-.137	-.135	-.133	-.119	-.103	-.116	-.100
1.297 157 1	-.096	-.101	-.108	-.111	-.112	-.120	-.126	-.114	-.109	-.106	-.097	-.093	-.095
1.439 147 0	-.048	-.068	-.062	-.073	-.076	-.069	-.066	-.066	-.072	-.064	-.051	-.045	-.047

LOCAL FLOW FIELD DATA

MACH = .804 RE = 4.40X10 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.988 145 1	-.007	.002	.008	.003	-.017	-.034	-.007	-.075	-.171	-.246	-.331	-.379	-.393
.841 207 0	-.019	-.015	-.000	.003	-.029	-.085	-.118	-.128	-.155	-.199	-.277	-.342	-.374
.703 159 0	-.025	-.003	.008	.005	-.010	-.037	-.069	-.092	-.114	-.137	-.155	-.154	-.145
.839 161 0	-.046	-.015	.006	-.002	-.022	-.042	-.049	-.068	-.089	-.112	-.128	-.134	-.113
.966 175 0	-.054	.001	.004	.007	-.009	-.030	-.035	-.047	-.068	-.084	-.104	-.115	-.109
1.047 175 0	-.049	-.015	.042	.054	.002	-.015	-.010	-.016	-.021	-.030	-.043	-.055	-.062
1.170 161 0	-.010	-.018	.005	.019	-.010	-.012	-.010	-.018	-.027	-.027	-.030	-.049	-.050
1.297 159 0	.043	-.047	-.022	-.023	-.019	-.012	-.011	-.014	-.017	-.025	-.038	-.045	-.049
1.439 145 1	.044	.007	-.008	.005	.013	.014	.013	.005	.001	-.000	.002	-.006	-.022

LOCAL FLOW FIELD DATA

MACH = .798 RE = 4.37X10⁺⁶ FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 123 0	1.003	.999	.998	.994	.993	.992	.941	.863	.862	.931	.990	.998	1.003
.395 127 1	1.003	1.001	.947	.848	.854	.943	.970	.963	.994	.998	1.000	.999	.999
.438 123 0	1.006	.996	.902	.814	.887	.968	.988	.994	.999	1.003	1.004	1.005	1.002
.495 127 1	1.003	1.005	.974	.929	.940	.985	1.005	1.007	1.007	1.007	1.005	1.004	1.005
.566 151 0	1.000	1.000	.998	.992	1.002	1.009	1.012	1.004	.998	.998	.998	.994	.993
.703 153 0	.995	.997	.998	1.001	1.004	1.005	1.009	1.006	.997	.994	.996	.994	.993
.839 167 0	.995	.997	.998	1.003	1.005	1.009	1.013	1.004	.998	.996	.997	.996	.995
.966 169 0	.999	.998	1.001	1.007	1.011	1.016	1.019	1.012	1.003	1.000	.999	.997	.995
1.047 169 0	1.007	1.004	1.005	1.005	1.005	1.005	1.006	1.007	1.006	1.004	1.005	1.005	1.003
1.170 167 0	1.007	1.005	1.004	1.004	1.005	1.006	1.007	1.007	1.006	1.006	1.006	1.005	1.003
1.297 153 0	1.003	1.001	1.000	1.000	1.001	1.002	1.003	1.003	1.002	1.001	1.000	1.000	.998
1.439 151 0	1.005	1.006	1.005	1.005	1.006	1.008	1.010	1.009	1.008	1.006	1.006	1.006	1.004

LOCAL FLOW FIELD DATA

MACH = .797 $RE = 4.36 \times 10^6$ $\alpha = 20.080$ $X/D = 4.100$ TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.393 143 0	.998	1.006	1.013	1.013	.998	.945	.880	.878	.942	.991	.987	.980	.983
.438 139 0	1.004	1.001	.975	.965	1.001	.975	.922	.945	.992	1.002	1.000	1.005	1.009
.495 143 0	1.003	.948	.821	.850	.962	.960	.977	1.008	1.014	1.011	1.008	1.007	1.005
.566 149 0	1.003	.972	.887	.885	.942	.974	.995	1.002	1.001	1.002	1.003	1.003	1.002
.703 155 0	.996	.996	.985	.977	.987	.994	.995	.997	1.001	1.000	.998	.999	1.000
.839 165 0	.995	.996	.998	1.000	1.001	1.001	1.004	1.009	1.014	1.006	.998	.998	.999
.966 171 0	1.002	1.000	.999	1.004	1.006	1.006	1.009	1.018	1.013	1.005	1.001	1.000	1.000
1.047 171 0	1.006	1.004	1.005	1.005	1.006	1.007	1.008	1.008	1.009	1.008	1.007	1.007	1.007
1.170 165 0	1.006	1.005	1.005	1.005	1.006	1.007	1.006	1.007	1.007	1.007	1.006	1.007	1.006
1.297 155 0	1.005	1.002	1.002	1.002	1.004	1.005	1.006	1.007	1.005	1.004	1.004	1.002	1.001
1.439 149 0	1.006	1.005	1.005	1.004	1.006	1.008	1.009	1.009	1.009	1.008	1.007	1.005	1.004

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.41X10⁶ FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 147 0	.996	.973	.790	.582	.496	.582	.683	.639	.650	.876	1.033	1.058	1.043
.641 203 0	1.008	.985	.946	.840	.700	.891	.973	.986	1.011	1.007	1.004	1.004	1.005
.703 157 1	1.007	.971	.862	.876	.968	.931	.952	.993	.997	.997	.995	.994	.998
.839 163 0	1.003	.991	.952	.938	.954	.967	.998	.993	.996	.996	.995	.993	.992
.966 173 0	.997	.999	.998	1.008	1.010	1.011	1.019	1.006	.999	1.000	1.000	.996	.994
1.047 173 0	1.004	1.006	1.005	1.005	1.006	1.006	1.006	1.007	1.006	1.005	1.005	1.004	1.003
1.170 163 0	1.005	1.002	1.005	1.005	1.003	1.004	1.003	1.003	1.002	1.004	1.007	1.002	1.005
1.297 157 1	1.002	1.000	1.002	1.002	1.002	1.001	1.002	1.002	1.002	1.001	1.002	1.002	1.001
1.439 147 0	1.006	1.005	1.005	1.005	1.006	1.008	1.008	1.009	1.007	1.006	1.006	1.005	1.004

LOCAL FLOW FIELD DATA

*6 -1

MACH = .804 RE = 4.40x10 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.366 145 1	.913	.911	.895	.876	.857	.819	.860	.944	.982	.987	.990	.996	.999
.641 207 0	.924	.906	.882	.901	.944	.976	.990	.994	.994	.993	.992	.991	.991
.703 159 0	.896	.868	.856	.903	.960	.989	.994	.993	.993	.990	.990	.994	.999
.839 161 0	.986	.941	.871	.879	.946	.990	1.000	.998	.997	.995	.992	.992	.999
.966 175 0	.998	.910	.826	.850	.933	.993	1.004	1.002	1.000	.999	.995	.994	.997
1.047 175 0	1.028	.795	.805	.894	.979	1.006	1.007	1.007	1.006	1.005	1.004	1.004	1.004
1.170 161 0	1.021	.872	.806	.897	.991	1.006	1.006	1.004	1.003	1.003	1.004	1.003	1.003
1.297 159 0	1.006	.949	.892	.964	1.002	1.002	1.003	1.003	1.002	1.002	1.001	.999	1.001
1.439 145 1	1.003	.999	.993	1.003	1.008	1.009	1.009	1.007	1.007	1.007	1.007	1.003	1.003

LOCAL FLOW FIELD DATA

MACH = .798 RE = 4.37x10⁶ FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 123 0	-.150	-.125	-.085	.025	.163	.198	.093	.020	.108	.147	.100	.079	.052
.395 127 1	-.257	-.250	-.227	-.000	.297	.382	.281	.198	.198	.174	.138	.094	.052
.438 123 0	-.223	-.274	-.240	.047	.331	.414	.372	.323	.275	.226	.180	.134	.087
.495 127 1	-.051	-.059	-.045	.079	.271	.366	.362	.321	.270	.223	.181	.140	.096
.566 151 0	.045	.046	.060	.114	.224	.272	.258	.231	.198	.165	.125	.084	.044
.703 153 0	.199	.203	.214	.234	.254	.264	.258	.237	.205	.173	.136	.092	.049
.839 167 0	.269	.274	.285	.294	.292	.282	.265	.240	.208	.172	.135	.093	.048
.966 169 0	.297	.295	.301	.305	.296	.284	.266	.241	.208	.173	.136	.092	.047
1.047 169 0	.318	.300	.300	.293	.280	.262	.242	.220	.190	.157	.119	.075	.036
1.170 167 0	.332	.319	.315	.304	.288	.269	.247	.220	.190	.155	.116	.072	.035
1.297 153 0	.337	.327	.319	.307	.290	.268	.245	.216	.184	.151	.112	.067	.028
1.439 151 0	.348	.342	.333	.318	.302	.282	.258	.232	.198	.163	.126	.084	.044

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.36x10 FT ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 143 0	-.007	.072	.195	.339	.362	.298	.255	.247	.249	.277	.243	.208	.199
.438 139 0	-.026	.009	.172	.385	.511	.473	.434	.411	.415	.396	.351	.308	.269
.495 143 0	-.144	-.146	.122	.484	.591	.538	.498	.475	.437	.394	.348	.299	.252
.566 149 0	-.092	-.109	.033	.323	.492	.490	.469	.435	.382	.333	.285	.241	.200
.703 155 0	.145	.151	.219	.324	.400	.422	.405	.372	.335	.295	.249	.205	.164
.839 165 0	.316	.326	.348	.362	.356	.347	.336	.320	.295	.259	.210	.166	.127
.966 171 0	.351	.349	.348	.351	.354	.341	.324	.304	.274	.233	.193	.156	.114
1.047 171 0	.347	.332	.342	.334	.324	.314	.301	.277	.249	.213	.174	.135	.087
1.170 165 0	.355	.355	.347	.331	.321	.305	.284	.258	.227	.192	.158	.115	.070
1.297 155 0	.353	.344	.341	.328	.317	.299	.278	.256	.226	.189	.152	.110	.066
1.439 149 0	.354	.349	.340	.329	.318	.298	.279	.255	.223	.188	.152	.111	.065

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.41X10⁶ FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 147 0	-.166	-.174	-.150	-.127	-.141	-.186	-.184	-.237	-.324	-.231	-.176	-.190	-.163
.641 205 0	-.040	-.041	.133	.231	.106	.172	.223	.174	.131	.093	.061	.036	.014
.703 157 1	-.088	-.103	.036	.495	.576	.382	.332	.292	.216	.157	.104	.062	.033
.839 163 0	.028	.017	.079	.332	.458	.431	.370	.303	.240	.187	.139	.093	.052
.966 173 0	.179	.189	.225	.298	.340	.329	.297	.263	.225	.182	.142	.098	.056
1.047 173 0	.229	.228	.265	.308	.320	.306	.277	.246	.214	.179	.142	.099	.054
1.170 163 0	.263	.266	.283	.295	.299	.285	.265	.238	.205	.168	.129	.089	.047
1.297 157 1	.290	.284	.291	.293	.288	.273	.254	.228	.197	.161	.124	.084	.043
1.439 147 0	.315	.299	.303	.296	.289	.279	.261	.236	.204	.169	.134	.094	.054

LOCAL FLOW FIELD DATA

*6 -1

MACH = .804 RE = 4.40x10 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 145 1	-.070	-.053	-.020	-.005	-.012	.007	.064	.077	.058	.038	.027	.019	.009
.641 207 0	-.083	-.051	.038	.099	.111	.122	.146	.155	.141	.113	.086	.061	.037
.703 159 0	-.099	-.042	.088	.159	.164	.164	.165	.155	.129	.098	.067	.042	.019
.839 161 0	-.081	-.029	.123	.235	.238	.221	.204	.177	.149	.116	.081	.048	.020
.966 175 0	-.057	-.002	.167	.263	.262	.253	.231	.199	.167	.131	.088	.052	.022
1.047 175 0	.018	.121	.211	.236	.244	.231	.211	.185	.157	.121	.080	.043	.000
1.170 161 0	.067	.072	.202	.254	.273	.254	.225	.192	.161	.125	.087	.048	.003
1.297 159 0	.153	.133	.192	.258	.271	.240	.215	.188	.158	.124	.085	.045	.006
1.439 145 1	.219	.208	.241	.278	.279	.260	.234	.202	.171	.137	.100	.061	.019

LOCAL FLOW FIELD DATA

MACH = .798 RE = 4.37X10 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 123 0	.000	-.079	-.209	-.299	-.277	-.195	-.113	-.006	.171	.385	.431	.465	.477
.395 127 1	.000	-.139	-.217	-.229	-.075	.126	.230	.352	.412	.430	.441	.447	.447
.438 123 0	-.000	.035	.055	.160	.244	.269	.313	.347	.379	.405	.420	.432	.432
.495 127 1	-.000	.124	.259	.360	.393	.388	.368	.364	.379	.394	.399	.403	.405
.566 151 0	-.000	.100	.239	.358	.386	.357	.365	.373	.380	.393	.404	.407	.404
.703 153 0	.000	.080	.168	.241	.296	.328	.343	.358	.367	.374	.385	.385	.381
.839 167 0	-.000	.067	.144	.207	.257	.294	.327	.335	.346	.361	.373	.374	.371
.966 169 0	.000	.032	.113	.183	.241	.288	.319	.331	.339	.349	.360	.363	.359
1.047 169 0	.000	.089	.130	.180	.224	.260	.290	.318	.338	.353	.366	.373	.370
1.170 167 0	.000	.078	.119	.166	.207	.245	.276	.303	.326	.344	.357	.364	.361
1.297 153 0	.000	.078	.115	.161	.202	.242	.273	.299	.321	.337	.350	.357	.355
1.439 151 0	.000	.085	.118	.162	.202	.242	.272	.298	.322	.340	.357	.366	.363

LOCAL FLOW FIELD DATA

+6 -1

MACH = .797 RE = 4.36X10 FT ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 143 0	.000	-.190	-.264	-.260	-.161	-.059	.051	.243	.373	.417	.445	.468	.473
.438 139 0	.000	-.135	-.296	-.281	-.134	-.018	.131	.299	.363	.387	.424	.455	.475
.495 143 0	.000	-.069	-.107	.011	.117	.207	.305	.342	.357	.376	.397	.416	.425
.566 149 0	-.000	.077	.221	.315	.289	.317	.343	.345	.363	.384	.405	.420	.425
.703 155 0	-.000	.153	.292	.346	.348	.336	.332	.344	.362	.376	.392	.400	.402
.839 165 0	-.000	.062	.153	.203	.243	.289	.324	.349	.375	.380	.382	.389	.392
.966 171 0	.000	.037	.111	.185	.235	.274	.308	.341	.355	.358	.367	.373	.373
1.047 171 0	.000	.100	.142	.195	.244	.278	.303	.325	.343	.359	.370	.374	.376
1.170 165 0	.000	.090	.129	.181	.224	.261	.288	.311	.332	.348	.362	.371	.370
1.297 155 0	.000	.084	.128	.177	.218	.257	.286	.310	.330	.347	.359	.365	.366
1.439 149 0	.000	.088	.121	.168	.210	.250	.280	.305	.328	.346	.361	.368	.368

LOCAL FLOW FIELD DATA

*6 -1

MACH = .797 RE = 4.41x10 FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 147 0	.000	-.109	-.243	-.334	.041	.076	-.030	.006	.125	.402	.589	.660	.698
.641 205 0	-.000	-.125	-.311	-.382	-.189	-.079	.091	.276	.381	.444	.486	.518	.544
.703 157 1	.000	-.041	-.197	-.238	-.120	.002	.179	.292	.353	.406	.445	.471	.497
.839 163 0	.000	.111	.294	.350	.286	.286	.300	.317	.362	.396	.421	.437	.444
.966 173 0	-.000	.111	.237	.322	.325	.319	.342	.340	.359	.386	.404	.411	.410
1.047 173 0	.000	.138	.207	.255	.277	.294	.308	.329	.352	.371	.388	.398	.402
1.170 163 0	.000	.123	.170	.220	.253	.277	.299	.322	.344	.367	.386	.387	.390
1.297 157 1	.000	.104	.148	.199	.239	.268	.295	.320	.340	.358	.373	.380	.382
1.439 147 0	.000	.098	.137	.187	.229	.263	.290	.318	.341	.358	.374	.382	.386

LOCAL FLOW FIELD DATA

MACH = .804 RE = 4.40x10⁶ FT ALPHA = 20.080 Y/D = 6.500 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (V_{THETA}/V_{INF})

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 145 1	.000	-.040	-.053	-.013	.060	.142	.295	.415	.471	.518	.574	.617	.638
.641 207 0	.000	-.022	.027	.141	.251	.330	.374	.398	.424	.455	.493	.521	.538
.703 159 0	.000	.003	.066	.164	.266	.313	.355	.389	.419	.443	.467	.489	.504
.839 161 0	.000	-.025	.003	.120	.217	.271	.319	.358	.390	.415	.433	.446	.463
.966 175 0	.000	-.014	.033	.156	.232	.267	.302	.336	.365	.390	.406	.416	.425
1.047 175 0	-.000	.033	.146	.220	.253	.280	.313	.345	.371	.393	.411	.418	.421
1.170 161 0	.000	.070	.167	.214	.246	.271	.303	.332	.356	.378	.395	.404	.404
1.297 159 0	.000	.112	.167	.220	.246	.269	.299	.324	.346	.366	.383	.390	.391
1.439 145 1	.000	.134	.185	.219	.242	.266	.294	.320	.343	.365	.384	.392	.391

LOCAL FLOW FIELD DATA

MACH = .798 RE = 4.37X10 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

(VC / VIN * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 123 0	.436	.431	.658	.874	.936	.809	.426	.061	.590	1.201	1.288	1.374	1.398
.395 127 1	.747	.833	.913	.667	.891	1.170	1.056	1.176	1.332	1.351	1.346	1.330	1.312
.438 123 0	.650	.806	.716	.485	1.198	1.439	1.417	1.381	1.365	1.352	1.330	1.317	1.285
.495 127 1	.148	.400	.765	1.075	1.390	1.554	1.504	1.414	1.356	1.319	1.277	1.242	1.212
.566 151 0	.130	.322	.718	1.094	1.302	1.308	1.302	1.277	1.248	1.242	1.233	1.209	1.183
.703 153 0	.579	.636	.793	.978	1.137	1.225	1.250	1.252	1.225	1.200	1.188	1.154	1.120
.839 167 0	.783	.821	.929	1.047	1.133	1.186	1.227	1.201	1.175	1.165	1.155	1.124	1.089
.966 169 0	.864	.865	.937	1.036	1.113	1.179	1.209	1.193	1.160	1.134	1.121	1.090	1.055
1.047 169 0	.925	.911	.953	1.001	1.046	1.075	1.101	1.125	1.129	1.125	1.122	1.107	1.083
1.170 167 0	.966	.957	.981	1.008	1.034	1.061	1.080	1.092	1.099	1.098	1.094	1.080	1.055
1.297 153 0	.982	.980	.987	1.008	1.030	1.052	1.068	1.076	1.076	1.074	1.070	1.057	1.038
1.439 151 0	1.012	1.026	1.027	1.039	1.058	1.081	1.093	1.099	1.102	1.100	1.101	1.094	1.064

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.36x10 FT ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

(VC / VINF * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 143 0	.021	.592	.957	1.244	1.155	.886	.759	1.010	1.305	1.458	1.478	1.492	1.495
.438 139 0	.076	.395	.998	1.388	1.539	1.378	1.320	1.481	1.605	1.612	1.603	1.601	1.589
.495 143 0	.419	.470	.471	1.410	1.754	1.680	1.700	1.704	1.644	1.586	1.537	1.492	1.440
.566 149 0	.268	.389	.650	1.314	1.661	1.700	1.693	1.618	1.536	1.481	1.443	1.409	1.368
.703 155 0	.422	.626	1.062	1.379	1.543	1.571	1.525	1.474	1.436	1.392	1.352	1.310	1.264
.839 165 0	.921	.966	1.107	1.208	1.257	1.315	1.359	1.379	1.390	1.339	1.271	1.232	1.201
.966 171 0	1.022	1.022	1.063	1.155	1.236	1.275	1.302	1.330	1.305	1.244	1.206	1.179	1.135
1.047 171 0	1.010	1.011	1.079	1.126	1.181	1.220	1.245	1.244	1.236	1.217	1.190	1.159	1.124
1.170 165 0	1.035	1.066	1.079	1.099	1.140	1.169	1.178	1.177	1.171	1.158	1.150	1.131	1.096
1.297 155 0	1.028	1.031	1.061	1.085	1.120	1.148	1.163	1.171	1.166	1.150	1.136	1.112	1.082
1.439 149 0	1.032	1.045	1.050	1.077	1.109	1.134	1.152	1.158	1.157	1.148	1.141	1.121	1.090

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.41x10⁺⁶ FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

(VC / VINF * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.966 147 0	.484	.599	.832	1.042	.427	.585	.844	.690	1.012	1.350	1.790	2.002	2.087
.841 203 0	.116	.384	.986	1.301	.632	.552	.702	.951	1.174	1.323	1.426	1.513	1.584
.703 157 1	.257	.323	.584	1.600	1.713	1.111	1.099	1.202	1.206	1.268	1.331	1.385	1.450
.839 163 0	.082	.327	.886	1.405	1.573	1.507	1.388	1.277	1.265	1.275	1.292	1.300	1.302
.966 173 0	.523	.640	.950	1.277	1.370	1.335	1.319	1.252	1.233	1.244	1.248	1.231	1.206
1.047 173 0	.667	.777	.978	1.165	1.233	1.234	1.207	1.197	1.201	1.200	1.203	1.196	1.182
1.170 163 0	.766	.853	.961	1.072	1.140	1.158	1.164	1.167	1.165	1.176	1.186	1.155	1.143
1.297 157 1	.845	.881	.951	1.036	1.089	1.113	1.133	1.145	1.143	1.143	1.145	1.135	1.120
1.439 147 0	.917	.916	.969	1.019	1.074	1.118	1.137	1.152	1.158	1.153	1.156	1.147	1.136

LOCAL FLOW FIELD DATA

MACH = .804 RE = 4.40x10 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

(VC / VIN * SIN ALPHA)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 145 1	.203	.192	.164	.039	.178	.413	.879	1.231	1.382	1.513	1.673	1.797	1.860
.841 207 0	.243	.163	.134	.503	.799	1.026	1.169	1.245	1.300	1.364	1.457	1.529	1.571
.703 159 0	.287	.123	.319	.707	.910	1.029	1.139	1.219	1.278	1.322	1.373	1.429	1.469
.639 161 0	.235	.112	.359	.768	.939	1.018	1.104	1.165	1.216	1.256	1.283	1.306	1.351
.966 175 0	.167	.042	.496	.891	1.019	1.071	1.107	1.138	1.168	1.199	1.209	1.221	1.239
1.047 175 0	.052	.366	.748	.941	1.025	1.056	1.100	1.140	1.173	1.199	1.220	1.224	1.227
1.170 161 0	.195	.293	.763	.967	1.071	1.083	1.099	1.118	1.139	1.161	1.178	1.184	1.176
1.297 159 0	.446	.507	.743	.989	1.065	1.050	1.073	1.092	1.109	1.127	1.143	1.144	1.140
1.439 145 1	.637	.720	.886	1.030	1.075	1.084	1.094	1.103	1.116	1.136	1.155	1.156	1.139

LOCAL FLOW FIELD DATA

MACH = .798 RE = 4.37X10 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 123 0	.991	1.002	.997	.976	.976	.981	.898	.748	.671	.712	.889	.891	.873
.395 127 1	.996	1.009	.975	.899	.840	.840	.854	.817	.866	.860	.861	.864	.861
.438 123 0	.979	.979	.941	.866	.868	.865	.882	.897	.886	.878	.872	.870	.876
.495 127 1	.974	.975	.948	.884	.834	.854	.877	.880	.883	.889	.895	.899	.900
.566 151 0	.946	.940	.934	.922	.890	.874	.865	.877	.884	.881	.884	.888	.887
.703 153 0	.927	.924	.914	.899	.884	.877	.873	.875	.882	.885	.886	.892	.892
.839 167 0	.920	.911	.894	.885	.882	.874	.865	.880	.890	.890	.890	.895	.900
.966 169 0	.939	.939	.920	.902	.894	.882	.878	.888	.901	.907	.908	.912	.916
1.047 169 0	.916	.923	.914	.912	.912	.913	.910	.902	.899	.898	.893	.891	.894
1.170 167 0	.913	.924	.914	.912	.912	.912	.911	.908	.904	.897	.895	.898	.899
1.297 153 0	.923	.930	.926	.922	.921	.920	.919	.917	.914	.911	.910	.912	.912
1.439 151 0	.920	.921	.919	.918	.916	.915	.911	.906	.903	.898	.894	.892	.892

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.36x10⁶ ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 143 0	.899	.901	.901	.880	.871	.831	.701	.631	.707	.758	.752	.745	.731
.438 139 0	.964	.953	.900	.853	.870	.879	.743	.750	.796	.789	.780	.766	.751
.495 143 0	1.034	.992	.879	.753	.797	.751	.775	.829	.835	.839	.841	.842	.840
.566 149 0	1.023	1.004	.950	.881	.834	.822	.842	.851	.849	.844	.838	.827	.817
.703 155 0	.980	.979	.938	.910	.897	.885	.882	.880	.878	.881	.876	.870	.862
.839 165 0	.962	.948	.931	.922	.921	.914	.902	.892	.881	.892	.900	.894	.888
.966 171 0	.972	.971	.964	.946	.936	.932	.922	.905	.907	.919	.921	.918	.915
1.047 171 0	.956	.955	.947	.943	.940	.935	.924	.920	.913	.908	.904	.898	.890
1.170 165 0	.954	.951	.950	.949	.947	.944	.941	.937	.931	.923	.916	.909	.907
1.297 155 0	.949	.955	.947	.948	.944	.943	.937	.930	.925	.922	.917	.913	.911
1.439 149 0	.954	.950	.950	.946	.943	.939	.938	.932	.924	.920	.914	.907	.907

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.41×10^{-1} FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.966 147 0	1.506	1.512	1.077	.578	.358	.575	.881	.726	.635	1.152	1.456	1.378	1.249
.841 205 0	1.404	1.364	1.372	1.304	1.091	1.314	1.355	1.355	1.378	1.329	1.271	1.235	1.212
.703 157 1	1.334	1.279	1.210	1.189	1.296	1.110	1.131	1.227	1.226	1.214	1.200	1.188	1.159
.839 163 0	1.226	1.219	1.204	1.150	1.097	1.117	1.132	1.141	1.138	1.135	1.133	1.129	1.125
.966 173 0	1.116	1.113	1.132	1.078	1.041	1.024	.990	1.047	1.074	1.069	1.069	1.078	1.075
1.047 173 0	1.049	1.060	1.060	1.041	1.037	1.036	1.032	1.020	1.015	1.011	1.003	1.002	1.002
1.170 163 0	1.028	1.018	1.014	1.005	.998	.998	.993	.992	.991	.983	.977	.983	.979
1.297 157 1	1.009	1.006	1.003	.995	.989	.989	.990	.983	.980	.979	.974	.973	.975
1.439 147 0	.982	.990	.982	.981	.977	.969	.966	.964	.965	.960	.952	.950	.951

LOCAL FLOW FIELD DATA

MACH = .804 RE = 4.40X10 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

AXIAL VELOCITY RATIO -- (VX / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 145 1	.893	.886	.859	.835	.814	.748	.758	.877	.954	.978	.999	1.008	1.005
.641 207 0	.913	.887	.844	.855	.908	.953	.968	.967	.973	.985	1.012	1.033	1.044
.703 159 0	.877	.825	.790	.840	.907	.942	.950	.950	.953	.955	.956	.951	.944
.839 161 0	1.004	.936	.814	.798	.889	.947	.951	.951	.953	.957	.959	.958	.948
.966 175 0	1.023	.887	.729	.729	.855	.938	.949	.948	.953	.956	.961	.964	.961
1.047 175 0	1.055	.690	.629	.767	.910	.946	.939	.937	.934	.934	.937	.942	.945
1.170 161 0	1.026	.833	.654	.788	.924	.942	.939	.938	.939	.935	.936	.944	.945
1.297 159 0	.973	.949	.836	.909	.943	.942	.939	.938	.937	.938	.942	.943	.947
1.439 145 1	.957	.965	.949	.936	.932	.931	.930	.932	.931	.930	.926	.927	.935

LOCAL VORTICITY X 100.

MACH = .798 RE = 4.37X10 FT ALPHA = 20.080 X/D = 3.300 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.3550	-4.071	-4.738	83.436	144.165	106.449	49.037	75.924	133.822	73.231	15.984	12.904	5.951
.4165	36.735	138.669	305.934	340.559	181.285	47.035	11.130	.202	-9.105	-6.893	-4.858	-2.721
.4665	9.598	80.545	183.952	189.770	112.726	46.602	16.251	3.279	-1.409	-3.668	-6.449	-8.676
.5305	-2.670	5.831	42.337	70.446	37.192	8.045	6.017	4.242	3.844	4.698	5.901	4.296
.6345	.813	1.269	3.819	13.378	11.277	5.939	3.618	2.375	2.133	.225	-.886	-.980
.7710	1.153	3.036	4.318	3.621	2.881	3.200	1.853	-.701	.232	.617	-.412	-.626
.9025	-2.333	-2.131	.489	1.112	2.949	3.417	2.599	1.418	.314	-.392	-1.360	-1.716
1.0065	7.612	14.097	5.509	.080	-3.681	-5.083	-3.132	-.011	2.555	3.319	3.207	4.264
1.1085	-2.731	-.200	-.819	-1.099	-1.176	-.469	-.382	-.578	-.335	-.501	-1.171	-.286
1.2335	-.961	.591	.036	.207	.567	1.114	.748	.606	.250	-.362	-1.012	.170
1.3680	.307	1.512	1.011	1.137	.957	1.382	1.184	1.120	1.740	1.893	1.881	2.526

LOCAL VORTICITY X 100.

MACH = .797 RE = 4.36x10 FT ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.4165	37.131	58.995	49.820	23.557	-9.415	17.826	43.511	33.730	13.836	-7.527	-.962	13.687
.4665	18.665	136.258	214.326	162.912	88.190	79.860	52.783	19.409	3.198	-5.892	-10.754	-13.504
.5305	22.388	155.520	233.630	142.093	50.707	28.716	12.732	1.905	3.423	4.264	4.759	4.624
.6345	7.517	52.303	80.119	57.871	22.936	7.947	2.283	.063	.499	-.790	-.251	-.055
.7710	-4.731	-4.610	-3.144	-4.820	-2.431	1.806	4.533	5.607	4.223	.148	-.101	1.016
.9025	-.687	-1.813	.480	3.074	2.613	2.284	3.027	1.289	-2.227	-2.924	-1.183	-1.431
1.0065	8.943	17.494	9.749	7.717	6.293	4.152	.489	-1.187	.065	2.255	2.650	1.306
1.1085	-1.199	.527	-1.252	-.404	-.310	.245	-.352	-.219	-.703	-.183	.212	-.633
1.2335	-.469	.769	.374	1.417	1.238	1.741	2.025	1.594	1.103	1.229	.051	-.412
1.3680	-.098	.607	-.330	.466	.362	.975	1.079	.883	.947	1.469	1.264	.928

LOCAL VORTICITY X 100.

+6 -1

MACH = .797 RE = 4.41X10 FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.6035	-6.478	9.109	-13.261	-77.220	-62.315	3.104	52.679	75.237	72.485	13.352	-23.724	-23.491
.6720	13.254	78.101	120.710	27.966	8.467	36.085	16.185	-7.109	-12.466	-11.391	-9.433	-7.313
.7710	11.326	85.328	189.091	119.242	39.671	29.709	8.962	-3.362	-1.846	-2.128	-1.823	-1.781
.9025	1.436	9.947	34.399	27.815	11.616	6.141	4.746	.872	-.885	-.934	-2.003	-2.891
1.0065	6.535	10.656	2.443	-5.482	-6.387	-7.052	-4.801	-.766	-1.512	-2.608	-2.667	-1.403
1.1085	.113	2.888	2.312	1.073	-.250	-.119	.426	.380	.654	1.299	.305	-1.038
1.2335	-.942	.654	.812	.918	.624	1.431	1.578	1.059	.188	-.607	-.335	.067
1.3680	-1.147	1.554	.754	.996	1.545	1.738	1.423	1.598	1.575	1.735	1.522	1.880

LOCAL VORTICITY X 100.

MACH = .804 RE = 4.40x10 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

THETA 176.25 168.75 161.25 153.75 146.25 138.75 131.25 123.75 116.25 108.75 101.25 93.75

R/D

.6035	10.027	34.349	52.182	62.627	76.112	69.369	29.189	1.515	-6.433	-9.133	-11.727	-13.886
.6720	17.478	44.693	39.253	21.879	11.901	9.054	8.160	6.578	4.638	1.316	-.709	-.903
.7710	10.654	26.940	13.980	-2.903	-1.911	1.093	.929	.416	.470	.339	.678	1.469
.9025	12.096	38.104	30.693	10.201	5.140	1.828	-.958	-1.188	-1.334	-2.088	-1.126	-.842
1.0065	22.400	50.600	42.405	19.223	9.470	6.966	5.760	5.251	4.008	3.303	4.437	3.286
1.1085	13.676	27.080	12.383	6.341	1.503	.390	.051	.095	-.781	-1.037	-.530	-1.443
1.2335	3.960	21.394	13.653	7.757	1.156	.867	.561	.456	-.293	-.639	-.646	-.997
1.3680	.928	12.744	12.218	4.727	.657	.912	.670	1.254	1.271	1.467	1.898	1.520

LOCAL CIRCULATION STRENGTH X 100.

*6 -1

MACH = .798 RE = 4.37X10 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.3550	-.023	-.022	.395	.682	.504	.232	.359	.633	.347	.076	.061	.028	3.2721
.4165	.116	.414	.913	1.017	.541	.140	.033	.001	-.027	-.021	-.015	-.008	3.1042
.4665	.043	.357	.815	.841	.500	.207	.072	.015	-.006	-.016	-.029	-.038	2.7589
.5305	-.017	.037	.266	.442	.233	.051	.038	.027	.024	.029	.037	.027	1.1939
.6345	.012	.018	.055	.194	.163	.086	.052	.034	.031	.003	-.013	-.014	.6227
.7710	.020	.053	.075	.063	.050	.056	.032	-.012	.004	.011	-.007	-.011	.3351
.9025	-.045	-.041	.009	.021	.056	.065	.050	.027	.006	-.007	-.026	-.033	.0834
1.0065	.103	.192	.075	.001	-.050	-.069	-.043	-.000	.035	.045	.044	.058	.3905
1.1085	-.062	-.005	-.019	-.025	-.027	-.011	-.009	-.013	-.008	-.011	-.027	-.006	-.2215
1.2335	-.025	.015	.001	.005	.015	.029	.020	.016	.007	-.009	-.026	.004	.0510
1.3680	.010	.049	.033	.037	.031	.045	.038	.036	.036	.061	.061	.082	.5390
RSUM	.132	1.067	2.619	3.279	2.017	.831	.643	.763	.468	.160	.060	.088	12.1292

LOCAL CIRCULATION STRENGTH X 100.

*6 -1

MACH = .797 RE = 4.36x10 FT ALPHA = 20.080 Y/D = 4.100 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.4165	.111	.176	.149	.072	-.028	.053	.130	.101	.041	-.022	-.003	.041	.8184
.4665	.083	.604	.950	.722	.391	.354	.234	.086	.014	-.026	-.048	-.060	3.3036
.5305	.141	.995	1.467	.892	.318	.180	.080	.012	.021	.027	.030	.029	4.1919
.6345	.109	.758	1.161	.858	.332	.115	.033	.001	.007	-.011	-.004	-.001	3.3386
.7710	-.083	-.081	-.055	-.084	-.042	.032	.079	.098	.074	.003	-.002	.018	-.0437
.9025	-.017	-.035	.009	.059	.050	.044	.058	.025	-.043	-.056	-.023	-.027	.0440
1.0065	.122	.238	.132	.105	.086	.056	.007	-.016	.001	.031	.036	.018	.8142
1.1085	-.027	.012	-.028	-.009	-.007	.006	-.008	-.005	-.016	-.004	.005	-.014	-.0971
1.2335	-.012	.020	.010	.037	.032	.045	.053	.042	.029	.032	.001	-.011	.2783
1.3680	-.003	.020	-.011	.015	.012	.032	.035	.029	.031	.048	.041	.030	.2769
RSUM	.422	2.707	3.783	2.645	1.143	.917	.700	.371	.160	.020	.034	.022	12.9253

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = .797 RE = 4.41x10 FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

THETA	176.25	166.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.6035	-.049	.069	-.100	-.583	-.470	.023	.397	.568	.547	.101	-.179	-.177	.1469
.6720	.092	.542	.838	.194	.059	.251	.112	-.049	-.087	-.079	-.066	-.051	1.7572
.7710	.198	1.491	3.305	2.084	.693	.519	.157	-.059	-.032	-.037	-.032	-.031	8.2555
.9025	.027	.190	.657	.531	.222	.117	.091	.017	-.017	-.018	-.038	-.055	1.7242
1.0065	.089	.145	.033	-.074	-.087	-.096	-.065	-.010	-.021	-.035	-.036	-.019	-.1772
1.1085	.003	.066	.053	.024	-.006	-.003	.010	.009	.015	.030	.007	-.024	.1828
1.2335	-.025	.017	.021	.024	.016	.037	.041	.028	.005	-.016	-.009	.002	.1422
1.3680	-.037	.050	.024	.032	.050	.056	.046	.052	.051	.056	.049	.061	.4912
RSUM	.298	2.570	4.831	2.233	.478	.906	.789	.554	.461	.001	-.303	-.294	12.5229

LOCAL CIRCULATION STRENGTH X 100.

*6 -1

MACH = .804 RE = 4.40x10 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

THETA	176.25	166.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.6035	.076	.259	.394	.472	.574	.523	.220	.011	-.049	-.069	-.088	-.105	2.2193
.6720	.121	.310	.273	.152	.083	.063	.057	.046	.032	.009	-.005	-.006	1.1342
.7710	.186	.471	.244	-.051	-.033	.019	.016	.007	.008	.006	.012	.026	.9115
.9025	.231	.728	.586	.195	.098	.035	-.018	-.023	-.025	-.040	-.022	-.016	1.7293
1.0065	.304	.688	.576	.261	.129	.095	.078	.071	.054	.045	.060	.045	2.4065
1.1085	.311	.615	.281	.144	.034	.009	.001	.002	-.018	-.024	-.012	-.033	1.3118
1.2335	.103	.559	.356	.203	.030	.023	.015	.012	-.008	-.017	-.017	-.026	1.2331
1.3680	.030	.413	.396	.153	.021	.030	.022	.041	.041	.048	.061	.049	1.5037
RSUM	1.363	4.042	3.106	1.529	.936	.796	.391	.168	.037	-.042	-.010	-.066	12.2494

SECTION II $M_{\infty}=0.8, \alpha=24.6^{\circ}, Re=4.4 \times 10^6 \text{ ft}^{-1},$ $X/D = 3.5, 4.1, 4.8, 6.5$

LOCAL FLOW FIELD DATA

MACH = .798 RE = 4.37x10⁺⁶ FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

LOCAL MACH NO. --- (M) ---

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 124 0	.819	.826	.828	.851	.864	.830	.648	.564	.755	.834	.839	.840	.827
.395 128 1	.895	.846	.814	.809	.826	.811	.658	.666	.774	.789	.799	.795	.786
.438 124 0	.957	.884	.777	.748	.753	.815	.849	.847	.831	.829	.827	.825	.814
.495 128 1	.866	.827	.728	.786	.833	.846	.861	.851	.840	.832	.830	.828	.825
.566 152 0	.811	.786	.784	.793	.847	.850	.830	.822	.814	.809	.804	.801	.795
.703 154 0	.751	.753	.774	.807	.825	.829	.824	.816	.808	.803	.798	.794	.789
.839 168 0	.757	.748	.760	.781	.802	.809	.807	.811	.810	.804	.798	.794	.788
.966 170 0	.775	.775	.774	.782	.793	.801	.798	.805	.807	.804	.800	.798	.794
1.047 170 0	.770	.775	.780	.790	.792	.793	.792	.794	.792	.789	.790	.789	.783
1.170 168 0	.775	.782	.785	.794	.797	.799	.797	.795	.795	.791	.790	.792	.784
1.297 154 0	.790	.796	.797	.801	.801	.799	.798	.798	.797	.797	.797	.796	.793
1.439 152 0	.788	.797	.797	.800	.800	.798	.797	.799	.796	.795	.794	.793	.790

LOCAL FLOW FIELD DATA

MACH = .802 RE = 4.36X10⁶ FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 144 1	.701	.708	.743	.781	.794	.782	.661	.562	.663	.720	.733	.736	.726
.438 140 0	.754	.736	.785	.813	.880	.884	.724	.718	.784	.801	.797	.779	.765
.495 144 1	.885	.834	.704	.766	.889	.785	.785	.854	.868	.861	.839	.810	.797
.566 150 0	.901	.870	.773	.844	.901	.804	.819	.862	.853	.831	.810	.798	.790
.703 156 0	.848	.813	.812	.849	.919	.933	.913	.879	.850	.831	.815	.801	.786
.839 166 0	.802	.804	.821	.849	.862	.862	.861	.853	.838	.823	.808	.798	.786
.966 172 0	.823	.821	.831	.844	.856	.865	.865	.853	.846	.837	.824	.813	.805
1.047 172 0	.808	.817	.826	.833	.833	.834	.835	.832	.824	.817	.812	.805	.796
1.170 166 0	.817	.821	.825	.834	.833	.832	.831	.828	.825	.820	.815	.807	.798
1.297 156 0	.818	.822	.826	.830	.830	.827	.827	.826	.822	.817	.813	.808	.798
1.439 150 0	.819	.823	.824	.827	.827	.825	.824	.825	.823	.819	.815	.809	.803

LOCAL FLOW FIELD DATA

MACH = .803 RE = 4.41x10 FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 148 0	1.301	1.338	.963	.373	.296	.409	.560	.627	.689	1.197	1.385	1.221	1.139
.641 206 0	1.161	1.131	1.205	.869	.586	1.102	1.120	1.124	1.212	1.179	1.155	1.132	1.108
.703 158 1	1.107	1.113	1.056	1.044	1.206	1.154	.965	1.034	1.091	1.084	1.091	1.077	1.057
.839 164 0	1.034	1.016	1.077	1.123	1.057	1.063	1.053	1.011	1.008	1.015	1.020	1.019	1.002
.966 174 0	.904	.931	.978	1.055	1.061	1.022	.974	.978	.985	.977	.975	.977	.964
1.047 174 0	.856	.892	.929	.951	.947	.928	.907	.902	.902	.917	.927	.922	.900
1.170 164 0	.838	.844	.861	.878	.877	.876	.874	.873	.875	.873	.873	.872	.864
1.297 158 1	.832	.837	.843	.858	.860	.862	.863	.864	.865	.864	.865	.865	.859
1.439 148 0	.825	.836	.838	.849	.854	.856	.859	.859	.859	.856	.855	.855	.856

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.40x10 FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

LOCAL MACH NO. -- (H) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 146 0	.783	.780	.764	.738	.693	.594	.531	.593	.799	.932	.993	1.028	1.042
.641 208 0	.801	.769	.741	.742	.727	.759	.856	.911	.957	.991	1.013	1.033	1.040
.703 160 0	.767	.744	.710	.736	.801	.846	.858	.855	.855	.861	.885	.913	.938
.839 162 0	.784	.675	.642	.743	.811	.831	.843	.848	.850	.853	.859	.865	.868
.966 176 1	.670	.558	.643	.786	.828	.832	.845	.852	.851	.850	.852	.852	.849
1.047 176 1	.892	.471	.594	.717	.788	.826	.827	.829	.835	.845	.855	.857	.858
1.170 162 0	.855	.531	.564	.698	.795	.824	.824	.827	.831	.838	.843	.842	.843
1.297 160 0	.838	.606	.551	.705	.818	.822	.821	.822	.828	.832	.836	.837	.839
1.439 146 0	.777	.763	.703	.767	.811	.811	.816	.819	.822	.826	.830	.832	.833

LOCAL FLOW FIELD DATA

MACH = .798 RE = 4.37X10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THEYA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 124 0 7.133	6.840	7.640	11.163	15.792	19.849	17.525	30.266	30.300	30.789	32.859	33.549	33.073	
.395 128 1 20.609	21.569	19.066	19.225	16.414	14.069	19.893	34.030	33.971	34.291	33.643	33.159	32.964	
.438 124 0 24.897	24.421	15.240	9.133	25.426	37.468	36.798	34.958	34.463	34.140	33.783	33.717	33.089	
.495 128 1 19.947	21.746	14.896	26.043	34.300	35.505	35.037	34.064	33.163	31.880	30.543	29.597	28.877	
.566 152 0 15.822	16.648	19.205	28.670	32.538	31.865	31.666	31.772	32.085	31.950	31.770	30.975	30.061	
.703 154 0 4.140	11.097	22.069	28.579	31.290	32.012	32.056	31.782	31.495	31.040	30.781	29.785	28.629	
.839 168 0 14.202	17.261	23.033	26.006	27.548	29.042	30.274	29.903	29.543	29.349	29.305	28.519	27.636	
.966 170 0 18.511	19.215	22.598	25.187	26.447	27.537	28.963	28.619	28.215	28.235	28.267	27.359	26.489	
1.047 170 0 20.752	21.164	22.829	24.719	26.227	27.500	28.296	28.520	28.517	28.424	27.899	27.312	26.867	
1.170 168 0 22.404	22.598	23.479	24.414	25.673	26.494	27.273	27.785	27.806	27.717	27.347	26.686	26.543	
1.297 154 0 23.420	23.461	24.055	24.658	25.783	26.735	27.290	27.644	27.652	27.360	26.943	26.541	26.038	
1.439 152 0 24.151	23.990	24.322	24.855	25.944	26.727	27.123	27.194	27.272	27.092	26.850	26.608	26.249	

LOCAL FLOW FIELD DATA

*6 -1

MACH = .802 RE = 4.36x10 FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 144 1 5.374	11.639	20.847	25.539	23.928	19.646	19.248	29.467	35.980	39.046	39.101	39.503	41.273	
.438 140 0 6.902	11.935	24.877	30.271	29.212	26.063	32.333	38.989	40.393	40.061	39.851	40.537	40.865	
.495 144 1 10.768	16.119	20.124	35.893	33.265	38.718	42.302	40.528	39.178	37.902	36.764	35.662	34.636	
.566 150 0 18.902	16.370	9.903	27.021	33.299	39.073	41.059	38.394	36.871	36.224	35.923	35.678	35.312	
.703 156 0 7.319	10.140	21.265	31.534	37.076	37.975	36.873	35.323	34.148	33.556	33.209	32.697	32.236	
.839 166 0 14.316	18.478	24.414	28.588	30.869	32.653	33.028	32.868	32.752	32.280	31.803	30.933	29.970	
.966 172 0 17.330	19.619	23.711	26.388	27.966	29.392	30.257	30.722	30.139	29.615	29.328	28.974	28.219	
1.047 172 0 20.397	21.248	23.447	26.114	28.225	29.199	29.786	30.166	30.096	29.384	28.875	28.235	27.208	
1.170 166 0 21.164	22.557	23.725	25.326	27.141	28.336	28.794	28.975	28.728	28.116	27.957	27.385	27.026	
1.297 156 0 22.669	22.948	23.766	25.057	26.471	27.584	28.025	28.215	28.298	28.127	27.557	26.871	26.414	
1.439 150 0 23.325	23.597	24.174	25.011	26.244	27.161	27.615	27.668	27.724	27.536	27.338	26.856	26.403	

LOCAL FLOW FIELD DATA

MACH = .803 RE = 4.41X10 FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

LOCAL ANGLE OF ATTACK		-- (ALPHA) -- DEG.												
THETA		180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D	RUN NO.													
.566	148 0	9.679	11.244	17.911	35.419	17.528	18.171	17.922	20.089	25.354	28.752	32.444	35.761	36.088
.641	206 0	9.424	10.367	15.631	22.142	12.885	7.471	8.590	13.799	19.381	24.151	27.426	29.235	30.060
.703	158 1	13.996	10.376	12.382	26.633	21.187	16.741	20.697	22.375	22.522	24.916	26.738	28.686	30.224
.839	164 0	10.750	9.324	12.971	24.824	29.886	28.460	27.569	28.541	25.872	26.221	27.090	27.482	27.995
.966	174 0	2.586	7.064	17.825	26.728	30.267	29.704	28.547	26.757	25.998	26.401	26.875	26.601	26.320
1.047	174 0	7.640	13.927	21.327	27.432	29.008	29.174	28.113	27.302	27.111	26.906	26.876	26.916	26.824
1.170	164 0	13.892	16.987	20.943	24.927	27.173	27.581	27.348	27.193	26.965	26.767	26.674	26.482	26.312
1.297	158 1	17.261	18.745	21.348	23.884	25.875	26.647	26.830	26.817	26.662	26.582	26.062	25.928	25.683
1.439	148 0	19.693	19.464	21.289	23.226	24.896	25.874	26.230	26.557	26.641	26.599	26.511	26.268	25.713

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.40x10 FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 146 0 5.279	5.886	7.558	8.061	9.801	9.597	15.363	26.603	30.215	31.367	34.255	36.378	37.824	
.641 208 0 8.553	7.164	3.019	6.727	15.368	25.311	28.972	29.224	29.875	30.291	30.820	31.775	32.177	
.703 160 0 10.659	7.697	3.068	13.734	21.136	26.122	29.240	30.218	30.788	31.285	31.603	32.150	32.735	
.839 162 0 11.495	5.688	10.764	21.345	24.594	26.375	27.860	28.778	29.514	30.099	30.312	30.656	31.130	
.966 176 1 8.702	10.296	24.249	26.195	26.909	27.961	27.829	27.921	28.606	29.237	29.005	28.538	28.913	
1.047 176 1 9.117	12.904	25.934	29.066	27.362	26.224	26.836	27.258	27.332	27.632	27.968	28.165	28.249	
1.170 162 0 2.245	7.216	28.861	29.099	26.954	26.383	26.950	27.321	27.584	27.562	27.532	27.658	27.654	
1.297 160 0 3.659	10.613	24.933	26.329	25.523	25.949	26.633	27.099	27.213	27.126	27.247	27.214	27.058	
1.439 146 0 11.053	13.419	21.043	25.325	26.211	26.460	26.612	26.853	27.001	27.077	27.056	26.935	26.906	

LOCAL FLOW FIELD DATA

MACH = .798 RE = 4.37x10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 124 0	-180.0	162.8	-138.3	-121.1	-95.3	-64.0	-20.6	61.2	74.1	75.5	78.9	81.9	82.3
.395 128 1	180.0	-136.9	-105.6	-56.1	-22.6	-1.4	34.3	65.2	66.6	67.0	70.3	75.3	80.9
.438 124 0	-180.0	-162.8	-135.6	-44.0	41.8	48.7	46.8	49.7	56.7	62.7	68.1	73.5	78.8
.495 128 1	180.0	177.9	129.0	46.4	35.0	40.8	44.1	46.6	51.3	57.7	64.1	69.3	75.3
.566 152 0	-180.0	151.2	99.5	63.3	50.4	49.1	52.4	56.9	61.0	65.6	71.7	77.5	83.0
.703 154 0	.0	61.5	61.8	54.2	49.1	48.0	50.2	54.1	58.9	63.9	69.6	75.8	82.2
.839 168 0	.0	25.3	40.4	44.1	44.9	47.2	50.8	54.5	59.1	64.2	70.1	76.3	82.8
.966 170 0	.0	10.8	26.8	35.0	39.8	44.1	49.1	53.3	58.5	64.1	70.1	76.5	83.2
1.047 170 0	.0	18.9	27.2	34.8	40.8	45.5	50.1	55.6	60.9	65.9	72.2	79.2	85.4
1.170 168 0	.0	16.3	23.6	31.8	38.1	43.9	48.9	54.2	59.9	65.4	71.6	79.0	85.2
1.297 154 0	.0	15.1	22.0	30.1	36.5	42.5	47.9	53.7	59.5	65.5	72.0	79.3	85.4
1.439 152 0	.0	15.2	21.0	28.9	35.4	41.4	46.9	53.1	59.2	65.4	71.9	79.0	84.8

LOCAL FLOW FIELD DATA

MACH = .802 RE = 4.36×10^6 ¹⁰ -1 FT ALPHA = 24.580 X/D = 4.1400 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 144 1	180.0	-83.1	-56.3	-37.1	-24.0	-12.8	4.8	42.1	57.1	57.5	61.8	67.8	70.0
.438 140 0	180.0	-97.9	-61.3	-35.0	-24.5	-5.6	13.4	38.2	44.2	44.8	50.6	58.0	63.2
.495 144 1	180.0	-147.9	-46.3	-7.5	3.1	15.6	32.9	37.7	40.3	44.6	48.9	54.0	60.1
.566 150 0	180.0	169.8	82.8	27.7	26.3	27.0	34.1	36.4	42.1	48.7	56.2	62.0	66.9
.703 156 0	-180.0	95.7	53.6	44.8	41.7	37.5	37.6	41.1	46.2	52.2	58.7	64.3	69.7
.839 166 0	.0	22.4	39.9	39.2	39.4	41.3	43.0	45.9	50.0	55.6	61.4	66.5	72.0
.966 172 0	.0	13.9	29.5	34.5	36.8	39.8	42.8	46.6	51.4	56.8	62.6	68.5	75.2
1.047 172 0	.0	20.2	28.2	34.7	39.4	43.4	47.2	51.2	55.6	61.3	66.8	72.9	80.9
1.170 166 0	.0	16.1	24.6	32.0	37.7	42.4	46.7	51.5	56.5	62.4	67.8	73.3	80.6
1.297 156 0	.0	16.2	23.3	30.9	36.7	41.8	46.7	51.8	57.0	62.7	68.4	74.9	81.5
1.439 150 0	.0	15.6	21.9	29.6	35.7	41.2	46.3	52.0	57.9	63.9	69.8	76.4	82.6

LOCAL FLOW FIELD DATA

*8 -1

MACH = .803 RE = 4.41X10 FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.966 148 0	-180.0	-134.8	-117.5	-113.9	134.2	133.4	172.4	175.7	136.5	107.2	100.8	95.9	91.3
.641 206 0	180.0	-129.2	-74.1	-62.4	-55.5	-27.2	6.2	54.7	72.0	78.6	82.4	85.0	86.6
.703 158 1	180.0	-160.6	-81.4	-29.5	-13.4	-7.7	22.5	45.5	60.7	71.6	78.3	82.6	85.5
.839 164 0	-180.0	145.5	75.9	39.5	27.6	36.2	42.9	49.1	58.7	66.9	73.7	79.2	83.8
.966 174 0	.0	70.1	65.2	53.2	44.6	41.8	46.4	53.2	59.7	65.9	72.1	77.8	83.0
1.047 174 0	.0	52.2	52.4	46.6	42.0	43.8	47.8	53.8	60.1	67.2	73.6	79.2	83.5
1.170 164 0	.0	33.4	39.9	42.2	43.0	45.3	49.2	54.5	60.0	66.1	72.5	78.8	84.1
1.297 158 1	.0	24.3	31.8	38.1	41.8	45.4	49.6	55.2	61.1	66.7	72.8	79.5	84.4
1.439 148 0	.0	19.9	27.9	35.2	40.4	44.9	49.5	54.8	60.4	66.1	72.3	78.8	84.2

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.40x10 FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 146 0	180.0	-125.8	-96.8	-102.4	-105.3	-53.6	12.8	62.7	77.8	82.1	84.3	85.8	87.0
.641 208 0	-180.0	-141.8	-54.4	48.0	72.3	70.6	64.7	63.0	67.9	73.2	77.8	82.2	85.4
.703 160 0	180.0	177.9	79.7	54.5	61.7	64.6	63.5	64.6	68.7	73.8	79.1	83.3	86.6
.839 162 0	-180.0	-168.1	25.8	34.6	44.3	52.1	57.5	62.1	67.2	72.5	78.0	83.0	87.1
.966 176 1	-180.0	74.8	44.2	44.3	48.2	52.9	57.2	61.4	66.4	71.3	76.3	81.2	85.7
1.047 176 1	180.0	44.6	30.2	29.9	37.2	44.8	51.2	57.9	64.2	70.8	77.5	82.7	87.4
1.170 162 0	-180.0	26.4	33.3	34.9	40.6	47.1	53.5	59.6	65.4	71.5	77.8	83.0	88.4
1.297 160 0	.0	28.8	33.6	37.6	41.5	47.1	52.4	58.6	65.1	71.4	77.6	82.8	88.2
1.439 146 0	.0	39.1	40.7	39.6	40.8	45.6	51.5	57.7	63.7	69.7	76.1	82.2	87.9

LOCAL FLOW FIELD DATA

MACH = .798 RE = 4.37X10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 124 0	-.046	-.093	-.103	-.138	-.187	-.208	.018	.176	.021	-.093	-.103	-.101	-.072
.395 128 1	-.219	-.174	-.170	-.167	-.120	-.082	.077	.085	.008	.009	-.009	-.003	.019
.438 124 0	-.351	-.285	-.334	-.321	-.231	-.186	-.147	-.123	-.078	-.066	-.056	-.040	-.023
.495 128 1	-.123	-.171	-.288	-.279	-.174	-.121	-.128	-.111	-.094	-.085	-.092	-.084	-.067
.566 152 0	-.008	-.037	-.172	-.189	-.158	-.106	-.068	-.051	-.030	-.018	-.005	-.008	-.006
.703 154 0	.107	.095	.041	-.022	-.056	-.065	-.049	-.029	-.009	.004	.021	.020	.017
.839 168 0	.088	.121	.110	.060	-.001	-.010	.006	-.016	-.022	-.011	.009	.011	.008
.966 170 0	.043	.040	.055	.043	.013	-.004	.023	-.009	-.029	-.018	.007	.002	.000
1.047 170 0	.083	.062	.054	.031	.019	.022	.024	.019	.020	.031	.025	.025	.035
1.170 168 0	.057	.049	.041	.020	.018	.013	.019	.029	.025	.034	.035	.026	.047
1.297 154 0	.036	.026	.027	.014	.017	.024	.026	.029	.031	.028	.023	.019	.028
1.439 152 0	.036	.012	.016	.007	.016	.024	.025	.020	.025	.023	.019	.024	.030

LOCAL FLOW FIELD DATA

MACH = .802 RE = 4.36x10 FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 144 1	.159	.146	.096	.041	.019	.001	.086	.146	.111	.146	.130	.107	.154
.438 140 0	.037	.038	-.071	-.116	-.198	-.200	.006	.037	.007	.007	.021	.074	.106
.495 144 1	-.237	-.287	-.266	-.212	-.241	-.047	-.001	-.086	-.113	-.103	-.069	-.025	.001
.566 150 0	-.236	-.279	-.384	-.424	-.348	-.142	-.103	-.147	-.127	-.070	-.012	.023	.048
.703 156 0	-.112	-.123	-.204	-.273	-.341	-.317	-.256	-.183	-.124	-.077	-.031	.004	.041
.839 166 0	-.027	-.023	-.047	-.123	-.163	-.158	-.149	-.127	-.086	-.049	-.014	.007	.027
.966 172 0	-.074	-.055	-.069	-.099	-.125	-.151	-.151	-.110	-.100	-.084	-.055	-.025	-.009
1.047 172 0	-.014	-.033	-.053	-.066	-.065	-.067	-.068	-.059	-.039	-.029	-.021	-.003	.009
1.170 166 0	-.036	-.046	-.053	-.073	-.064	-.059	-.057	-.054	-.045	-.033	-.022	-.006	.018
1.297 156 0	-.038	-.046	-.059	-.068	-.062	-.048	-.049	-.048	-.038	-.030	-.027	-.020	.006
1.439 150 0	-.032	-.040	-.042	-.052	-.047	-.038	-.037	-.041	-.039	-.035	-.022	-.011	-.001

LOCAL FLOW FIELD DATA

MACH = .803 RE = 4.41x10 FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.966 146 0	-.989	-1.059	-.683	-.618	-.661	-.644	-.546	-.533	-.369	-.819	-1.038	-.809	-.691
.641 206 0	-.773	-.751	-.931	-.677	-.679	-.869	-.754	-.735	-.845	-.790	-.745	-.701	-.659
.703 158 1	-.664	-.736	-.820	-.874	-1.031	-.833	-.457	-.543	-.625	-.611	-.624	-.594	-.543
.839 164 0	-.500	-.546	-.725	-.792	-.627	-.600	-.554	-.456	-.460	-.475	-.480	-.482	-.448
.966 174 0	-.228	-.306	-.459	-.596	-.568	-.482	-.362	-.382	-.411	-.390	-.384	-.400	-.377
1.047 174 0	-.127	-.199	-.276	-.324	-.310	-.265	-.220	-.210	-.212	-.251	-.277	-.263	-.209
1.170 164 0	-.079	-.092	-.128	-.169	-.161	-.159	-.154	-.148	-.154	-.155	-.160	-.158	-.133
1.297 158 1	-.064	-.083	-.091	-.122	-.125	-.130	-.131	-.132	-.140	-.142	-.147	-.144	-.128
1.439 148 0	-.035	-.066	-.067	-.091	-.099	-.102	-.109	-.110	-.113	-.109	-.108	-.107	-.114

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.40x10 FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.966 146 0	-.022	-.032	-.038	-.051	-.108	-.129	-.110	.030	-.114	-.330	-.447	-.511	-.535
.641 208 0	-.083	-.064	-.061	-.053	-.091	-.154	-.229	-.266	-.358	-.435	-.481	-.528	-.547
.703 160 0	-.093	-.070	-.033	-.020	-.064	-.129	-.149	-.138	-.132	-.146	-.207	-.271	-.318
.839 162 0	-.094	-.042	-.035	-.041	-.053	-.065	-.100	-.116	-.123	-.130	-.155	-.169	-.167
.966 176 1	-.069	-.019	-.011	-.038	-.042	-.038	-.092	-.123	-.117	-.104	-.119	-.132	-.116
1.047 176 1	-.144	-.075	.016	.022	-.010	-.041	-.040	-.045	-.062	-.087	-.113	-.115	-.115
1.170 162 0	-.091	-.017	.016	.027	-.017	-.043	-.048	-.056	-.066	-.085	-.101	-.098	-.090
1.297 160 0	-.024	-.042	.007	.015	-.033	-.042	-.040	-.041	-.059	-.078	-.087	-.088	-.094
1.439 146 0	.052	-.027	-.016	-.008	-.007	-.008	-.024	-.035	-.047	-.058	-.068	-.072	-.072

LOCAL FLOW FIELD DATA

MACH = .798 RE = 4.37X10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 124 0	1.000	.988	.986	.990	.982	.939	.879	.880	.969	.994	.995	.998	.998
.395 128 1	1.002	.968	.939	.937	.975	.978	.910	.919	.980	.996	.998	.997	.998
.438 124 0	1.002	.956	.837	.817	.860	.936	.986	.995	1.002	1.003	1.004	1.010	1.007
.495 128 1	1.012	.950	.814	.865	.956	.991	1.005	1.004	.999	.995	.992	.992	.997
.566 152 0	1.009	.973	.912	.912	.977	1.004	1.001	1.002	1.002	1.003	1.006	.999	.994
.703 154 0	.998	.993	.989	.993	.995	.996	.999	.999	1.001	1.002	1.003	.998	.992
.839 168 0	1.000	1.005	1.012	1.011	1.005	1.007	1.012	1.006	1.004	1.004	1.005	1.001	.996
.966 170 0	1.000	.997	1.003	1.007	1.005	1.005	1.013	1.006	1.000	.999	1.002	.998	.994
1.047 170 0	1.006	1.003	1.005	1.007	1.007	1.007	1.008	1.008	1.008	1.008	1.005	1.004	1.006
1.170 168 0	1.006	1.006	1.007	1.008	1.009	1.008	1.009	1.011	1.009	1.009	1.009	1.006	1.008
1.297 154 0	1.003	1.002	1.005	1.004	1.005	1.006	1.007	1.008	1.007	1.006	1.004	1.002	1.004
1.439 152 0	1.006	1.004	1.007	1.006	1.008	1.011	1.010	1.009	1.009	1.007	1.006	1.006	1.005

LOCAL FLOW FIELD DATA

MACH = .802 RE = 4.36x10 FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 144 1	.973	.977	.987	.999	1.002	.982	.913	.865	.924	.985	.991	.983	.993
.438 140 0	.974	.958	.957	.963	.993	.999	.936	.942	.991	1.008	1.010	1.015	1.015
.493 144 1	.974	.899	.802	.872	.974	.961	.984	1.014	1.017	1.014	1.007	.999	.996
.566 150 0	.993	.939	.806	.850	.941	.942	.975	.997	.999	1.002	1.006	1.010	1.013
.703 156 0	.999	.959	.922	.925	.962	.990	.997	.996	.996	.998	1.003	1.005	1.005
.839 166 0	.992	.995	1.002	.995	.992	.994	.995	.997	1.002	1.004	1.005	1.004	1.002
.966 172 0	.995	1.000	1.004	1.003	1.001	.998	.998	1.005	1.002	1.001	1.001	1.004	1.003
1.047 172 0	1.004	1.004	1.004	1.005	1.005	1.006	1.005	1.007	1.007	1.007	1.007	1.006	1.006
1.170 166 0	1.004	1.004	1.005	1.005	1.007	1.008	1.008	1.008	1.008	1.007	1.007	1.006	1.008
1.297 156 0	1.003	1.002	1.002	1.001	1.004	1.005	1.006	1.007	1.006	1.006	1.003	1.001	1.003
1.439 150 0	1.005	1.007	1.006	1.006	1.009	1.009	1.010	1.009	1.007	1.006	1.005	1.005	1.002

LOCAL FLOW FIELD DATA

MACH = .803 RE = 4.41x10 FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 148 0	1.005	.996	.822	.590	.488	.522	.609	.648	.751	1.000	1.083	1.039	1.014
.641 206 0	.986	.963	.932	.748	.576	.857	.952	.970	1.005	1.003	1.005	1.002	.999
.703 158 1	.993	.954	.840	.797	.862	.938	.948	.978	.997	.997	.997	1.001	1.007
.839 164 0	1.003	.957	.922	.931	.955	.978	.997	1.004	.999	.997	.998	.996	.997
.966 174 0	1.001	.992	.964	.976	.997	1.002	1.011	1.003	.996	.998	1.000	.995	.993
1.047 174 0	1.000	1.004	1.004	1.004	1.006	1.008	1.009	1.009	1.007	1.006	1.003	1.003	1.006
1.170 164 0	1.005	1.002	1.004	1.004	1.006	1.006	1.006	1.006	1.005	1.003	1.002	1.002	1.004
1.297 158 1	1.003	1.001	1.002	1.002	1.004	1.003	1.003	1.004	1.002	1.000	.998	1.000	1.002
1.439 148 0	1.009	1.005	1.005	1.006	1.008	1.008	1.006	1.007	1.005	1.005	1.004	1.003	1.001

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.40X10 FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 146 0	.977	.969	.952	.925	.866	.788	.758	.646	.951	.985	.992	.996	.999
.641 208 0	.963	.943	.920	.923	.895	.895	.952	.989	.994	.990	.987	.985	.985
.703 160 0	.933	.921	.907	.936	.976	.989	.993	.995	.997	.996	.992	.992	.996
.839 162 0	.946	.877	.855	.931	.989	1.005	1.002	.999	.998	.999	.993	.992	.995
.966 176 1	.858	.802	.861	.969	1.009	1.015	1.003	.997	.998	1.002	.998	.994	.997
1.047 176 1	1.029	.739	.839	.932	.984	1.008	1.009	1.009	1.007	1.005	1.002	1.002	1.006
1.170 162 0	1.018	.791	.823	.923	.991	1.008	1.007	1.006	1.003	1.002	1.001	1.002	1.005
1.297 160 0	1.032	.826	.811	.921	1.004	1.006	1.006	1.006	1.004	1.002	1.000	1.001	1.001
1.439 146 0	1.005	.957	.909	.969	1.011	1.011	1.008	1.007	1.006	1.004	1.003	1.002	1.004

LOCAL FLOW FIELD DATA

+6 -1

MACH = .798 RE = 4.37X10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/O RUN NO.													
.315 124 0	-.127	-.118	-.103	-.106	-.027	.154	.233	.177	.132	.134	.109	.081	.075
.395 128 1	-.391	-.283	-.090	.186	.269	.247	.236	.199	.216	.218	.187	.138	.085
.438 124 0	-.494	-.433	-.184	.108	.304	.411	.434	.391	.324	.266	.214	.163	.108
.495 128 1	-.366	-.382	-.149	.298	.480	.462	.441	.408	.357	.293	.231	.180	.126
.566 152 0	-.276	-.248	-.053	.215	.361	.365	.332	.296	.262	.221	.167	.111	.061
.703 154 0	.068	.087	.171	.281	.348	.364	.348	.313	.271	.227	.177	.121	.064
.839 168 0	.234	.253	.285	.310	.329	.334	.322	.294	.257	.215	.167	.113	.058
.966 170 0	.311	.316	.335	.344	.342	.335	.318	.290	.251	.208	.161	.107	.053
1.047 170 0	.342	.332	.337	.341	.334	.323	.303	.270	.232	.193	.142	.086	.036
1.170 168 0	.373	.362	.361	.351	.341	.322	.301	.272	.234	.192	.144	.085	.037
1.297 154 0	.392	.380	.375	.360	.349	.330	.308	.273	.234	.189	.139	.082	.035
1.439 152 0	.405	.392	.385	.369	.357	.338	.311	.275	.234	.189	.140	.085	.040

LOCAL FLOW FIELD DATA

MACH = .802 RE = 4.36x10 FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 144 1	-.083	.022	.185	.336	.368	.321	.276	.264	.269	.307	.275	.222	.206
.438 140 0	-.114	-.026	.199	.420	.515	.480	.477	.450	.458	.459	.407	.337	.284
.495 144 1	-.315	-.244	.211	.557	.599	.590	.555	.544	.517	.466	.409	.347	.282
.566 150 0	-.359	-.298	.021	.423	.586	.564	.557	.535	.473	.404	.331	.274	.225
.703 156 0	-.134	-.018	.219	.392	.509	.559	.534	.473	.411	.351	.290	.235	.182
.839 166 0	.248	.295	.325	.391	.425	.435	.426	.400	.363	.310	.256	.205	.153
.966 172 0	.307	.335	.364	.385	.399	.404	.397	.372	.329	.282	.232	.180	.122
1.047 172 0	.353	.347	.362	.376	.379	.368	.351	.327	.291	.241	.193	.140	.072
1.170 166 0	.369	.378	.377	.377	.375	.363	.343	.313	.274	.223	.181	.133	.074
1.297 156 0	.394	.384	.382	.376	.370	.356	.332	.302	.265	.221	.173	.119	.066
1.439 150 0	.405	.396	.390	.379	.371	.353	.329	.294	.254	.208	.161	.108	.058

LOCAL FLOW FIELD DATA

MACH = .803 RE = 4.41X10 FT ALPHA = 24.980 X/D = 4.800 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 148 0	-.250	-.209	-.166	-.173	-.081	-.114	-.219	-.274	-.271	-.198	-.157	-.085	-.018
.641 206 0	-.224	-.152	.104	.187	.095	.151	.197	.184	.145	.112	.083	.057	.039
.703 158 1	-.319	-.225	.040	.489	.494	.388	.384	.332	.244	.172	.119	.080	.051
.839 164 0	-.232	-.164	.070	.432	.560	.490	.430	.358	.277	.213	.157	.106	.062
.966 174 0	.050	.048	.153	.342	.457	.456	.391	.321	.265	.216	.165	.112	.064
1.047 174 0	.141	.163	.253	.368	.417	.400	.354	.301	.253	.198	.145	.096	.056
1.170 164 0	.251	.256	.293	.339	.363	.353	.325	.287	.245	.197	.146	.093	.048
1.297 158 1	.307	.305	.324	.338	.347	.336	.311	.275	.232	.188	.139	.086	.045
1.439 148 0	.346	.325	.333	.339	.339	.327	.304	.273	.235	.192	.144	.091	.047

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.40x10 FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	160.00	172.50	185.00	197.50	210.00	222.50	235.00	247.50	260.00	272.50	285.00	297.50	310.00
R/D RUN NO.													
.566 146 0	-.091	-.059	-.015	-.028	-.040	.076	.178	.157	.106	.082	.068	.033	.041
.641 208 0	-.149	-.095	.029	.073	.074	.136	.220	.248	.219	.175	.132	.089	.053
.703 160 0	-.179	-.126	.009	.129	.171	.199	.233	.229	.198	.155	.108	.070	.037
.839 162 0	-.196	-.083	.138	.281	.302	.283	.264	.238	.202	.160	.112	.067	.028
.966 176 1	-.129	.034	.241	.311	.311	.293	.265	.237	.203	.165	.121	.078	.038
1.047 176 1	-.175	.098	.288	.381	.361	.323	.292	.251	.207	.160	.108	.064	.023
1.170 162 0	-.042	.077	.294	.354	.344	.312	.278	.240	.200	.153	.103	.060	.014
1.297 160 0	.067	.126	.250	.314	.329	.306	.280	.243	.199	.152	.102	.059	.015
1.439 146 0	.188	.173	.243	.319	.339	.317	.285	.248	.207	.163	.113	.064	.017

LOCAL FLOW FIELD DATA

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MACH = .798 RE = 4.37X10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 124 0	-.000	.036	-.092	-.175	-.291	-.317	-.087	.322	.462	.515	.557	.573	.559
.395 128 1	.000	-.265	-.320	-.277	-.112	-.006	.161	.432	.499	.514	.523	.528	.531
.438 124 0	-.000	-.134	-.180	-.104	.272	.467	.462	.462	.492	.516	.532	.548	.546
.495 128 1	.000	.014	.184	.314	.336	.399	.426	.431	.447	.463	.474	.477	.481
.566 152 0	-.000	.136	.320	.426	.437	.422	.430	.453	.473	.488	.504	.504	.495
.703 154 0	.000	.160	.320	.389	.401	.405	.417	.432	.450	.463	.477	.476	.467
.839 168 0	.000	.120	.243	.300	.329	.361	.395	.412	.430	.446	.461	.462	.456
.966 170 0	-.000	.060	.169	.241	.285	.324	.367	.388	.409	.429	.445	.445	.440
1.047 170 0	.000	.114	.174	.237	.288	.328	.363	.394	.417	.432	.442	.447	.445
1.170 168 0	.000	.106	.157	.217	.268	.310	.345	.378	.403	.420	.433	.438	.439
1.297 154 0	.000	.102	.151	.209	.258	.302	.338	.372	.397	.415	.428	.436	.433
1.439 152 0	.000	.106	.147	.204	.253	.297	.333	.366	.393	.413	.428	.437	.436

LOCAL FLOW FIELD DATA

MACH = .802 RE = 4.36x10⁶ FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 144 1	.000	-.180	-.277	-.254	-.164	-.073	.023	.238	.416	.483	.513	.545	.566
.438 140 0	.000	-.191	-.364	-.294	-.133	-.047	.114	.354	.445	.456	.495	.540	.563
.495 144 1	.000	-.153	-.220	-.073	.032	.164	.359	.420	.438	.459	.470	.477	.490
.566 150 0	.000	.055	.165	.222	.171	.288	.377	.394	.427	.460	.493	.515	.527
.703 156 0	-.000	.178	.296	.389	.453	.429	.411	.413	.428	.453	.477	.488	.493
.839 166 0	-.000	.121	.272	.319	.349	.382	.397	.413	.433	.453	.468	.472	.469
.966 172 0	.000	.083	.206	.265	.298	.337	.367	.393	.413	.431	.447	.458	.461
1.047 172 0	.000	.128	.194	.260	.312	.349	.379	.406	.425	.440	.452	.456	.453
1.170 166 0	.000	.110	.173	.236	.290	.332	.363	.392	.413	.428	.442	.445	.448
1.297 156 0	.000	.112	.164	.225	.276	.318	.352	.383	.408	.428	.437	.441	.440
1.439 150 0	.000	.110	.157	.216	.267	.310	.345	.377	.405	.425	.438	.444	.442

LOCAL FLOW FIELD DATA

MACH = .803 RE = 4.41x10 FT ALPHA = 24.560 X/D = 4.600 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.966 148 0	-.000	-.210	-.319	-.390	.083	.121	.029	.021	.258	.640	.822	.826	.793
.641 206 0	.000	-.186	-.365	-.358	-.139	-.077	.022	.260	.447	.556	.623	.653	.660
.703 158 1	.000	-.079	-.269	-.277	-.118	-.052	.159	.338	.435	.517	.573	.614	.637
.839 164 0	-.000	.113	.281	.355	.292	.359	.399	.414	.456	.499	.539	.558	.567
.966 174 0	-.000	.132	.331	.457	.451	.409	.411	.428	.453	.482	.511	.521	.518
1.047 174 0	.000	.210	.328	.389	.375	.384	.390	.411	.439	.471	.494	.504	.497
1.170 164 0	.000	.168	.245	.308	.338	.357	.376	.402	.425	.445	.463	.472	.471
1.297 158 1	.000	.138	.201	.266	.310	.341	.368	.396	.420	.437	.449	.460	.459
1.439 148 0	.000	.118	.176	.239	.289	.326	.356	.388	.414	.433	.450	.459	.456

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.40X10⁶ FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (V_{THETA}/V_{INF})

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 146 0	.000	-.081	-.126	-.128	-.145	-.103	.040	.304	.493	.592	.678	.737	.771
.641 208 0	-.000	-.075	-.040	.081	.232	.385	.466	.488	.540	.581	.613	.649	.665
.703 160 0	.000	.005	.047	.180	.319	.419	.466	.483	.506	.532	.563	.595	.622
.839 162 0	-.000	-.018	.067	.194	.295	.364	.415	.450	.481	.509	.528	.544	.557
.966 176 1	-.000	.124	.235	.303	.348	.387	.411	.435	.463	.488	.498	.500	.508
1.047 176 1	.000	.096	.167	.220	.274	.321	.362	.400	.429	.459	.485	.496	.502
1.170 162 0	-.000	.038	.193	.248	.294	.335	.376	.409	.436	.458	.475	.484	.487
1.297 160 0	.000	.069	.166	.242	.292	.329	.365	.399	.429	.450	.467	.474	.476
1.439 146 0	.000	.141	.210	.264	.293	.323	.358	.391	.419	.441	.458	.466	.471

LOCAL FLOW FIELD DATA

MACH = .796 RE = 4.37x10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

(VC / VIN * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 124 0	.305	.296	.331	.492	.702	.848	.598	.883	1.155	1.280	1.366	1.392	1.396
.395 128 1	.939	.931	.799	.802	.701	.594	.686	1.143	1.308	1.343	1.335	1.313	1.292
.438 124 0	1.187	1.090	.619	.360	.979	1.496	1.524	1.455	1.416	1.397	1.379	1.375	1.338
.495 128 1	.880	.919	.568	1.040	1.409	1.467	1.474	1.426	1.375	1.317	1.267	1.227	1.195
.566 152 0	.665	.680	.779	1.147	1.363	1.342	1.306	1.300	1.300	1.289	1.276	1.241	1.199
.703 154 0	.164	.437	.873	1.153	1.277	1.310	1.305	1.283	1.263	1.240	1.222	1.180	1.132
.839 168 0	.563	.674	.901	1.036	1.119	1.183	1.225	1.216	1.204	1.190	1.178	1.143	1.106
.966 170 0	.747	.773	.901	1.009	1.071	1.120	1.169	1.165	1.153	1.147	1.138	1.101	1.065
1.047 170 0	.822	.844	.912	.998	1.060	1.107	1.136	1.148	1.147	1.137	1.117	1.094	1.074
1.170 168 0	.897	.908	.946	.992	1.043	1.075	1.102	1.118	1.119	1.110	1.096	1.073	1.058
1.297 154 0	.942	.947	.972	1.000	1.043	1.076	1.096	1.109	1.107	1.096	1.081	1.067	1.045
1.439 152 0	.973	.976	.990	1.014	1.053	1.082	1.095	1.099	1.099	1.091	1.083	1.071	1.053

LOCAL FLOW FIELD DATA

MACH = .802 RE = 4.36X10⁶ FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

(VC / VINP * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 144 1	.199	.435	.801	1.014	.968	.792	.666	.855	1.191	1.375	1.400	1.415	1.448
.438 140 0	.275	.462	.998	1.233	1.279	1.159	1.180	1.376	1.536	1.555	1.541	1.531	1.517
.495 144 1	.757	.691	.733	1.351	1.442	1.472	1.588	1.652	1.630	1.573	1.499	1.418	1.360
.566 150 0	.864	.729	.400	1.148	1.469	1.523	1.616	1.597	1.532	1.473	1.428	1.402	1.377
.703 156 0	.323	.430	.885	1.327	1.639	1.694	1.620	1.509	1.427	1.377	1.342	1.303	1.263
.839 166 0	.597	.767	1.019	1.214	1.322	1.390	1.401	1.383	1.358	1.321	1.282	1.236	1.187
.966 172 0	.739	.829	1.004	1.124	1.198	1.266	1.299	1.301	1.270	1.238	1.211	1.184	1.145
1.047 172 0	.848	.890	.986	1.099	1.180	1.219	1.241	1.253	1.239	1.206	1.182	1.147	1.102
1.170 166 0	.887	.947	.998	1.070	1.139	1.184	1.201	1.206	1.192	1.161	1.148	1.116	1.093
1.297 156 0	.947	.961	.999	1.054	1.109	1.146	1.164	1.172	1.169	1.157	1.131	1.098	1.070
1.439 150 0	.973	.989	1.011	1.049	1.098	1.130	1.146	1.149	1.149	1.138	1.122	1.097	1.073

LOCAL FLOW FIELD DATA

MACH = .803 RE = 4.41x10⁴ ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

(VC / VINF * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 148 0	.601	.713	.864	1.025	.280	.399	.532	.660	.899	1.609	2.011	1.995	1.907
.641 206 0	.538	.579	.912	.971	.404	.407	.477	.765	1.129	1.364	1.512	1.576	1.589
.703 158 1	.766	.573	.653	1.352	1.222	.942	.998	1.140	1.198	1.311	1.407	1.488	1.536
.839 164 0	.559	.479	.696	1.344	1.520	1.459	1.410	1.316	1.283	1.305	1.349	1.366	1.372
.966 174 0	.121	.338	.877	1.373	1.543	1.473	1.363	1.287	1.261	1.270	1.290	1.282	1.255
1.047 174 0	.340	.638	.996	1.287	1.349	1.333	1.265	1.226	1.218	1.228	1.238	1.232	1.202
1.170 164 0	.603	.736	.917	1.101	1.192	1.208	1.195	1.186	1.179	1.169	1.166	1.158	1.139
1.297 158 1	.738	.805	.916	1.034	1.119	1.151	1.159	1.159	1.155	1.143	1.131	1.126	1.110
1.439 148 0	.832	.832	.907	.997	1.070	1.110	1.126	1.141	1.143	1.139	1.135	1.124	1.103

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.40x10 FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

(VC / VINP * SIN ALPHAINP)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.966 146 0	.218	.242	.304	.315	.362	.307	.438	.822	1.213	1.436	1.638	1.776	1.857
.641 208 0	.358	.290	.118	.263	.585	.981	1.238	1.315	1.400	1.459	1.507	1.575	1.604
.703 160 0	.430	.303	.116	.532	.871	1.114	1.252	1.286	1.307	1.333	1.379	1.439	1.497
.839 162 0	.472	.205	.369	.821	1.015	1.108	1.182	1.223	1.254	1.282	1.298	1.318	1.340
.966 176 1	.310	.308	.809	1.044	1.121	1.167	1.177	1.191	1.216	1.237	1.232	1.216	1.226
1.047 176 1	.420	.330	.801	1.058	1.091	1.093	1.118	1.136	1.146	1.169	1.193	1.202	1.209
1.170 162 0	.100	.208	.846	1.039	1.088	1.100	1.123	1.141	1.154	1.161	1.168	1.173	1.171
1.297 160 0	.161	.345	.722	.952	1.058	1.081	1.106	1.124	1.137	1.141	1.148	1.149	1.146
1.439 146 0	.452	.537	.772	.995	1.079	1.088	1.099	1.113	1.124	1.130	1.134	1.130	1.132

LOCAL FLOW FIELD DATA

MACH = .798 RE = 4.37X10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 124 0	1.014	1.026	1.027	1.038	1.033	.977	.787	.629	.822	.894	.879	.873	.866
.395 128 1	1.039	.979	.961	.956	.990	.986	.789	.704	.807	.819	.834	.836	.829
.438 124 0	1.064	.998	.945	.933	.857	.812	.847	.866	.858	.857	.858	.857	.854
.495 128 1	1.008	.958	.888	.886	.859	.855	.874	.877	.875	.881	.893	.898	.902
.566 152 0	.975	.946	.930	.873	.889	.898	.881	.873	.862	.859	.857	.860	.862
.703 154 0	.940	.927	.896	.881	.874	.872	.867	.862	.857	.857	.853	.857	.863
.839 168 0	.926	.902	.882	.883	.892	.886	.873	.880	.883	.880	.873	.875	.878
.966 170 0	.928	.922	.901	.892	.895	.894	.878	.888	.894	.888	.880	.885	.889
1.047 170 0	.903	.907	.901	.901	.895	.885	.878	.879	.878	.874	.878	.881	.882
1.170 168 0	.905	.907	.906	.909	.902	.897	.889	.883	.883	.879	.881	.888	.881
1.297 154 0	.904	.908	.906	.906	.898	.889	.884	.881	.879	.881	.885	.888	.890
1.439 152 0	.903	.912	.911	.910	.900	.894	.889	.890	.887	.887	.890	.890	.888

LOCAL FLOW FIELD DATA

MACH = .002 RE = 4.36x10⁶ ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 144 1	.881	.878	.874	.863	.907	.922	.794	.629	.682	.705	.716	.714	.686
.438 140 0	.944	.910	.895	.879	.952	.986	.775	.707	.751	.769	.768	.744	.729
.495 144 1	1.044	.995	.832	.777	.914	.764	.726	.804	.832	.840	.834	.822	.819
.966 150 0	1.050	1.033	.954	.936	.930	.780	.772	.839	.849	.836	.820	.812	.808
.703 156 0	1.046	1.000	.946	.900	.902	.903	.898	.886	.875	.864	.853	.844	.833
.839 166 0	.973	.954	.934	.927	.920	.902	.896	.890	.878	.870	.860	.856	.856
.966 172 0	.985	.968	.951	.943	.938	.935	.926	.911	.910	.906	.897	.889	.888
1.047 172 0	.948	.952	.946	.932	.915	.908	.902	.896	.889	.891	.892	.889	.891
1.170 166 0	.953	.948	.944	.941	.925	.913	.909	.906	.905	.904	.900	.896	.891
1.297 156 0	.943	.944	.944	.938	.927	.913	.910	.909	.903	.900	.901	.901	.896
1.439 150 0	.938	.942	.937	.935	.926	.916	.912	.912	.910	.908	.902	.902	.899

LOCAL FLOW FIELD DATA

MACH = .803 RE = 4.41X10⁺⁶ FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 148 0	1.467	1.491	1.112	.599	.369	.506	.684	.751	.789	1.220	1.316	1.152	1.088
.641 206 0	1.348	1.315	1.356	.993	.735	1.291	1.314	1.295	1.335	1.265	1.212	1.171	1.142
.703 158 1	1.279	1.301	1.238	1.121	1.311	1.303	1.099	1.152	1.202	1.174	1.162	1.131	1.097
.839 164 0	1.224	1.213	1.256	1.209	1.100	1.120	1.123	1.096	1.100	1.102	1.097	1.092	1.074
.966 174 0	1.112	1.133	1.134	1.134	1.100	1.074	1.042	1.062	1.076	1.064	1.059	1.065	1.055
1.047 174 0	1.053	1.070	1.061	1.031	1.012	.993	.985	.988	.989	1.007	1.016	1.010	.989
1.170 164 0	1.014	1.002	.997	.986	.966	.962	.961	.960	.964	.964	.966	.966	.959
1.297 158 1	.989	.987	.975	.971	.959	.954	.953	.954	.957	.959	.962	.963	.960
1.439 148 0	.967	.979	.968	.966	.959	.952	.951	.949	.948	.947	.947	.947	.953

LOCAL FLOW FIELD DATA

MACH = .797 RE = 4.40x10⁶ ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.566 146 0	.981	.975	.955	.925	.871	.755	.663	.683	.866	.980	1.000	1.003	.995
.641 208 0	.990	.958	.934	.929	.886	.863	.930	.978	1.014	1.039	1.051	1.058	1.061
.703 160 0	.951	.932	.899	.906	.937	.945	.930	.919	.912	.912	.932	.953	.969
.839 162 0	.966	.857	.808	.874	.922	.930	.930	.926	.922	.920	.923	.925	.923
.966 176 1	.841	.705	.747	.883	.919	.914	.928	.935	.927	.919	.924	.930	.923
1.047 176 1	1.089	.599	.685	.791	.877	.923	.919	.917	.922	.929	.935	.934	.936
1.170 162 0	1.064	.683	.639	.777	.890	.922	.919	.919	.918	.925	.932	.931	.930
1.297 160 0	1.044	.765	.646	.801	.921	.924	.918	.914	.919	.926	.928	.929	.933
1.439 146 0	.962	.937	.835	.875	.911	.909	.912	.915	.917	.920	.924	.925	.928

LOCAL VORTICITY X 100.

MACH = .798 RE = 4.37X10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

THETA 176.25 166.75 161.25 153.75 146.25 138.75 131.25 123.75 116.25 108.75 101.25 93.75

R/D

.3550	-19.453	-38.062	6.677	40.634	106.584	101.014	45.754	45.638	41.608	16.388	5.276	11.319
.4165	70.660	166.436	207.661	222.323	277.905	244.147	100.750	23.487	16.300	15.606	17.653	17.943
.4665	40.006	209.465	325.371	193.973	36.967	1.200	-6.286	-16.400	-20.912	-21.355	-21.950	-24.511
.5305	25.579	130.261	187.095	114.523	37.998	14.657	12.721	14.639	12.211	11.470	14.118	11.427
.6345	12.166	53.442	67.825	41.735	14.725	6.140	3.358	2.379	1.345	-1.574	-2.596	-2.199
.7710	3.287	10.535	11.417	7.380	4.036	3.060	1.816	.485	.389	-.306	-1.162	-.897
.9025	-2.085	-3.698	-2.975	-.189	.903	.618	-.236	-.976	-.731	-.934	-2.150	-2.279
1.0065	8.967	14.541	6.383	5.550	6.980	5.106	3.656	4.746	4.337	1.644	.381	2.307
1.1085	-1.361	.932	.255	.209	.162	.483	-.479	-.679	-.110	-.991	-1.919	.015
1.2335	-.988	1.114	.396	1.457	1.089	1.616	1.201	.723	.504	-.008	-.861	.705
1.3680	-.405	1.422	.301	1.793	1.564	1.340	.579	.495	.577	.601	.289	1.818

LOCAL VORTICITY X 100.

*8 -1

MACH = .802 RE = 4.36x10 FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

THETA 176.25 168.75 161.25 153.75 146.25 138.75 131.25 123.75 116.25 108.75 101.25 93.75

R/D

.4165	35.405	45.510	30.751	13.534	-8.476	23.405	61.826	67.148	36.560	-3.030	-3.368	15.196
.4665	36.253	106.621	183.269	106.315	73.745	100.187	76.853	31.451	13.035	-1.849	-20.007	-26.276
.5305	59.079	241.845	255.642	117.560	48.304	31.219	10.838	-2.653	-2.397	3.109	12.329	16.340
.6345	40.269	113.721	124.268	95.568	56.071	25.988	8.158	-.473	-2.600	-3.902	-1.335	-.801
.7710	17.423	32.677	31.271	14.974	6.470	3.291	1.296	1.913	.822	-.085	.053	-1.177
.9025	5.463	.673	4.742	3.179	1.632	1.178	.498	-.858	-2.811	-2.822	-1.398	-1.037
1.0065	10.331	12.909	6.553	10.070	11.349	10.158	8.685	6.595	4.578	3.834	1.736	-2.160
1.1085	-.143	.563	1.493	1.664	1.428	1.488	1.021	.220	-1.394	-.067	-.737	-2.329
1.2335	1.269	1.974	1.713	2.051	1.279	.966	.874	.777	.637	1.305	.263	-.860
1.3680	-.405	1.169	.844	1.834	1.621	1.367	.892	.988	.875	1.029	.833	1.330

LOCAL VORTICITY X 100.

MACH = .803 RE = 4.41x10⁶ FT ALPHA = 24.980 X/D = 4.800 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.6035	17.715	32.439	-5.227	-40.059	-66.572	-42.596	31.207	75.953	43.597	-17.758	-24.321	-12.687
.6720	42.668	106.739	93.571	-.053	-1.512	39.105	41.433	9.144	-6.920	-8.513	-4.542	4.741
.7710	36.026	130.390	209.702	114.438	57.466	58.864	24.508	1.214	-1.118	-1.066	-.883	-1.381
.9025	10.539	48.697	83.062	62.247	23.453	3.679	-.905	-1.253	-.880	-1.714	-2.509	-3.361
1.0065	15.907	36.315	27.178	3.649	-7.081	-7.764	-7.222	-3.993	-2.310	-2.044	-2.389	-1.723
1.1085	.204	3.604	4.357	2.178	-.566	-2.062	-1.261	-.729	-2.956	-4.173	-4.278	-2.048
1.2335	-1.219	.802	1.417	1.734	.900	.827	.651	.754	.400	-.715	-1.394	.469
1.3680	-2.153	.875	.928	1.406	.958	.649	.505	.408	.625	1.020	.774	2.105

LOCAL VORTICITY X 100.

MACH = .797 RE = 4.40x10 FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

THETA	176.25	166.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.6035	13.156	38.552	51.963	96.509	175.928	189.815	116.036	44.750	18.217	3.844	-6.849	-10.760
.6720	30.585	69.650	63.423	51.286	49.613	39.761	20.429	2.562	-8.753	-11.340	-10.081	-6.115
.7710	18.420	44.687	39.574	14.954	5.051	5.485	3.263	1.721	1.471	.148	-.142	-.817
.9025	43.763	78.623	55.277	26.113	13.318	8.008	4.329	1.964	1.161	-.689	-2.362	-2.769
1.0065	38.433	27.021	-2.055	-19.012	-18.706	-14.203	-9.465	-7.269	-6.324	-3.520	1.356	3.433
1.1085	28.617	34.584	23.363	8.069	4.281	5.109	4.304	3.783	2.562	.698	1.215	.885
1.2335	17.336	29.113	10.656	4.984	1.209	.860	.027	.196	.104	.007	1.164	.698
1.3680	10.583	26.405	19.523	9.574	2.081	1.122	.439	.056	-.094	-.141	.562	1.042

LOCAL CIRCULATION STRENGTH X 100.

MACH = .798 RE = 4.37x10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.3550	-.092	-.180	.032	.192	.504	.478	.217	.216	.197	.078	.025	.054	1.7200
.4165	.211	.497	.620	.664	.830	.729	.301	.070	.049	.047	.053	.054	4.1218
.4665	.177	.928	1.442	.860	.164	.005	-.028	-.073	-.093	-.095	-.097	-.109	3.0826
.5305	.161	.818	1.175	.719	.239	.092	.080	.092	.077	.072	.089	.072	3.6831
.6345	.176	.774	.983	.605	.213	.089	.049	.034	.019	-.023	-.038	-.032	2.8504
.7710	.057	.184	.200	.129	.071	.053	.032	.008	.007	-.005	-.020	-.016	.6997
.9025	-.040	-.071	-.057	-.004	.017	.012	-.005	-.019	-.014	-.018	-.041	-.044	-.2814
1.0065	.122	.198	.087	.075	.095	.069	.050	.064	.059	.022	.005	.031	.8777
1.1085	-.031	.021	.006	.005	.004	.011	-.011	-.015	-.003	-.023	-.044	.000	-.0792
1.2335	-.026	.029	.010	.038	.028	.042	.031	.019	.013	-.000	-.022	.018	.1814
1.3680	-.013	.046	.010	.038	.051	.043	.019	.016	.019	.019	.009	.059	.3359
RSUM	.703	3.244	4.506	3.341	2.215	1.624	.734	.414	.330	.075	-.082	.088	17.1921

LOCAL CIRCULATION STRENGTH X 100.

*6 -1

MACH = .802 RE = 4.36x10 FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.4165	.106	.136	.092	.040	-.025	.070	.185	.200	.109	-.009	-.010	.045	.9386
.4665	.161	.738	.812	.471	.327	.444	.341	.139	.058	-.008	-.089	-.116	3.2777
.5305	.371	1.518	1.605	.738	.303	.196	.068	-.017	-.015	.020	.077	.103	4.9669
.6345	.583	1.648	1.800	1.385	.812	.377	.118	-.007	-.038	-.057	-.019	-.012	6.5909
.7710	.304	.571	.546	.262	.113	.058	.023	.033	.014	-.001	.001	-.021	1.9036
.9025	.104	.013	.091	.061	.031	.022	.010	-.016	-.054	-.054	-.027	-.020	.1612
1.0065	.140	.175	.089	.137	.154	.138	.118	.090	.062	.052	.024	-.029	1.1500
1.1085	-.003	.013	.034	.038	.032	.034	.023	.005	-.032	-.002	-.017	-.053	.0729
1.2335	.033	.052	.045	.054	.033	.025	.023	.020	.017	.034	.007	-.022	.3198
1.3680	-.013	.038	.027	.059	.052	.044	.029	.032	.028	.033	.027	.043	.4007
RSUM	1.787	4.902	5.141	3.244	1.834	1.408	.936	.480	.150	.008	-.026	-.082	19.7825

LOCAL CIRCULATION STRENGTH X 100.

*6 -1

MACH = .803 RE = 4.41x10 FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

THETA	176.25	166.75	161.25	153.75	146.25	136.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.8035	.134	.245	-.039	-.302	-.502	-.321	.235	.573	.329	-.134	-.183	-.096	-.0627
.8720	.296	.741	.691	-.000	-.010	.272	.288	.063	-.048	-.059	-.032	.033	2.2350
.7710	.665	2.279	3.665	2.000	1.004	1.029	.428	.021	-.020	-.019	-.015	-.024	11.0127
.9025	.201	.930	1.587	1.189	.448	.070	-.017	-.024	-.017	-.033	-.048	-.064	4.2228
1.0065	.216	.493	.369	.050	-.096	-.105	-.098	-.054	-.031	-.028	-.032	-.023	.6593
1.1085	.005	.082	.099	.049	-.013	-.047	-.029	-.017	-.067	-.095	-.097	-.047	-.1757
1.2335	-.032	.021	.037	.045	.024	.022	.017	.020	.010	-.019	-.036	.012	.1208
1.3660	-.070	.028	.030	.046	.031	.021	.016	.013	.027	.033	.025	.068	.2687
RSUM	1.415	4.819	6.439	3.076	.885	.939	.841	.596	.183	-.353	-.419	-.141	18.2809

LOCAL CIRCULATION STRENGTH X 100.

MACH = .797 RE = 4.40x10 FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.6035	.099	.291	.392	.728	1.327	1.432	.875	.338	.137	.029	-.052	-.081	5.5157
.6720	.212	.484	.440	.356	.345	.276	.142	.018	-.061	-.079	-.070	-.042	2.0208
.7710	.322	.781	.692	.261	.088	.096	.057	.030	.026	.003	-.002	-.014	2.3385
.9025	.836	1.502	1.056	.499	.254	.153	.083	.038	.022	-.013	-.045	-.053	4.3313
1.0065	.522	.367	-.028	-.258	-.254	-.193	-.129	-.099	-.086	-.048	.018	.047	-.1401
1.1085	.650	.786	.531	.183	.097	.116	.098	.086	.058	.016	.028	.020	2.6694
1.2335	.453	.760	.278	.130	.032	.022	.001	.005	.003	.000	.030	.018	1.7324
1.3680	.336	.855	.632	.310	.067	.036	.014	.002	-.003	-.005	.018	.034	2.2971
RSUM	3.431	5.825	3.993	2.209	1.956	1.939	1.141	.417	.096	-.097	-.075	-.072	20.7653

SECTION III $M_{\infty}=0.8, \alpha=20.1^{\circ}, Re=7.9 \times 10^6 ft^{-1},$ $X/D = 3.5, 4.1, 4.8, 6.5$

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.94X10 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 115 0	.781	.754	.737	.775	.766	.620	.513	.694	.823	.810	.820	.829	.837
.395 119 0	.834	.728	.622	.666	.732	.703	.796	.786	.788	.795	.801	.805	.796
.438 115 0	.802	.722	.667	.727	.778	.793	.789	.780	.783	.785	.787	.792	.794
.495 119 0	.725	.734	.759	.779	.783	.785	.790	.786	.783	.784	.781	.787	.796
.571 193 0	.726	.723	.746	.765	.770	.773	.773	.773	.776	.778	.780	.777	.773
.711 191 0	.748	.749	.753	.761	.769	.772	.774	.775	.778	.781	.782	.779	.774
.841 213 0	.759	.760	.763	.768	.776	.780	.781	.780	.780	.783	.782	.778	.773
.961 211 0	.770	.770	.770	.773	.777	.782	.783	.781	.780	.780	.782	.780	.775
1.055 211 0	.769	.777	.774	.775	.779	.782	.781	.779	.776	.774	.773	.774	.771
1.221 213 0	.778	.785	.784	.786	.787	.788	.789	.783	.775	.773	.774	.775	.772
1.307 191 0	.790	.790	.788	.787	.789	.791	.792	.789	.783	.776	.777	.780	.776
1.439 193 0	.796	.791	.790	.789	.790	.791	.791	.787	.777	.775	.776	.778	.776

LOCAL FLOW FIELD DATA

MACH = .803 RE = 7.93x10⁶ -1 ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

LOCAL MACH NO. -- (H) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 135 0	.733	.669	.682	.714	.623	.556	.734	.741	.745	.750	.747	.742	.728
.438 131 0	.757	.680	.673	.778	.712	.744	.804	.799	.795	.791	.776	.756	.738
.495 135 0	.786	.700	.722	.775	.781	.810	.812	.804	.805	.799	.781	.753	.742
.571 195 0	.792	.742	.750	.808	.830	.821	.809	.801	.791	.781	.769	.760	.751
.711 189 0	.786	.790	.804	.816	.820	.822	.821	.810	.805	.800	.792	.785	.775
.841 215 0	.802	.803	.809	.818	.823	.825	.823	.818	.810	.803	.799	.794	.784
.961 209 0	.814	.813	.815	.819	.822	.824	.825	.821	.815	.808	.803	.798	.788
1.055 209 0	.804	.811	.815	.821	.823	.822	.818	.811	.805	.800	.793	.785	.781
1.221 215 0	.818	.823	.820	.822	.829	.831	.830	.829	.822	.813	.802	.796	.797
1.307 189 0	.822	.825	.821	.821	.822	.825	.824	.818	.809	.799	.795	.790	.788
1.439 195 0	.824	.824	.822	.824	.827	.829	.826	.819	.809	.799	.792	.790	.790

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.91x10⁶ FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 197 0	1.320	1.200	.687	.316	.570	.683	.485	.483	.699	1.084	1.302	1.264	1.169
.641 203 0	1.129	1.099	1.168	1.075	1.159	1.270	1.280	1.252	1.231	1.199	1.149	1.118	1.103
.711 187 0	1.111	1.024	1.037	1.133	1.114	1.079	1.075	1.072	1.072	1.067	1.061	1.053	1.041
.838 181 0	.942	.980	1.042	1.042	1.014	1.003	1.002	.994	.999	1.009	1.007	1.000	.986
.966 179 0	.909	.919	.922	.930	.937	.941	.947	.942	.943	.952	.951	.946	.936
1.047 179 0	.864	.881	.881	.891	.888	.892	.895	.883	.875	.875	.878	.877	.877
1.173 181 0	.861	.859	.862	.864	.865	.866	.866	.861	.859	.857	.857	.857	.859
1.307 187 0	.852	.849	.850	.850	.852	.856	.857	.853	.850	.848	.847	.847	.846
1.439 197 0	.835	.834	.834	.835	.839	.841	.841	.838	.833	.831	.829	.828	.833

LOCAL FLOW FIELD DATA

MACH = .801 RE = 7.93x10 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 199 0	.643	.627	.609	.609	.596	.580	.693	.823	.878	.914	.958	.997	1.016
.641 201 0	.606	.568	.592	.676	.739	.812	.847	.849	.861	.860	.880	.916	.947
.711 185 0	.619	.576	.611	.721	.799	.823	.831	.839	.846	.852	.856	.859	.860
.838 183 0	.709	.644	.583	.672	.776	.809	.818	.826	.834	.840	.844	.845	.843
.966 177 1	.776	.630	.542	.661	.780	.815	.817	.823	.832	.838	.842	.845	.843
1.047 177 1	.831	.508	.552	.738	.811	.811	.810	.814	.818	.826	.834	.839	.843
1.173 183 0	.619	.640	.645	.785	.806	.802	.803	.806	.811	.817	.824	.828	.830
1.307 185 0	.785	.792	.789	.801	.802	.797	.800	.802	.804	.806	.810	.816	.821
1.439 199 0	.792	.795	.796	.799	.802	.803	.804	.803	.803	.804	.808	.814	.811

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.94x10 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

LOCAL ANGLE OF ATTACK		-- (ALPHA) -- DEG.												
THETA		180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D	RUN NO.													
.315	115 0	9.980	9.883	14.158	14.529	10.488	6.518	20.457	28.628	25.897	28.085	29.436	30.594	31.382
.395	119 0	19.693	19.094	3.768	18.688	22.022	26.964	26.479	26.413	26.716	27.253	27.595	28.198	28.445
.438	115 0	16.660	13.561	12.100	22.967	27.163	26.755	26.299	26.678	26.680	27.066	27.516	27.310	27.014
.495	119 0	.558	9.640	18.515	23.771	25.455	26.125	25.804	25.403	24.967	24.614	24.303	24.255	24.322
.571	193 0	2.883	10.255	19.988	24.481	25.563	25.743	25.842	25.792	25.349	25.099	25.159	25.128	25.366
.711	191 0	16.693	17.695	19.589	21.398	22.921	24.034	24.442	24.547	24.382	23.963	23.847	23.722	23.674
.841	213 0	18.376	19.031	20.369	21.614	22.707	23.419	23.963	24.216	23.993	23.526	23.438	23.171	22.977
.961	211 0	19.613	19.944	20.883	21.786	22.465	22.761	23.023	23.314	23.312	22.926	22.814	22.547	22.342
1.055	211 0	20.899	20.431	20.968	21.660	22.218	22.754	23.264	23.909	24.217	24.337	24.155	23.264	22.579
1.221	213 0	22.012	21.199	21.593	22.116	22.596	22.974	23.287	23.835	24.259	24.056	23.810	23.021	22.559
1.307	191 0	21.071	20.646	20.903	21.274	21.535	21.852	22.096	22.329	22.935	23.551	23.315	22.531	22.099
1.439	193 0	21.224	21.099	21.041	21.218	21.353	21.675	21.894	22.424	23.281	23.411	23.160	22.488	22.106

LOCAL FLOW FIELD DATA

+6 -1

MACH = .803 RE = 7.93x10 FT ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 135 0	4.837	13.773	22.318	21.754	21.003	30.665	29.858	32.192	33.023	33.666	34.465	35.954	36.099
.438 131 0	5.528	7.164	23.377	27.260	32.256	33.421	32.697	32.821	33.152	33.759	34.321	34.842	34.884
.495 135 0	5.975	5.484	25.740	34.175	36.141	34.530	32.741	32.491	32.079	31.565	30.974	30.107	29.416
.571 195 0	.172	12.110	24.647	30.393	31.691	31.141	30.586	30.364	30.548	30.759	30.864	30.277	29.495
.711 189 0	14.222	17.437	22.872	26.050	27.310	27.916	27.624	28.008	28.181	28.165	27.787	27.100	26.580
.841 215 0	19.381	20.829	23.395	25.127	26.022	26.234	26.166	26.453	26.908	26.728	25.859	25.195	24.843
.961 209 0	20.675	21.211	22.881	24.224	24.914	25.243	25.254	25.431	25.483	25.325	24.744	24.125	23.617
1.055 209 0	22.045	21.341	22.338	23.225	23.973	24.576	24.924	25.344	25.567	25.488	25.479	25.166	23.869
1.221 215 0	22.165	21.525	22.125	22.952	22.707	22.887	23.049	23.254	23.693	24.134	24.319	23.997	22.848
1.307 189 0	21.585	21.209	21.380	21.762	22.042	22.500	22.831	23.064	23.478	23.997	24.057	23.593	22.481
1.439 195 0	21.342	20.908	21.175	21.527	21.953	22.341	22.660	23.065	23.693	23.913	24.166	23.777	22.220

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.91x10 FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.371 197 0 7.379	9.269	26.434	22.055	14.049	11.080	22.090	27.454	20.126	20.477	26.771	29.973	30.190	
.641 203 0 4.680	3.994	12.261	10.849	9.051	10.883	15.126	16.840	18.288	19.636	21.151	22.974	24.320	
.711 187 0 5.254	3.069	10.982	20.806	21.894	20.612	19.816	20.181	20.629	21.359	22.271	23.165	24.068	
.838 181 0 9.334	11.342	18.329	22.353	23.050	22.046	21.355	21.463	21.553	21.599	22.110	22.593	22.905	
.966 179 0 12.928	14.108	17.388	19.832	20.748	21.202	21.319	21.783	21.937	21.861	22.101	22.163	22.120	
1.047 179 0 14.246	16.270	18.128	20.004	21.202	21.417	21.787	22.242	22.883	23.023	22.798	22.920	22.340	
1.173 181 0 16.696	16.772	18.204	19.681	20.499	21.121	21.821	22.551	22.919	23.254	23.345	22.958	22.426	
1.307 187 0 17.725	17.928	18.589	19.578	20.277	20.832	21.406	22.133	22.768	23.216	23.213	22.592	22.196	
1.439 197 0 18.856	18.576	19.232	20.258	20.847	21.418	21.976	22.682	23.179	23.431	23.700	23.340	21.667	

LOCAL FLOW FIELD DATA

MACH = .801 RE = 7.93x10⁺⁶ FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 33

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 199 0 4.805	3.981	2.702	2.405	7.467	17.653	25.134	26.280	27.449	29.305	31.376	33.033	33.919	
.641 201 0 6.589	2.993	7.907	14.625	19.075	21.362	23.308	24.315	24.811	25.184	25.806	26.516	27.145	
.711 185 0 6.289	5.058	15.321	19.768	21.052	22.464	23.791	24.716	25.479	26.114	27.091	28.241	29.119	
.838 183 0 3.311	.159	11.267	19.330	20.508	21.459	22.669	23.324	24.010	24.629	25.223	25.987	26.790	
.966 177 1 .207	5.233	17.546	21.435	20.814	21.347	22.484	23.001	23.321	23.783	24.087	24.359	24.897	
1.047 177 1 1.458	9.436	21.202	20.074	20.146	21.592	23.009	23.822	24.546	24.737	24.504	24.364	24.143	
1.173 183 0 8.006	9.623	17.739	19.393	19.903	21.315	22.490	23.368	24.067	24.407	24.299	23.948	23.549	
1.307 185 0 12.501	15.222	17.710	19.095	20.083	21.559	22.330	23.000	23.602	24.174	24.121	23.455	23.202	
1.439 199 0 15.339	16.373	18.350	19.674	20.496	21.362	22.066	22.780	23.399	23.950	23.820	22.984	22.653	

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.94x10 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 115 0	180.0	-119.2	-71.4	-42.4	-36.5	-18.4	55.3	71.6	76.1	77.7	82.0	85.4	87.6
.395 119 0	180.0	-150.4	-123.5	15.2	35.7	52.2	59.6	64.2	68.4	74.0	79.8	84.5	88.2
.438 115 0	180.0	168.8	86.2	43.0	41.1	45.5	50.6	57.8	64.2	70.3	76.0	81.3	86.2
.495 119 0	.0	73.4	56.8	47.8	44.4	44.7	48.1	52.2	58.2	64.0	69.8	75.5	80.9
.571 193 0	.0	59.7	55.5	48.4	46.0	47.7	51.6	56.3	61.4	66.9	73.0	78.7	84.2
.711 191 0	.0	15.7	26.5	33.6	39.5	44.6	49.4	54.7	60.0	65.3	71.2	76.8	82.8
.841 213 0	.0	13.0	22.1	29.7	36.6	42.4	47.8	53.2	58.9	64.7	70.8	77.0	83.2
.961 211 0	.0	10.3	19.1	26.4	33.5	39.8	45.6	51.3	57.5	63.5	69.8	76.2	82.9
1.055 211 0	.0	16.2	22.2	30.0	36.8	43.0	48.6	54.0	59.4	65.5	71.1	76.7	83.4
1.221 213 0	.0	15.3	20.6	28.1	34.8	41.6	47.4	52.7	58.0	63.8	69.3	75.2	82.4
1.307 191 0	.0	12.6	18.5	26.3	33.5	40.5	46.3	52.0	58.3	65.4	71.1	77.0	83.4
1.439 193 0	.0	12.1	18.0	25.9	33.0	40.0	45.8	52.2	59.1	65.1	70.8	76.8	83.7

LOCAL FLOW FIELD DATA

MACH = .803 RE = 7.93X10 FT ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

CROSSFLOW DIRECTION (THETA) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 135 0	180.0	-64.6	-31.1	-14.5	5.5	37.7	48.2	53.5	59.2	64.0	66.7	68.6	68.9
.438 131 0	180.0	-55.7	-16.0	.3	15.5	30.8	36.4	40.3	46.4	51.4	55.9	59.7	62.7
.495 135 0	-180.0	45.4	21.3	20.8	26.2	32.0	35.5	38.5	43.8	48.0	51.0	54.0	59.0
.571 195 0	-180.0	51.4	34.5	32.3	31.7	32.9	37.4	42.5	47.6	53.0	57.9	62.1	66.4
.711 189 0	.0	24.9	33.2	32.1	32.7	36.1	39.9	44.9	49.7	55.0	59.9	64.5	69.6
.841 215 0	.0	15.0	24.7	29.7	33.0	36.6	41.0	45.8	51.4	56.7	61.4	66.3	72.1
.961 209 0	.0	10.5	20.0	26.8	31.9	36.4	41.3	46.2	51.5	56.9	62.3	68.1	74.1
1.055 209 0	.0	17.2	23.0	29.7	35.2	40.7	45.4	49.8	55.0	60.2	65.1	70.5	76.1
1.221 215 0	.0	15.5	20.3	27.3	34.2	40.3	45.7	50.9	56.5	62.4	67.7	73.6	79.3
1.307 189 0	.0	12.8	18.7	26.3	33.1	39.2	44.9	50.1	55.5	62.0	67.8	73.4	79.1
1.439 195 0	.0	12.7	18.3	25.4	32.0	38.6	44.5	50.2	56.1	61.7	67.5	73.2	78.9

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.91X10⁶ FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 197 0	-180.0	-128.6	-115.1	179.2	142.9	-172.3	177.7	158.6	137.8	115.2	104.2	99.6	96.7
.641 203 0	180.0	-93.2	-52.6	-46.3	-15.6	36.5	60.6	66.1	71.8	78.3	83.3	86.1	87.8
.711 187 0	-180.0	137.1	20.5	13.2	24.4	35.7	44.1	54.4	62.7	69.8	76.2	81.6	85.6
.838 181 0	.0	47.4	47.2	39.5	36.2	38.8	45.6	53.8	60.7	66.7	72.9	78.5	83.2
.966 179 0	.0	21.4	31.7	34.0	37.0	41.9	47.5	53.5	59.8	65.5	70.9	76.6	82.0
1.047 179 0	.0	21.0	28.4	35.3	40.0	44.0	48.5	54.3	61.0	66.1	70.9	77.0	82.2
1.173 181 0	.0	19.8	26.3	33.0	39.0	44.5	49.7	55.9	61.5	67.0	72.2	77.2	82.9
1.307 187 0	.0	16.5	23.4	31.0	37.7	43.8	49.1	54.8	60.6	66.4	71.6	76.4	82.0
1.439 197 0	.0	15.7	22.4	30.3	37.3	43.6	49.3	54.8	59.9	65.4	70.8	76.0	80.7

LOCAL FLOW FIELD DATA

MACH = .801 RE = 7.93X10 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 199 0	180.0	-162.6	-136.1	119.5	94.0	76.6	75.4	78.9	82.0	84.4	86.0	87.1	88.1
.641 201 0	180.0	-169.1	70.8	67.9	69.3	69.2	66.7	67.3	71.7	76.3	80.5	84.0	87.0
.711 185 0	-180.0	107.5	63.4	60.1	60.6	62.5	64.9	68.2	72.7	77.3	81.6	84.9	87.6
.838 183 0	-180.0	126.4	27.8	40.8	46.8	52.3	58.4	63.3	68.7	74.1	79.3	83.6	87.0
.966 177 1	.0	4.2	29.2	41.3	44.4	48.2	54.9	60.7	66.2	71.6	77.3	82.3	86.4
1.047 177 1	.0	10.6	39.7	46.4	48.4	54.2	60.3	65.2	69.7	74.3	79.0	84.1	89.2
1.173 183 0	.0	33.9	39.8	42.0	46.4	53.2	58.7	63.7	68.8	74.1	79.0	83.3	88.6
1.307 185 0	.0	29.3	32.2	36.7	43.5	50.8	56.0	60.7	66.0	71.7	76.7	81.4	87.1
1.439 199 0	.0	23.7	28.9	34.7	41.4	47.6	52.9	58.5	64.2	69.8	74.8	79.7	85.4

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.94x10 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 115 0	.031	.042	.064	.030	.038	.135	.228	.116	-.063	-.027	-.049	-.067	-.083
.395 119 0	-.059	.004	-.005	-.007	.055	.113	.006	.035	.032	.018	.003	-.000	.014
.438 115 0	.014	.037	-.011	-.039	-.017	-.004	.019	.042	.035	.031	.027	.009	-.002
.495 119 0	.168	.112	.040	.026	.041	.044	.032	.035	.036	.028	.031	.020	.009
.571 193 0	.157	.144	.097	.077	.071	.072	.072	.069	.053	.040	.036	.035	.053
.711 191 0	.114	.116	.111	.091	.073	.068	.067	.066	.051	.038	.036	.039	.052
.841 213 0	.095	.094	.092	.078	.059	.054	.052	.057	.053	.037	.041	.047	.055
.961 211 0	.069	.070	.076	.070	.057	.047	.046	.051	.047	.040	.039	.043	.052
1.055 211 0	.068	.054	.060	.062	.061	.064	.069	.078	.086	.095	.097	.080	.076
1.221 213 0	.054	.032	.041	.040	.046	.048	.052	.069	.083	.090	.088	.074	.076
1.307 191 0	.023	.018	.024	.028	.026	.029	.028	.036	.057	.081	.076	.058	.062
1.439 193 0	.009	.008	.013	.018	.021	.024	.027	.045	.071	.079	.073	.062	.058

LOCAL FLOW FIELD DATA

MACH = .803 RE = 7.93x10 FT ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 135 0	.123	.184	.150	.119	.182	.224	.117	.128	.100	.077	.082	.090	.123
.438 131 0	.034	.045	.031	-.049	.035	.021	-.011	.009	.012	.024	.046	.087	.126
.495 135 0	-.022	-.051	-.062	-.022	.002	-.022	-.000	.020	.011	.018	.040	.069	.088
.571 195 0	.017	.018	-.030	-.073	-.063	-.028	.001	.018	.047	.076	.102	.105	.112
.711 189 0	.026	.024	-.003	-.028	-.032	-.039	-.044	-.010	.007	.018	.030	.039	.058
.841 215 0	-.001	.001	-.003	-.024	-.035	-.041	-.043	-.026	.004	.018	.010	.014	.036
.961 209 0	-.029	-.027	-.028	-.033	-.041	-.042	-.048	-.036	-.019	-.007	-.004	.002	.020
1.055 209 0	-.007	-.031	-.029	-.038	-.036	-.027	-.013	.008	.021	.032	.051	.068	.065
1.221 215 0	-.038	-.054	-.043	-.036	-.059	-.061	-.059	-.053	-.032	-.004	.027	.039	.026
1.307 189 0	-.050	-.060	-.053	-.049	-.048	-.047	-.042	-.023	.004	.029	.040	.048	.034
1.439 195 0	-.046	-.048	-.046	-.044	-.046	-.043	-.030	-.009	.021	.043	.064	.060	.041

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.91x10 FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 33

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.371 197 0	-1.043	-.971	-.964	-.966	-.950	-.975	-.907	-.473	-.504	-.824	-.973	-.876	-.744
.641 203 0	-.737	-.749	-.945	-.942	-.935	-.966	-.950	-.909	-.871	-.819	-.735	-.679	-.647
.711 187 0	-.651	-.556	-.706	-.846	-.712	-.600	-.568	-.583	-.582	-.573	-.559	-.546	-.518
.838 181 0	-.327	-.427	-.558	-.541	-.475	-.457	-.455	-.436	-.441	-.459	-.453	-.439	-.408
.966 179 0	-.242	-.261	-.266	-.285	-.302	-.310	-.322	-.307	-.312	-.333	-.331	-.320	-.301
1.047 179 0	-.131	-.175	-.169	-.194	-.184	-.193	-.199	-.168	-.145	-.148	-.157	-.151	-.157
1.173 181 0	-.126	-.132	-.129	-.134	-.143	-.149	-.141	-.123	-.118	-.111	-.111	-.122	-.121
1.307 187 0	-.107	-.114	-.113	-.110	-.112	-.120	-.117	-.101	-.087	-.078	-.075	-.084	-.089
1.439 197 0	-.071	-.076	-.072	-.071	-.073	-.073	-.067	-.054	-.043	-.038	-.029	-.029	-.076

LOCAL FLOW FIELD DATA

MACH = .801 RE = 7.93x10⁶ FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 199 0	.021	.034	.035	.016	-.010	-.002	-.007	-.109	-.187	-.254	-.334	-.409	-.444
.641 201 0	.000	.014	.009	-.011	-.045	-.115	-.144	-.134	-.167	-.185	-.229	-.298	-.357
.711 185 0	.012	.026	.046	.022	-.022	-.052	-.079	-.096	-.111	-.127	-.135	-.132	-.123
.838 183 0	-.008	.020	.031	.019	-.013	-.023	-.036	-.060	-.080	-.097	-.107	-.103	-.087
.966 177 1	-.006	.041	.023	.013	-.023	-.037	-.031	-.045	-.072	-.089	-.100	-.105	-.090
1.047 177 1	-.046	-.004	.056	.027	-.016	-.005	.007	-.005	-.011	-.032	-.061	-.076	-.084
1.173 183 0	.002	-.008	.038	.001	-.005	.008	.016	.014	.007	-.008	-.029	-.047	-.057
1.307 185 0	.024	-.010	-.002	-.008	-.000	.022	.019	.022	.018	.018	.003	-.027	-.037
1.439 199 0	.020	.013	.018	.017	.013	.019	.021	.026	.025	.029	.016	-.013	-.015

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.94X10 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 115 0	.996	.977	.969	.988	.983	.901	.866	.954	.996	.999	.998	.998	1.001
.395 119 0	1.005	.934	.848	.880	.959	.957	.998	1.000	1.001	1.001	1.001	1.003	1.000
.438 115 0	1.010	.945	.880	.916	.970	.991	.997	1.001	.999	.999	1.000	.996	.993
.495 119 0	1.000	.986	.979	.991	1.001	1.004	1.002	1.001	1.000	.998	.994	.995	1.000
.571 193 0	.999	.990	.993	1.003	1.007	1.008	1.007	1.007	1.003	1.000	.999	.997	1.000
.711 191 0	.999	1.002	1.003	1.003	1.003	1.004	1.006	1.006	1.002	.999	.999	.997	.998
.841 213 0	1.001	1.003	1.005	1.004	1.004	1.004	1.005	1.006	1.004	1.000	1.000	1.000	.999
.961 211 0	1.001	1.002	1.003	1.003	1.004	1.004	1.004	1.004	1.002	1.000	1.001	1.000	1.000
1.055 211 0	1.001	1.002	1.003	1.005	1.008	1.011	1.013	1.015	1.015	1.015	1.015	1.010	1.006
1.221 213 0	1.003	1.000	1.001	1.004	1.007	1.010	1.012	1.013	1.013	1.014	1.014	1.010	1.006
1.307 191 0	1.002	.999	.999	1.000	1.002	1.006	1.007	1.007	1.010	1.013	1.011	1.006	1.004
1.439 193 0	1.002	.999	.999	1.001	1.002	1.005	1.006	1.009	1.014	1.014	1.011	1.006	1.005

LOCAL FLOW FIELD DATA

MACH = .803 RE = 7.93x10⁶ -1 FT ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 135 O	.986	.958	.954	.970	.919	.889	.987	.998	.990	.985	.984	.984	.986
.438 131 O	.975	.912	.902	.959	.936	.958	1.001	1.005	1.003	1.003	1.001	1.000	.997
.495 135 O	.975	.889	.901	.965	.982	1.001	1.013	1.013	1.010	1.006	.998	.986	.985
.571 195 O	.999	.953	.938	.973	.999	1.006	1.008	1.008	1.011	1.014	1.014	1.007	1.001
.711 189 O	.998	1.001	1.003	1.004	1.004	1.004	1.001	1.008	1.010	1.010	1.007	1.004	1.002
.841 215 O	1.002	1.004	1.006	1.007	1.007	1.007	1.005	1.006	1.012	1.011	1.005	1.002	1.001
.961 209 O	1.000	1.002	1.005	1.006	1.006	1.004	1.003	1.005	1.006	1.004	1.001	.999	.999
1.055 209 O	1.003	.997	1.001	1.003	1.007	1.010	1.012	1.015	1.016	1.017	1.017	1.017	1.008
1.221 215 O	1.001	1.000	1.002	1.006	1.003	1.004	1.005	1.006	1.007	1.011	1.014	1.014	1.010
1.307 189 O	1.002	.999	1.000	1.000	1.002	1.006	1.006	1.007	1.009	1.013	1.013	1.012	1.004
1.439 195 O	1.002	1.001	1.001	1.003	1.005	1.008	1.011	1.012	1.016	1.017	1.019	1.017	1.006

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.91x10 FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 197 0	.999	.895	.671	.524	.616	.665	.593	.606	.703	.670	1.030	1.056	1.024
.641 203 0	.972	.932	.884	.785	.879	.989	1.012	1.013	1.012	1.007	1.001	.999	1.000
.711 187 0	1.001	.955	.881	.900	.966	.997	.999	.999	.999	1.000	1.001	1.000	1.001
.838 181 0	.998	.990	.988	.996	1.001	1.000	.998	.999	1.000	.999	.998	.999	.999
.966 179 0	.998	.999	1.000	1.001	1.001	1.001	1.000	1.002	1.001	.999	1.000	1.000	.999
1.047 179 0	1.005	1.002	1.005	1.004	1.005	1.005	1.005	1.009	1.011	1.010	1.007	1.008	1.006
1.173 181 0	1.004	1.001	1.004	1.005	1.004	1.004	1.007	1.012	1.011	1.011	1.012	1.009	1.007
1.307 187 0	1.001	.999	.999	1.000	1.001	1.001	1.003	1.007	1.009	1.010	1.010	1.006	1.005
1.439 197 0	1.004	1.002	1.002	1.005	1.006	1.008	1.009	1.013	1.014	1.014	1.016	1.013	1.002

LOCAL FLOW FIELD DATA

1

+6 -1

MACH = .801 RE = 7.93X10 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 199 0	.874	.867	.855	.849	.831	.824	.901	.972	.993	.999	1.006	1.012	1.014
.641 201 0	.844	.822	.838	.891	.926	.962	.986	.991	.988	.980	.980	.983	.987
.711 185 0	.854	.833	.863	.938	.989	1.001	1.000	.998	.998	.996	.998	1.002	1.006
.838 183 0	.914	.874	.837	.895	.970	.999	1.001	.999	.998	.996	.996	.999	1.004
.966 177 1	.973	.873	.810	.887	.972	1.001	1.005	1.004	1.001	.999	.999	.999	1.002
1.047 177 1	1.010	.782	.828	.955	1.006	1.010	1.015	1.015	1.015	1.013	1.008	1.005	1.003
1.173 183 0	1.022	.860	.883	.986	1.003	1.006	1.011	1.012	1.013	1.013	1.010	1.006	1.005
1.307 185 0	.998	.990	.991	1.000	1.004	1.010	1.013	1.014	1.013	1.015	1.013	1.007	1.004
1.439 199 0	1.001	1.002	1.004	1.007	1.008	1.010	1.013	1.015	1.015	1.016	1.014	1.007	1.004

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.94X10 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 115 0	-.170	-.080	.073	.180	.141	.086	.132	.133	.107	.101	.070	.043	.023
.395 119 0	-.349	-.261	-.029	.262	.281	.247	.224	.190	.163	.125	.082	.046	.015
.438 115 0	-.288	-.210	.012	.262	.335	.313	.277	.234	.192	.151	.110	.069	.030
.495 119 0	.009	.044	.166	.265	.301	.308	.287	.259	.219	.179	.139	.101	.065
.571 193 0	.046	.082	.182	.265	.291	.285	.264	.235	.200	.163	.122	.082	.042
.711 191 0	.270	.276	.284	.291	.291	.282	.262	.234	.202	.166	.128	.090	.049
.841 213 0	.301	.304	.309	.309	.302	.287	.267	.241	.205	.167	.128	.087	.045
.961 211 0	.325	.325	.325	.322	.311	.292	.269	.242	.208	.171	.131	.089	.046
1.055 211 0	.345	.327	.322	.311	.296	.277	.256	.233	.203	.166	.129	.088	.043
1.221 213 0	.366	.343	.338	.327	.311	.288	.264	.240	.212	.175	.139	.097	.049
1.307 191 0	.356	.341	.334	.321	.303	.281	.258	.232	.201	.162	.125	.084	.042
1.439 193 0	.361	.350	.339	.323	.303	.281	.258	.231	.199	.163	.126	.085	.040

LOCAL FLOW FIELD DATA

*6 -1

MACH = .803 RE = 7.93X10 FT ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 135 O	-.078	.087	.281	.324	.283	.288	.307	.296	.262	.229	.210	.200	.195
.438 131 O	-.092	.061	.327	.448	.464	.444	.438	.414	.376	.344	.309	.275	.244
.495 135 O	-.102	.059	.368	.510	.518	.487	.447	.422	.385	.349	.316	.280	.237
.571 195 O	-.003	.122	.324	.431	.460	.443	.408	.373	.339	.301	.263	.226	.186
.711 189 O	.242	.269	.327	.379	.394	.387	.364	.337	.308	.271	.232	.193	.152
.841 215 O	.333	.345	.364	.376	.377	.365	.341	.317	.285	.248	.209	.170	.127
.981 209 O	.358	.361	.372	.375	.367	.352	.329	.304	.272	.235	.195	.152	.108
1.055 209 O	.378	.352	.356	.350	.340	.323	.302	.280	.250	.214	.180	.140	.095
1.221 215 O	.385	.363	.362	.355	.330	.307	.283	.257	.227	.192	.156	.115	.072
1.307 189 O	.378	.363	.354	.340	.323	.305	.282	.256	.227	.191	.153	.113	.071
1.439 195 O	.373	.357	.351	.340	.326	.306	.282	.255	.226	.192	.155	.115	.072

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.91x10 FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 197 0	-.194	-.141	-.164	-.156	-.142	-.165	-.236	-.269	-.226	-.193	-.165	-.122	-.081
.641 203 0	-.109	-.005	.178	.161	.207	.222	.188	.171	.141	.096	.058	.035	.020
.711 187 0	-.121	-.048	.222	.463	.448	.369	.313	.258	.207	.161	.115	.073	.039
.838 181 0	.108	.160	.270	.370	.389	.357	.311	.262	.218	.178	.135	.093	.055
.966 179 0	.250	.256	.288	.321	.325	.310	.285	.254	.217	.180	.143	.101	.060
1.047 179 0	.263	.285	.298	.307	.304	.289	.271	.241	.204	.172	.138	.095	.056
1.173 181 0	.306	.289	.299	.303	.293	.277	.259	.231	.199	.165	.130	.092	.050
1.307 187 0	.321	.312	.309	.303	.290	.273	.254	.230	.200	.166	.130	.095	.055
1.439 197 0	.336	.319	.316	.311	.295	.276	.255	.232	.205	.171	.136	.098	.062

LOCAL FLOW FIELD DATA

MACH = .801 RE = 7.93x10 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 199 0	-.069	-.053	-.026	-.016	-.007	.053	.094	.087	.070	.054	.042	.034	.023
.641 201 0	-.089	-.038	.035	.082	.108	.131	.165	.168	.141	.108	.078	.053	.028
.711 185 0	-.087	-.020	.093	.154	.176	.181	.178	.162	.135	.102	.071	.045	.022
.838 183 0	-.052	-.001	.129	.214	.233	.226	.206	.183	.153	.119	.083	.052	.025
.966 177 1	.004	.073	.184	.232	.249	.247	.225	.196	.166	.133	.094	.058	.028
1.047 177 1	.026	.106	.198	.221	.232	.218	.196	.173	.147	.117	.082	.044	.006
1.173 183 0	.142	.113	.192	.243	.236	.218	.200	.177	.149	.116	.081	.048	.010
1.307 185 0	.213	.228	.255	.263	.250	.232	.214	.192	.164	.130	.095	.061	.021
1.439 199 0	.262	.257	.274	.277	.263	.246	.227	.203	.174	.141	.106	.071	.031

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.94×10^5 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 115 0	.000	-.142	-.216	-.164	-.104	-.025	.191	.401	.436	.466	.497	.523	.542
.395 119 0	.000	-.148	-.043	.071	.202	.318	.383	.394	.412	.437	.456	.472	.473
.438 115 0	.000	.041	.178	.244	.292	.318	.338	.372	.397	.421	.442	.449	.450
.493 119 0	-.000	.149	.254	.292	.295	.304	.319	.334	.352	.368	.378	.392	.405
.571 193 0	-.000	.141	.265	.299	.302	.312	.332	.352	.367	.382	.399	.408	.415
.711 191 0	-.000	.078	.142	.193	.239	.277	.306	.330	.349	.361	.375	.383	.387
.841 213 0	-.000	.070	.126	.176	.224	.262	.295	.321	.340	.354	.368	.374	.377
.961 211 0	-.000	.059	.112	.160	.206	.243	.274	.303	.327	.342	.357	.364	.367
1.055 211 0	.000	.095	.131	.180	.221	.259	.290	.321	.344	.364	.375	.373	.369
1.221 213 0	.000	.094	.127	.175	.216	.256	.287	.315	.339	.355	.367	.368	.368
1.307 191 0	.000	.076	.112	.159	.201	.240	.270	.296	.326	.354	.365	.365	.363
1.439 193 0	.000	.075	.110	.157	.197	.236	.265	.298	.333	.352	.362	.364	.365

LOCAL FLOW FIELD DATA

MACH = .803 $RE = 7.93 \times 10^6$ FT $\alpha = 20.080$ $X/D = 4.100$ TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (V_{θ}/V_{∞})

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 135 0	.000	-.183	-.169	-.084	.027	.223	.344	.400	.439	.470	.488	.512	.506
.438 131 0	.000	-.089	-.094	.003	.128	.265	.323	.351	.395	.431	.457	.471	.474
.495 135 0	-.000	.060	.144	.194	.255	.304	.319	.336	.370	.388	.391	.385	.395
.571 195 0	-.000	.153	.222	.272	.284	.287	.312	.341	.371	.399	.419	.425	.428
.711 189 0	-.000	.125	.214	.238	.253	.282	.304	.336	.363	.387	.401	.405	.408
.841 215 0	-.000	.093	.167	.214	.245	.271	.297	.326	.358	.377	.383	.388	.393
.961 209 0	-.000	.067	.136	.189	.229	.260	.289	.317	.342	.361	.372	.378	.381
1.055 209 0	.000	.109	.151	.200	.240	.278	.306	.331	.356	.374	.388	.395	.384
1.221 215 0	.000	.101	.134	.183	.224	.260	.290	.316	.343	.367	.382	.388	.381
1.307 189 0	.000	.082	.120	.169	.210	.249	.281	.306	.331	.359	.376	.379	.371
1.439 195 0	.000	.080	.116	.162	.204	.244	.277	.306	.336	.356	.374	.382	.366

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.91×10^6 FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (V_{THETA}/V_{INF})

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 197 0	-.000	-.177	-.349	.002	.107	-.022	.009	.105	.204	.410	.653	.721	.689
.641 203 0	.000	-.091	-.232	-.181	-.058	.165	.335	.384	.427	.462	.487	.518	.541
.711 187 0	-.000	.045	.083	.108	.204	.265	.303	.360	.401	.437	.468	.492	.510
.838 181 0	-.000	.174	.291	.305	.285	.288	.317	.358	.389	.413	.439	.457	.463
.966 179 0	-.000	.100	.178	.216	.245	.278	.310	.344	.372	.394	.413	.424	.427
1.047 179 0	.000	.109	.161	.217	.255	.279	.307	.336	.368	.387	.397	.411	.408
1.173 181 0	.000	.104	.148	.196	.237	.272	.305	.341	.366	.388	.403	.407	.404
1.307 187 0	.000	.092	.134	.182	.224	.261	.293	.325	.355	.379	.392	.391	.393
1.439 197 0	.000	.090	.130	.181	.225	.263	.296	.328	.353	.374	.392	.395	.379

LOCAL FLOW FIELD DATA

MACH = .001 RE = 7.93×10^5 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 199 0	.000	-.017	-.025	.029	.099	.220	.361	.445	.495	.548	.607	.659	.685
.641 201 0	.000	-.007	.099	.202	.286	.346	.384	.402	.427	.443	.469	.502	.530
.711 185 0	-.000	.062	.185	.268	.313	.348	.379	.406	.432	.455	.479	.503	.519
.838 183 0	-.000	.002	.068	.185	.248	.292	.335	.364	.393	.419	.439	.457	.471
.966 177 1	-.000	.005	.103	.203	.244	.277	.319	.350	.376	.399	.417	.429	.440
1.047 177 1	.000	.020	.165	.232	.261	.303	.344	.373	.398	.415	.423	.428	.427
1.173 183 0	.000	.076	.161	.218	.248	.292	.328	.358	.385	.405	.414	.415	.413
1.307 185 0	.000	.127	.161	.196	.237	.285	.316	.342	.368	.392	.403	.402	.402
1.439 199 0	.000	.113	.152	.192	.232	.269	.301	.331	.359	.382	.393	.389	.388

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.94X10 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

(VC / VINP * SIN ALPHAINP)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 115 0	.495	.475	.663	.710	.510	.262	.676	1.230	1.307	1.388	1.463	1.529	1.581
.395 119 0	1.016	.875	.152	.790	1.007	1.174	1.292	1.273	1.290	1.323	1.349	1.381	1.377
.458 115 0	.839	.624	.518	1.043	1.296	1.301	1.274	1.281	1.283	1.303	1.328	1.324	1.314
.495 119 0	.026	.452	.883	1.147	1.228	1.260	1.251	1.230	1.208	1.193	1.172	1.178	1.194
.571 193 0	.135	.474	.938	1.164	1.222	1.231	1.235	1.233	1.217	1.211	1.214	1.211	1.214
.711 191 0	.787	.835	.925	1.018	1.096	1.151	1.173	1.178	1.174	1.159	1.155	1.146	1.136
.841 213 0	.876	.908	.972	1.036	1.096	1.131	1.159	1.169	1.158	1.140	1.134	1.119	1.105
.961 211 0	.945	.961	1.002	1.047	1.086	1.105	1.118	1.129	1.129	1.112	1.108	1.093	1.078
1.055 211 0	1.004	.991	1.014	1.048	1.078	1.105	1.127	1.154	1.164	1.164	1.154	1.118	1.082
1.221 213 0	1.066	1.036	1.052	1.080	1.103	1.123	1.137	1.154	1.165	1.153	1.143	1.109	1.082
1.307 191 0	1.037	1.017	1.026	1.042	1.058	1.075	1.089	1.095	1.115	1.134	1.123	1.091	1.064
1.439 193 0	1.052	1.044	1.038	1.045	1.052	1.069	1.079	1.098	1.128	1.129	1.118	1.088	1.071

LOCAL FLOW FIELD DATA

MACH = .803 RE = 7.93X10⁺⁶ FT ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

(VC / VINP * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 135 0	.226	.590	.956	.974	.828	1.061	1.342	1.448	1.468	1.523	1.548	1.600	1.580
.438 131 0	.267	.313	.990	1.305	1.403	1.506	1.584	1.581	1.588	1.605	1.606	1.590	1.553
.495 135 0	.298	.247	1.151	1.589	1.681	1.671	1.599	1.571	1.555	1.521	1.465	1.385	1.341
.571 195 0	.009	.571	1.144	1.484	1.576	1.536	1.494	1.472	1.464	1.456	1.441	1.402	1.354
.711 189 0	.704	.863	1.138	1.303	1.364	1.396	1.382	1.386	1.386	1.377	1.349	1.306	1.268
.841 215 0	.969	1.039	1.167	1.260	1.310	1.323	1.318	1.323	1.332	1.315	1.271	1.233	1.203
.961 209 0	1.043	1.070	1.154	1.222	1.259	1.274	1.276	1.280	1.273	1.256	1.223	1.188	1.154
1.055 209 0	1.101	1.073	1.125	1.175	1.214	1.240	1.251	1.262	1.267	1.257	1.246	1.220	1.191
1.221 215 0	1.122	1.097	1.123	1.163	1.160	1.171	1.180	1.187	1.198	1.207	1.202	1.180	1.129
1.307 189 0	1.101	1.084	1.089	1.107	1.122	1.148	1.161	1.163	1.170	1.185	1.181	1.153	1.099
1.439 195 0	1.087	1.066	1.077	1.096	1.119	1.141	1.152	1.161	1.179	1.177	1.179	1.161	1.087

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.91x10 FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

(VC / VINF * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 197 0	.565	.659	1.124	.453	.517	.486	.687	.842	.687	1.320	1.961	2.130	2.020
.641 203 0	.318	.266	.851	.705	.626	.806	1.119	1.225	1.310	1.374	1.427	1.511	1.577
.711 187 0	.351	.192	.690	1.384	1.434	1.323	1.269	1.289	1.316	1.357	1.405	1.450	1.489
.838 181 0	.314	.687	1.155	1.395	1.405	1.337	1.293	1.292	1.300	1.310	1.336	1.357	1.359
.966 179 0	.728	.800	.984	1.127	1.186	1.215	1.226	1.245	1.256	1.261	1.274	1.270	1.257
1.047 179 0	.767	.888	.986	1.095	1.154	1.170	1.193	1.204	1.227	1.234	1.224	1.228	1.199
1.173 181 0	.892	.896	.972	1.051	1.096	1.131	1.166	1.199	1.213	1.227	1.232	1.215	1.186
1.307 187 0	.935	.946	.979	1.030	1.066	1.099	1.128	1.160	1.186	1.205	1.202	1.172	1.155
1.439 197 0	.978	.965	.996	1.049	1.081	1.111	1.137	1.169	1.188	1.197	1.207	1.186	1.118

LOCAL FLOW FIELD DATA

MACH = .801 RE = 7.93x10 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

(VC / VINF * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.371 199 0	.200	.162	.107	.095	.290	.659	1.086	1.320	1.457	1.603	1.773	1.921	1.997
.641 201 0	.261	.111	.306	.635	.889	1.078	1.217	1.268	1.309	1.327	1.385	1.469	1.544
.711 185 0	.253	.191	.603	.899	1.045	1.143	1.220	1.274	1.320	1.358	1.412	1.470	1.513
.838 183 0	.151	.007	.426	.824	.992	1.076	1.144	1.186	1.229	1.268	1.302	1.339	1.375
.966 177 1	.010	.214	.615	.898	1.014	1.081	1.137	1.168	1.196	1.226	1.246	1.262	1.284
1.047 177 1	.077	.315	.751	.932	1.017	1.086	1.153	1.198	1.237	1.256	1.255	1.254	1.245
1.173 183 0	.415	.397	.730	.951	.998	1.061	1.118	1.163	1.201	1.225	1.229	1.217	1.203
1.307 185 0	.622	.760	.878	.957	1.005	1.070	1.112	1.143	1.172	1.202	1.206	1.184	1.174
1.439 199 0	.764	.817	.913	.980	1.022	1.063	1.098	1.132	1.161	1.187	1.185	1.153	1.135

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.94x10 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 115 0	.965	.937	.902	.940	.945	.787	.622	.774	.924	.893	.890	.888	.890
.395 119 0	.974	.868	.792	.802	.854	.792	.890	.880	.880	.882	.886	.885	.873
.438 115 0	.963	.888	.830	.845	.867	.886	.885	.875	.877	.876	.875	.881	.885
.495 119 0	.915	.913	.905	.894	.886	.882	.888	.889	.891	.894	.891	.898	.907
.571 193 0	.918	.900	.885	.878	.877	.876	.875	.876	.882	.887	.888	.886	.880
.711 191 0	.902	.899	.893	.892	.890	.886	.886	.886	.890	.895	.897	.893	.890
.841 213 0	.905	.904	.899	.897	.899	.897	.895	.892	.893	.899	.898	.898	.895
.961 211 0	.911	.909	.902	.899	.902	.904	.903	.900	.899	.903	.904	.904	.900
1.055 211 0	.903	.914	.908	.906	.906	.904	.900	.894	.888	.884	.884	.892	.894
1.221 213 0	.905	.917	.912	.912	.910	.909	.907	.897	.887	.887	.889	.896	.894
1.307 191 0	.924	.927	.922	.919	.920	.920	.921	.915	.905	.893	.895	.903	.902
1.439 193 0	.930	.929	.926	.924	.924	.923	.922	.914	.900	.896	.897	.902	.905

LOCAL FLOW FIELD DATA

MACH = .803 $Re = 7.93 \times 10^6$ $\alpha = 20.060$ $X/D = 4.100$ TEST NO. = 35

AXIAL VELOCITY RATIO -- (V_x / V_{inf}) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 135 O	.918	.826	.799	.838	.740	.614	.803	.790	.786	.785	.774	.757	.744
.438 131 O	.949	.856	.786	.869	.763	.784	.847	.842	.835	.824	.808	.784	.765
.495 135 O	.978	.882	.820	.803	.790	.834	.854	.847	.852	.850	.838	.820	.817
.571 195 O	.990	.914	.856	.869	.876	.873	.868	.863	.852	.840	.828	.825	.822
.711 189 O	.954	.944	.926	.915	.907	.904	.907	.895	.888	.883	.879	.876	.870
.841 215 O	.946	.938	.926	.923	.921	.922	.921	.913	.901	.896	.900	.900	.892
.961 209 O	.949	.947	.939	.933	.931	.928	.929	.924	.917	.911	.911	.911	.906
1.055 209 O	.933	.943	.940	.940	.937	.931	.924	.915	.909	.905	.897	.892	.893
1.221 215 O	.945	.955	.949	.943	.952	.953	.952	.948	.938	.925	.913	.910	.920
1.307 189 O	.955	.959	.955	.952	.951	.951	.947	.938	.925	.914	.909	.906	.912
1.439 195 O	.955	.958	.955	.954	.954	.953	.947	.936	.922	.912	.902	.905	.913

LOCAL FLOW FIELD DATA

+8 -1

MACH = .799 RE = 7.91X10 FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 197 0	1.499	1.386	.776	.384	.709	.851	.581	.556	.831	1.213	1.335	1.268	1.192
.641 203 0	1.333	1.308	1.345	1.263	1.350	1.439	1.422	1.390	1.361	1.322	1.267	1.224	1.198
.711 187 0	1.312	1.230	1.221	1.251	1.225	1.207	1.209	1.204	1.200	1.191	1.177	1.164	1.144
.838 181 0	1.153	1.176	1.197	1.165	1.134	1.133	1.136	1.128	1.130	1.136	1.129	1.120	1.104
.966 179 0	1.089	1.093	1.079	1.073	1.075	1.075	1.079	1.070	1.070	1.079	1.077	1.071	1.062
1.047 179 0	1.037	1.044	1.034	1.033	1.021	1.024	1.025	1.010	.998	.997	.999	.997	1.002
1.173 181 0	1.021	1.021	1.014	1.009	1.007	1.005	1.000	.991	.985	.980	.980	.985	.987
1.307 187 0	1.004	1.004	1.000	.994	.991	.992	.988	.979	.971	.964	.963	.967	.972
1.439 197 0	.983	.986	.980	.976	.975	.972	.968	.960	.953	.948	.944	.944	.966

LOCAL FLOW FIELD DATA

MACH = .801 RE = 7.93×10^4 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

AXIAL VELOCITY RATIO -- (V_X / V_{INF}) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 199 0	.817	.799	.778	.780	.759	.711	.795	.918	.963	.981	.998	1.014	1.020
.641 201 0	.774	.731	.756	.836	.883	.946	.970	.963	.972	.969	.984	1.011	1.034
.711 185 0	.788	.740	.756	.859	.932	.949	.950	.950	.951	.951	.947	.940	.932
.838 183 0	.895	.820	.734	.806	.911	.940	.941	.944	.947	.949	.949	.943	.935
.966 177 1	.972	.802	.668	.785	.916	.950	.943	.945	.952	.955	.957	.957	.950
1.047 177 1	1.035	.650	.664	.876	.952	.942	.932	.932	.930	.936	.945	.951	.954
1.173 183 0	1.013	.805	.784	.928	.946	.934	.927	.924	.923	.927	.934	.941	.947
1.307 185 0	.963	.959	.944	.949	.944	.930	.929	.924	.921	.919	.925	.937	.940
1.439 199 0	.956	.955	.945	.941	.939	.933	.930	.925	.921	.917	.922	.933	.934

LOCAL VORTICITY X 100.

*6 -1

MACH = .799 RE = 7.94x10 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.3550	41.794	119.824	164.593	79.194	84.634	105.100	44.110	9.831	10.632	1.647	2.508	2.853
.4165	91.423	223.972	245.246	109.919	30.519	-5.963	-14.430	-2.717	-1.885	-1.302	-1.009	-1.302
.4665	49.228	116.854	111.518	48.517	10.525	-1.665	-9.018	-15.541	-17.145	-20.925	-20.865	-15.208
.5350	14.835	49.763	48.740	27.518	16.593	10.759	10.601	8.412	8.278	9.127	10.542	9.636
.6410	2.723	5.606	1.669	-1.095	-.017	.459	.191	.064	-.034	-.979	-.730	-1.158
.7760	1.565	2.769	2.703	2.691	2.147	1.795	1.395	.848	.744	.748	.777	.236
.9010	.034	.596	.491	-.163	-1.095	-1.159	-1.430	-1.737	-1.213	-.854	-.835	-.761
1.0090	4.085	9.465	7.456	7.036	6.336	6.684	7.238	6.640	6.630	6.966	4.845	2.183
1.1380	-2.473	1.195	.772	.929	1.086	1.721	2.052	1.629	.454	.640	.281	-.206
1.2640	-4.581	-3.634	-3.571	-3.432	-3.453	-3.153	-3.359	-2.834	-1.057	1.133	.286	-.794
1.3730	-1.256	.196	.097	.042	.250	.637	1.108	2.164	1.455	.958	.576	.684

31

LOCAL VORTICITY X 100.

MACH = .803 RE = 7.93x10 FT ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

THETA 176.25 168.75 161.25 153.75 146.25 138.75 131.25 123.75 116.25 108.75 101.25 93.75

R/D

.4165	95.905	146.689	79.705	49.984	47.969	26.335	-6.938	-19.490	-13.058	-5.152	-1.919	.092
.4665	96.665	202.727	151.126	82.207	38.630	14.413	3.466	-4.616	-7.496	-15.253	-24.965	-28.322
.5330	69.253	126.402	80.141	36.198	6.549	-3.099	4.310	5.033	6.683	12.346	16.983	16.226
.6410	22.857	42.344	29.154	11.069	4.004	1.811	2.305	3.138	1.949	1.372	1.237	.733
.7760	3.428	6.759	7.821	6.621	4.249	1.818	2.156	2.189	1.434	.221	-.218	-.695
.9010	.049	.460	.449	1.052	1.161	.832	1.510	.081	-1.127	-.823	-.181	-.786
1.0080	4.482	11.811	7.365	6.601	7.085	7.446	7.282	6.083	5.675	6.025	6.014	3.656
1.1380	-3.477	1.013	.090	-.826	-.432	-.067	.527	.299	.489	1.405	.679	.426
1.2640	-4.582	-3.202	-2.597	-3.465	-1.993	-.989	-.737	-1.211	-1.420	-.338	-.850	-1.698
1.3730	-1.647	.238	-.199	-.057	.505	.632	1.228	2.182	1.547	1.036	1.426	.718

LOCAL VORTICITY X 100.

MACH = .799 RE = 7.91X10 FT ALPHA = 20.080 X/D = 4.800 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.6060	37.312	52.608	-20.866	-53.930	4.604	80.127	108.520	103.239	62.590	-1.309	-36.122	-33.168
.6760	48.788	142.755	137.539	103.401	60.783	9.356	-7.492	-5.873	-6.010	-2.427	1.229	2.126
.7745	29.752	84.774	88.158	35.223	4.926	.376	-.749	-.774	-.927	-2.026	-1.898	-1.425
.9020	.874	1.941	1.288	-2.675	-2.105	-1.047	-1.215	-1.508	-.888	-1.313	-2.522	-2.744
1.0065	5.222	6.470	6.438	7.434	5.335	2.716	.593	-.099	1.167	-.350	-2.416	-2.260
1.1100	1.119	3.098	1.819	.121	.850	2.652	2.626	2.356	2.566	3.501	2.399	1.440
1.2400	-2.166	.427	.527	-.125	.217	.619	-.284	-.234	.416	.577	-.028	-.835
1.3730	-1.213	1.091	1.717	1.701	2.230	2.784	2.952	2.289	1.266	1.555	2.408	.848

LOCAL VORTICITY X 100.

MACH = .801 RE = 7.93x10 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 33

THETA 176.25 168.75 161.25 153.75 146.25 138.75 131.25 123.75 116.25 108.75 101.25 93.75

R/D

.6060	12.093	39.981	65.483	76.105	78.639	52.064	12.070	-8.662	-19.130	-28.477	-35.050	-36.963
.6760	29.767	57.012	49.408	33.146	21.190	17.383	12.682	9.641	10.099	12.523	12.839	10.521
.7745	9.049	15.047	4.010	-1.240	-2.327	-1.857	-1.358	-2.160	-1.915	-1.424	-.367	.375
.9020	13.116	30.597	23.106	11.254	4.445	.977	1.171	.775	.345	-.400	.133	.647
1.0065	16.592	32.819	24.845	15.640	11.990	11.251	11.095	11.111	9.769	6.562	4.234	2.113
1.1100	10.483	22.286	8.894	3.196	1.057	1.031	.821	1.033	1.160	1.428	1.225	.149
1.2400	4.648	15.652	6.130	.018	.896	1.567	.797	-.046	-.173	.583	.807	.018
1.3730	.312	3.402	2.595	1.153	.230	-.192	.167	.546	.464	.499	.161	-.830

LOCAL CIRCULATION STRENGTH X 100.

*6 -1

MACH = .799 RE = 7.94x10 FT ALPHA = 20.080 X/D = 3.500 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.3550	.198	.567	.779	.375	.401	.497	.209	.047	.050	.008	.012	.014	3.1558
.4165	.273	.669	.732	.328	.091	-.018	-.043	-.008	-.006	-.004	-.003	-.004	2.0073
.4665	.218	.527	.494	.215	.047	-.007	-.040	-.069	-.076	-.093	-.092	-.067	1.0560
.5330	.100	.336	.329	.186	.112	.073	.072	.057	.056	.062	.071	.065	1.5177
.6410	.041	.084	.025	-.016	-.000	.007	.003	.001	-.001	-.015	-.011	-.017	.1002
.7760	.026	.047	.045	.045	.036	.030	.023	.014	.013	.013	.013	.004	.3097
.9010	.001	.011	.009	-.003	-.020	-.021	-.026	-.031	-.022	-.015	-.015	-.014	-.1464
1.0080	.065	.149	.118	.111	.100	.106	.114	.105	.105	.110	.077	.034	1.1933
1.1380	-.078	.038	.024	.029	.034	.054	.065	.051	.014	.020	.009	-.006	.2544
1.2640	-.083	-.066	-.065	-.062	-.063	-.057	-.061	-.051	-.019	.021	.005	-.014	-.5154
1.3730	-.038	.006	.003	.001	.008	.019	.033	.065	.044	.029	.017	.021	.2088
RSUM	.722	2.367	2.494	1.209	.746	.683	.349	.180	.159	.135	.083	.014	9.1414

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = .805 RE = 7.03X10⁶ FT ALPHA = 20.080 X/D = 4.100 TEST NO. = 35

THETA	176.25	166.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.4165	.286	.438	.238	.149	.143	.079	-.021	-.058	-.039	-.015	-.006	.000	1.1943
.4665	.428	.898	.670	.364	.171	.064	.015	-.020	-.033	-.068	-.111	-.126	2.2539
.5330	.468	.653	.541	.244	.044	-.021	.029	.034	.045	.083	.115	.110	2.5454
.6410	.342	.633	.436	.166	.060	.027	.034	.047	.029	.021	.019	.011	1.8243
.7760	.058	.114	.132	.111	.071	.031	.036	.037	.024	.004	-.004	-.012	.6016
.9010	.001	.008	.008	.019	.021	.015	.027	.001	-.020	-.015	-.003	-.014	.0482
1.0080	.071	.187	.116	.104	.112	.118	.115	.096	.090	.095	.095	.058	1.2559
1.1380	-.109	.032	.003	-.026	-.014	-.002	.017	.009	.015	.044	.021	.013	.0039
1.2640	-.083	-.058	-.047	-.063	-.036	-.018	-.013	-.022	-.026	-.006	-.015	-.031	-.4182
1.3730	-.050	.007	-.006	-.002	.015	.019	.037	.066	.047	.031	.043	.022	.2298
RSUM	1.411	3.113	2.090	1.067	.588	.311	.277	.190	.132	.174	.154	.032	9.5393

LOCAL CIRCULATION STRENGTH X 100.

*6 -1

MACH = .799 RE = 7.91X10 FT ALPHA = 20.080 X/D = 4.600 TEST NO. = 35

THETA	176.25	166.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.6060	.264	.372	-.148	-.381	.033	.567	.767	.730	.443	-.009	-.270	-.235	2.1324
.6760	.385	1.126	1.085	.815	.479	.074	-.059	-.046	-.047	-.019	.010	.017	3.8185
.7745	.488	1.390	1.445	.577	.081	.006	-.012	-.013	-.015	-.033	-.031	-.023	3.8592
.9020	.017	.037	.025	-.051	-.041	-.020	-.023	-.029	-.017	-.025	-.049	-.053	-.2293
1.0065	.071	.088	.087	.101	.072	.037	.008	-.001	.016	-.005	-.033	-.031	.4113
1.1100	.026	.072	.042	.003	.020	.062	.061	.055	.060	.082	.056	.034	.5722
1.2400	-.060	.012	.015	-.003	.006	.017	-.008	-.006	.012	.016	-.001	-.023	-.0246
1.3730	-.037	.033	.052	.051	.067	.084	.089	.069	.038	.047	.073	.026	.5929
RSUM	1.154	3.130	2.604	1.112	.718	.826	.823	.758	.488	.053	-.244	-.289	11.1326

LOCAL CIRCULATION STRENGTH X 100.

MACH = .801 RE = 7.93X10 FT ALPHA = 20.080 X/D = 6.500 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.6060	.085	.283	.463	.538	.556	.368	.085	-.061	-.135	-.201	-.248	-.261	1.4716
.6760	.235	.450	.390	.261	.167	.137	.100	.076	.080	.099	.101	.083	2.1784
.7745	.148	.247	.066	-.020	-.038	-.030	-.022	-.035	-.031	-.023	-.006	.006	.2595
.9020	.252	.589	.445	.217	.086	.019	.023	.015	.007	-.008	.003	.012	1.6581
1.0065	.225	.446	.338	.213	.163	.153	.151	.151	.133	.089	.058	.029	2.1472
1.1100	.244	.519	.207	.075	.025	.024	.019	.024	.027	.033	.029	.003	1.2299
1.2400	.129	.433	.170	.001	.025	.043	.022	-.001	-.005	.016	.022	.001	.8557
1.3730	.009	.103	.078	.035	.007	-.006	.005	.016	.014	.015	.005	-.025	.2570
RSUM	1.329	3.069	2.156	1.318	.990	.708	.383	.185	.089	.020	-.037	-.152	10.0574

SECTION IV

$$M_{\infty}=0.8, \alpha=24.6^{\circ}, Re=7.9 \times 10^6 ft^{-1},$$

$$X/D = 3.5, 4.1, 4.8, 6.5$$

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.94X10⁺⁶ FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 116 0	.788	.780	.784	.794	.772	.662	.578	.717	.821	.830	.847	.867	.901
.395 120 0	.798	.738	.719	.744	.678	.662	.783	.796	.806	.823	.832	.831	.821
.438 116 0	.820	.744	.680	.755	.744	.783	.819	.811	.807	.804	.805	.804	.811
.495 120 0	.871	.712	.662	.791	.810	.813	.813	.809	.795	.793	.798	.811	.828
.571 194 0	.833	.732	.625	.798	.850	.827	.808	.800	.797	.793	.793	.790	.786
.711 192 0	.729	.726	.755	.786	.798	.800	.800	.799	.802	.802	.799	.798	.790
.841 214 0	.752	.742	.755	.784	.798	.802	.802	.799	.799	.800	.796	.792	.784
.961 212 0	.764	.766	.778	.789	.800	.806	.807	.804	.803	.802	.798	.794	.786
1.055 212 0	.765	.780	.787	.790	.790	.794	.795	.796	.797	.795	.794	.793	.793
1.221 214 0	.776	.792	.794	.794	.793	.795	.794	.794	.794	.791	.790	.792	.789
1.307 192 0	.800	.804	.800	.804	.805	.800	.799	.799	.800	.799	.798	.799	.787
1.439 194 0	.801	.808	.804	.805	.808	.806	.803	.803	.801	.798	.798	.800	.791

LOCAL FLOW FIELD DATA

+8 -1

MACH = .799 RE = 7.93x10 FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 136 0	.706	.712	.759	.799	.701	.598	.725	.758	.767	.776	.774	.766	.770
.438 132 0	.699	.704	.758	.817	.717	.749	.831	.839	.839	.835	.808	.780	.768
.495 136 0	.747	.694	.766	.764	.810	.859	.857	.854	.840	.825	.794	.758	.753
.571 196 0	.807	.697	.726	.808	.866	.878	.857	.844	.834	.820	.802	.782	.770
.711 190 0	.814	.772	.802	.893	.924	.906	.870	.851	.839	.825	.814	.798	.783
.841 216 0	.785	.800	.838	.864	.868	.863	.856	.849	.836	.819	.816	.809	.795
.961 210 0	.812	.809	.835	.855	.858	.856	.855	.850	.837	.830	.826	.814	.802
1.055 210 0	.817	.788	.828	.831	.837	.839	.835	.831	.830	.826	.818	.813	.807
1.221 216 0	.814	.831	.834	.836	.834	.837	.834	.830	.828	.822	.814	.810	.811
1.307 190 0	.834	.841	.838	.838	.839	.836	.835	.834	.831	.825	.820	.820	.804
1.439 196 0	.832	.835	.837	.837	.835	.829	.827	.824	.819	.817	.813	.808	.795

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.91x10⁶ FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 198 0	1.251	1.070	.622	.393	.368	.432	.527	.509	.793	1.217	1.239	1.148	1.126
.641 204 0	1.097	1.081	1.145	.927	1.001	1.066	1.202	1.295	1.246	1.170	1.126	1.103	1.092
.711 188 0	1.072	.921	.956	1.141	.998	1.034	1.093	1.082	1.080	1.078	1.074	1.067	1.053
.838 182 0	1.014	.950	.986	1.072	1.055	1.026	1.021	1.013	1.016	1.019	1.020	1.015	.994
.966 180 1	.853	.903	.951	.971	.982	.984	.972	.968	.973	.975	.970	.967	.950
1.047 180 1	.848	.859	.898	.919	.906	.899	.900	.895	.887	.889	.897	.907	.919
1.173 182 0	.837	.853	.859	.876	.881	.877	.877	.876	.872	.870	.871	.875	.896
1.307 188 0	.821	.841	.849	.859	.866	.866	.864	.865	.864	.862	.863	.863	.859
1.439 198 0	.832	.835	.842	.853	.855	.853	.853	.850	.851	.850	.851	.848	.845

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.93X10⁺⁶ -1 FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 200 0	.554	.556	.599	.643	.584	.499	.540	.736	.968	1.058	1.083	1.115	1.128
.641 202 0	.593	.575	.632	.715	.735	.789	.854	.874	.890	.913	.952	1.011	1.052
.711 186 0	.616	.575	.612	.725	.789	.839	.862	.860	.863	.887	.912	.939	.963
.838 184 0	.650	.655	.667	.764	.812	.820	.824	.840	.848	.849	.857	.859	.858
.966 178 0	.724	.661	.616	.731	.801	.821	.825	.827	.839	.844	.850	.851	.845
1.047 178 0	.762	.492	.671	.812	.826	.827	.833	.840	.841	.854	.869	.869	.863
1.173 184 0	.854	.560	.687	.809	.821	.821	.826	.829	.832	.841	.850	.850	.851
1.307 186 0	.810	.662	.657	.799	.822	.820	.822	.825	.825	.832	.840	.844	.843
1.439 200 0	.767	.779	.769	.820	.819	.817	.816	.819	.822	.827	.833	.836	.833

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.94X10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 116 0 2.333	1.600	4.045	4.713	4.752	7.091	20.299	30.070	29.982	32.927	35.193	37.048	37.672	
.395 120 0 13.445	17.251	9.205	10.330	12.841	27.908	30.083	30.726	31.332	32.255	32.163	32.834	33.147	
.438 116 0 17.753	13.750	13.866	16.514	23.938	30.024	30.518	31.389	31.812	32.173	32.709	32.441	32.413	
.495 120 0 22.348	16.541	19.680	32.789	32.862	32.723	31.782	30.680	29.794	29.047	28.330	27.997	28.067	
.571 194 0 20.074	20.188	20.289	34.835	33.538	32.035	31.908	31.910	31.129	30.538	30.577	30.275	30.697	
.711 192 0 10.634	16.084	23.774	27.134	28.217	28.763	29.412	29.849	29.689	29.475	29.523	29.125	29.320	
.841 214 0 15.283	18.324	23.990	26.918	27.967	28.466	29.083	29.708	29.269	28.740	28.693	28.411	28.313	
.961 212 0 20.084	21.455	24.296	26.292	27.280	27.620	28.075	28.606	28.605	28.210	28.077	27.601	27.473	
1.055 212 0 22.926	23.004	24.928	27.049	28.424	28.733	28.770	28.835	28.783	28.688	28.255	27.490	27.093	
1.221 214 0 25.363	24.612	25.789	26.977	28.128	28.520	28.603	28.544	28.471	28.475	28.089	27.213	26.794	
1.307 192 0 25.117	24.385	24.869	25.607	26.831	27.315	27.288	27.201	27.135	27.195	27.432	26.563	26.229	
1.439 194 0 25.120	24.386	24.715	25.364	26.486	27.126	27.018	27.037	27.196	27.520	27.269	26.561	25.854	

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.93X10 FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 136 0	8.156	10.810	13.870	14.879	19.274	30.673	34.651	35.873	36.623	38.003	40.439	42.364	42.514
.438 132 0	8.225	11.469	17.795	20.019	28.617	35.847	37.359	37.177	37.383	38.386	39.947	40.670	40.539
.495 136 0	9.303	17.087	25.751	31.119	36.382	37.693	37.305	36.652	36.265	35.750	35.073	34.412	33.683
.571 196 0	15.027	6.472	22.179	31.603	34.807	35.348	34.728	34.235	34.382	34.452	34.684	34.670	34.814
.711 190 0	4.783	14.083	26.652	32.666	34.215	34.018	32.998	32.601	32.952	32.944	32.511	32.420	32.055
.841 216 0	10.422	18.190	26.786	30.107	30.974	31.217	31.234	31.170	31.484	31.899	30.720	29.904	29.932
.961 210 0	15.402	20.222	26.458	28.707	29.484	29.861	29.696	29.766	30.337	30.012	29.264	29.076	28.659
1.055 210 0	19.897	24.720	26.846	29.085	29.782	29.916	29.984	29.904	29.826	29.695	29.536	28.954	27.666
1.221 216 0	24.793	24.163	25.711	27.075	28.346	28.608	28.864	28.904	28.817	28.706	28.797	28.183	26.750
1.307 190 0	24.657	24.396	24.864	25.644	26.916	27.859	28.032	27.778	27.730	27.924	27.994	27.079	26.911
1.439 196 0	24.688	24.100	24.848	25.728	26.938	27.781	27.947	28.023	28.121	28.052	27.862	27.637	27.872

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.91X10 FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 198 0	7.423	9.871	24.495	36.498	28.136	21.367	18.335	23.618	28.551	31.568	34.111	35.867	36.348
.641 204 0	4.840	6.310	13.798	13.666	8.192	9.395	15.726	19.357	22.481	25.272	27.272	28.697	29.857
.711 188 0	11.993	6.949	18.585	23.390	22.745	24.500	24.346	24.606	25.245	26.829	28.314	29.690	31.034
.838 182 0	6.123	10.275	23.065	27.577	27.627	26.303	25.746	25.863	25.985	26.608	27.588	28.105	28.600
.966 180 1	7.329	16.371	22.385	24.977	26.093	26.101	26.185	26.542	26.566	26.706	27.270	27.427	27.608
1.047 180 1	11.355	18.367	23.082	25.146	26.116	26.218	26.475	27.146	27.860	28.123	28.197	27.982	26.566
1.173 182 0	16.622	19.057	21.652	23.427	25.029	25.924	26.181	26.632	27.148	27.689	27.649	27.212	25.897
1.307 188 0	18.912	21.099	22.329	23.587	24.956	25.688	26.199	26.565	26.890	27.422	27.563	27.206	26.106
1.439 198 0	20.941	21.474	22.565	23.802	25.112	26.104	26.506	27.112	27.378	27.412	27.610	27.567	25.890

LOCAL FLOW FIELD DATA

MACH = .802 $RZ = 7.95 \times 10^4$ FT $\alpha = 24.580$ $X/D = 6.500$ TEST NO. = 39

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.971 200 0	5.646	5.647	6.057	6.058	5.760	11.290	27.466	30.317	31.588	34.222	36.427	36.132	39.253
.841 202 0	4.019	3.342	6.778	14.911	21.267	27.713	29.007	29.141	29.361	29.353	29.786	31.539	32.923
.711 186 0	8.332	2.303	9.729	16.595	19.114	25.696	28.925	28.937	30.127	31.499	32.827	33.922	34.701
.636 184 0	4.694	2.192	13.606	23.945	24.915	25.435	25.397	27.185	28.252	29.418	30.097	30.728	31.682
.966 178 0	3.730	3.488	16.591	24.480	24.960	26.442	26.415	26.667	27.404	28.256	28.833	29.164	29.832
1.047 178 0	6.779	30.050	24.949	24.783	26.055	27.351	28.169	28.550	29.280	29.068	28.736	28.799	28.618
1.175 184 0	1.075	19.648	23.469	24.142	25.199	26.384	27.148	27.492	28.274	28.518	28.231	28.321	28.094
1.307 186 0	4.169	14.252	23.927	24.884	25.199	26.162	26.723	27.289	28.215	28.217	27.638	27.502	27.404
1.439 200 0	11.989	19.316	22.925	25.103	25.675	26.399	26.777	27.238	27.706	27.992	27.672	27.359	26.941

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.94X10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 116 0	180.0	-129.0	-76.3	-69.6	-66.6	-8.2	48.3	67.6	71.0	76.3	80.4	83.5	85.9
.395 120 0	180.0	-122.7	-81.1	-24.2	26.0	51.5	56.5	61.7	66.4	70.9	77.0	81.0	85.1
.438 116 0	180.0	-138.4	-54.2	-4.3	29.7	40.7	46.7	54.1	61.4	68.0	74.4	80.7	86.0
.495 120 0	180.0	-172.1	37.4	29.4	32.0	37.1	41.6	46.9	52.6	60.0	67.5	74.5	80.8
.571 194 0	180.0	171.9	60.4	34.7	34.9	40.4	46.9	52.7	58.3	64.3	71.2	78.0	83.8
.711 192 0	.0	29.5	38.2	37.9	39.3	43.7	49.1	54.9	60.1	65.2	71.1	77.2	83.4
.841 214 0	.0	25.3	32.4	34.9	37.7	41.4	46.6	52.5	58.6	64.2	70.7	77.3	83.3
.961 212 0	.0	16.3	26.3	31.6	35.6	39.9	45.2	51.1	57.4	63.4	69.8	76.5	83.1
1.055 212 0	.0	21.2	26.9	32.8	37.8	42.8	47.9	53.7	59.6	65.8	71.8	78.0	84.6
1.221 214 0	.0	17.2	22.6	29.7	35.7	41.4	46.6	52.3	58.3	64.6	70.5	76.9	83.3
1.307 192 0	.0	14.4	20.6	28.4	34.0	40.0	45.9	52.3	58.9	65.7	72.5	78.6	84.1
1.439 194 0	.0	13.5	19.8	27.9	33.9	40.1	45.9	51.8	58.9	66.0	72.1	78.2	84.2

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.93x10 FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

CROSSFLOW DIRECTION (THETA) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 136 0	.0	-7.4	-18.6	-18.8	-7.2	27.1	49.3	54.3	60.3	65.4	69.6	71.7	72.0
.438 132 0	.0	-7.4	-19.9	-12.5	4.7	29.9	36.8	40.1	46.6	53.5	59.7	63.2	65.6
.495 136 0 180.0	-59.9	-14.3	10.5	25.5	30.8	34.7	39.7	42.9	46.8	50.7	54.4	61.2	
.571 196 0 -180.0	-107.8	-4.0	18.6	27.0	30.1	34.7	42.1	48.2	53.7	59.3	64.0	69.1	
.711 190 0 -180.0	59.2	35.1	32.9	31.2	34.5	40.1	44.8	49.7	55.9	61.4	66.4	72.1	
.841 216 0	.0	35.3	35.0	32.0	32.8	36.2	40.8	45.5	51.2	57.4	62.6	68.0	74.1
.961 210 0	.0	23.9	29.4	29.6	31.7	35.7	40.2	45.5	51.8	57.5	63.3	69.1	75.5
1.055 210 0	.0	24.5	28.4	32.1	36.6	41.5	46.0	50.7	55.9	61.1	66.8	72.6	78.9
1.221 216 0	.0	17.8	23.4	30.2	36.0	41.2	45.6	50.5	55.8	61.6	67.9	73.9	80.4
1.307 190 0	.0	14.5	21.0	28.7	34.1	39.6	45.2	51.4	57.4	63.5	69.5	75.2	81.5
1.439 196 0	.0	14.7	20.3	27.6	33.7	39.3	44.7	50.3	56.8	63.3	69.0	75.8	82.6

LOCAL FLOW FIELD DATA

+6 -1

MACH = .802 RE = 7.91X10 FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 198 0	180.0	-130.0	-124.9	-163.0	-178.0	-175.4	179.9	151.5	113.6	98.9	92.1	88.7	88.7
.641 204 0	180.0	-105.3	-59.3	-46.0	-29.8	24.9	54.8	69.5	76.0	79.2	81.9	84.4	86.8
.711 188 0	180.0	-141.4	-4.5	-2.1	12.4	33.4	44.4	54.6	64.1	71.9	78.1	82.4	85.2
.838 182 0	-180.0	62.3	34.4	34.2	36.1	39.7	46.1	54.3	61.5	67.7	74.4	79.6	83.7
.966 180 1	.0	42.0	37.8	36.6	38.0	41.7	47.1	53.3	59.7	66.1	72.1	77.9	82.9
1.047 180 1	.0	35.6	37.4	38.3	41.0	45.1	50.2	56.1	62.3	67.2	73.0	79.3	83.2
1.173 182 0	.0	26.0	30.9	35.9	39.7	44.3	49.4	54.9	60.7	66.4	71.8	78.0	83.6
1.307 188 0	.0	20.0	26.7	33.6	38.8	43.8	49.0	54.8	61.0	67.2	72.8	78.8	83.0
1.439 198 0	.0	16.7	24.5	31.8	37.5	42.9	48.4	54.2	60.3	66.1	72.2	78.3	82.9

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LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.93x10 FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

CROSSFLOW DIRECTION (THETA) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 200 0	180.0	-155.9	157.0	177.7	-133.2	32.2	59.5	74.2	80.2	82.7	84.4	86.0	87.1
.841 202 0	180.0	-84.3	67.7	79.4	80.0	70.0	63.5	62.7	67.0	72.5	77.8	83.4	87.1
.711 186 0	-180.0	-20.2	57.1	65.6	66.2	64.9	64.3	67.1	71.2	75.8	80.2	83.8	86.7
.838 184 0	180.0	172.9	38.7	46.5	50.8	53.8	58.1	63.2	66.2	70.6	76.5	81.7	85.6
.966 178 0	180.0	-48.9	20.6	39.0	41.6	47.5	52.6	56.9	62.6	68.7	74.8	80.4	84.9
1.047 178 0	-180.0	54.9	45.9	46.4	50.2	54.5	58.3	63.1	69.0	73.8	79.4	83.9	88.1
1.173 184 0	.0	52.3	43.2	44.0	48.2	52.4	58.0	62.7	67.6	72.8	78.2	83.0	88.4
1.307 186 0	.0	20.6	30.9	37.1	44.0	49.0	53.9	60.2	66.6	71.7	76.7	81.4	87.0
1.439 200 0	.0	34.7	33.5	35.1	39.9	45.3	51.3	57.7	63.9	69.9	75.7	81.0	86.6

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.94X10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 116 0	.032	.043	.034	.011	.014	.094	.190	.091	-.063	-.071	-.101	-.132	-.202
.395 120 0	-.013	-.001	.039	.038	.116	.120	.031	.019	-.015	-.058	-.089	-.091	-.069
.438 116 0	-.089	-.041	.030	.011	.049	.001	-.041	-.012	-.008	-.010	-.014	-.029	-.047
.495 120 0	-.153	-.143	-.068	-.073	-.020	-.007	-.009	-.013	-.008	-.020	-.046	-.070	-.087
.571 194 0	-.041	-.093	-.100	-.156	-.103	-.042	.018	.037	.023	.017	.016	.014	.033
.711 192 0	.145	.135	.083	.035	.014	.011	.025	.031	.014	.006	.008	.005	.032
.841 214 0	.105	.102	.088	.044	.016	.005	.016	.032	.018	.007	.016	.016	.035
.961 212 0	.087	.086	.066	.038	.017	-.003	-.002	.015	.014	.005	.013	.017	.034
1.055 212 0	.081	.052	.041	.042	.050	.044	.041	.042	.039	.044	.045	.035	.044
1.221 214 0	.051	.011	.020	.024	.036	.038	.039	.041	.042	.050	.051	.034	.044
1.307 192 0	.013	-.009	.006	.004	.011	.027	.028	.022	.020	.027	.040	.020	.039
1.439 194 0	.004	-.017	-.006	-.005	.001	.014	.020	.020	.027	.039	.037	.021	.034

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.93X10 FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 136 0	.122	.139	.083	.019	.110	.183	.087	.084	.045	.011	.019	.055	.054
.438 132 0	.106	.101	.046	-.038	.049	.005	-.074	-.078	-.090	-.080	-.006	.040	.054
.495 136 0	-.081	-.060	-.082	-.018	-.077	-.125	-.104	-.090	-.079	-.068	-.032	.013	.017
.571 196 0	-.153	-.096	-.085	-.119	-.182	-.172	-.117	-.086	-.058	-.030	.005	.042	.073
.711 190 0	-.109	-.108	-.128	-.226	-.265	-.225	-.142	-.093	-.059	-.029	-.015	.021	.048
.841 216 0	.004	-.039	-.108	-.144	-.147	-.131	-.116	-.099	-.059	-.003	-.019	-.017	.022
.961 210 0	-.042	-.037	-.085	-.118	-.124	-.110	-.114	-.098	-.050	-.039	-.046	-.020	.007
1.055 210 0	-.021	-.005	-.049	-.042	-.055	-.060	-.054	-.043	-.041	-.028	-.009	.004	.003
1.221 216 0	-.031	-.074	-.075	-.077	-.067	-.072	-.064	-.049	-.042	-.028	.001	.008	-.017
1.307 190 0	-.066	-.090	-.083	-.083	-.074	-.052	-.050	-.055	-.053	-.035	-.016	-.028	.012
1.439 196 0	-.063	-.076	-.078	-.071	-.054	-.031	-.027	-.020	-.008	-.007	.001	.016	.064

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.91X10⁶ FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 198 0	-1.008	-.828	-.534	-.615	-.626	-.548	-.515	-.480	-.410	-.838	-.836	-.712	-.667
.641 204 0	-.691	-.684	-.881	-.763	-.876	-.779	-.857	-.976	-.904	-.781	-.702	-.665	-.645
.711 188 0	-.626	-.532	-.625	-.793	-.507	-.532	-.618	-.600	-.601	-.590	-.585	-.564	-.521
.838 182 0	-.507	-.452	-.530	-.624	-.549	-.488	-.479	-.465	-.478	-.483	-.485	-.475	-.426
.966 180 1	-.133	-.235	-.336	-.375	-.392	-.396	-.373	-.358	-.370	-.383	-.371	-.367	-.331
1.047 180 1	-.106	-.143	-.210	-.247	-.214	-.200	-.205	-.185	-.161	-.170	-.187	-.210	-.260
1.173 182 0	-.087	-.123	-.133	-.168	-.172	-.160	-.158	-.152	-.142	-.131	-.135	-.149	-.199
1.307 188 0	-.065	-.094	-.109	-.132	-.140	-.132	-.125	-.126	-.125	-.112	-.112	-.114	-.122
1.439 198 0	-.069	-.078	-.086	-.105	-.099	-.083	-.087	-.077	-.076	-.074	-.074	-.066	-.088

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.93X10⁴ ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 200 0	.033	.025	.009	-.043	-.113	-.143	-.018	-.038	-.390	-.553	-.588	-.648	-.671
.641 202 0	.007	.002	-.005	-.075	-.119	-.187	-.217	-.221	-.254	-.305	-.391	-.511	-.580
.711 186 0	.025	.014	.043	.033	-.007	-.099	-.139	-.133	-.136	-.196	-.252	-.299	-.340
.838 184 0	.006	.020	.030	-.010	-.026	-.036	-.046	-.088	-.107	-.110	-.129	-.130	-.114
.966 178 0	-.005	.030	.042	.007	-.014	-.022	-.037	-.053	-.085	-.097	-.115	-.119	-.090
1.047 178 0	-.079	-.019	.058	-.022	-.037	-.040	-.049	-.058	-.056	-.095	-.141	-.142	-.113
1.173 164 0	-.058	-.020	.045	-.021	-.029	-.027	-.039	-.049	-.047	-.071	-.103	-.106	-.106
1.307 166 0	.017	-.009	.031	-.008	-.026	-.025	-.031	-.042	-.037	-.055	-.085	-.088	-.090
1.439 200 0	.073	-.007	.002	-.015	-.009	-.001	-.005	-.008	-.013	-.023	-.044	-.061	-.063

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.94x10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 116 0	1.000	.998	.998	.996	.977	.916	.891	.961	.992	.997	1.001	1.008	1.008
.395 120 0	.991	.939	.940	.961	.938	.928	.997	1.003	.998	.995	.990	.989	.990
.438 116 0	.978	.928	.904	.959	.965	.982	.998	1.003	1.002	1.000	.999	.992	.991
.495 120 0	1.002	.860	.852	.959	1.001	1.009	1.009	1.003	.993	.984	.979	.979	.987
.571 194 0	1.014	.897	.815	.928	1.002	1.006	1.016	1.017	1.008	1.001	1.000	.996	1.001
.711 192 0	.996	.988	.991	1.001	1.004	1.006	1.011	1.012	1.007	1.002	1.003	1.000	1.004
.841 214 0	1.001	.991	.996	1.006	1.007	1.006	1.010	1.015	1.010	1.005	1.005	1.001	1.002
.961 212 0	1.002	1.004	1.006	1.006	1.006	1.004	1.007	1.010	1.009	1.005	1.004	1.002	1.001
1.055 212 0	1.001	1.003	1.006	1.008	1.013	1.013	1.013	1.014	1.014	1.015	1.012	1.009	1.010
1.221 214 0	1.002	.999	1.005	1.007	1.011	1.013	1.013	1.014	1.015	1.015	1.014	1.009	1.010
1.307 192 0	1.003	1.001	1.002	1.003	1.008	1.012	1.012	1.010	1.009	1.010	1.014	1.008	1.006
1.439 194 0	1.003	1.001	1.001	1.003	1.008	1.012	1.012	1.010	1.012	1.015	1.015	1.009	1.005

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.93x10 FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 136 0	.966	.977	.996	1.007	.954	.903	.967	.996	.987	.981	.985	.993	.997
.438 132 0	.953	.954	.980	1.000	.944	.954	.999	1.004	.998	.999	1.007	.999	.994
.495 136 0	.918	.882	.931	.957	.975	1.003	1.012	1.014	1.006	.996	.983	.967	.964
.571 196 0	.936	.869	.897	.955	.983	1.001	1.005	1.006	1.009	1.008	1.005	1.001	1.003
.711 190 0	.962	.924	.943	.988	1.003	1.002	1.004	1.007	1.012	1.012	1.006	1.006	1.003
.841 216 0	.988	.984	.991	1.000	1.003	1.007	1.007	1.008	1.012	1.020	1.009	1.003	1.007
.961 210 0	.992	.991	.996	1.002	1.003	1.005	1.003	1.006	1.014	1.011	1.004	1.005	1.004
1.055 210 0	1.005	.987	1.006	1.010	1.012	1.011	1.010	1.011	1.013	1.013	1.014	1.014	1.007
1.221 216 0	1.003	.999	1.002	1.004	1.007	1.008	1.009	1.010	1.010	1.012	1.016	1.015	1.004
1.307 190 0	1.001	.999	.999	1.001	1.006	1.010	1.010	1.008	1.007	1.009	1.011	1.007	1.007
1.439 196 0	1.003	1.001	1.003	1.007	1.012	1.015	1.015	1.015	1.016	1.015	1.015	1.016	1.021

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.91X10 FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 198 0	.927	.845	.645	.525	.516	.563	.609	.612	.811	1.019	1.033	1.014	1.016
.641 204 0	.962	.948	.901	.751	.755	.876	.982	1.016	1.009	1.000	.996	.993	.992
.711 188 0	.969	.863	.849	.949	.956	.982	1.004	1.001	1.000	1.004	1.003	1.006	1.013
.838 182 0	.973	.939	.937	.981	1.006	1.005	1.003	1.004	1.002	1.001	1.002	1.001	1.004
.966 180 1	.993	.997	1.001	1.003	1.004	1.003	1.004	1.006	1.003	1.001	1.003	1.001	1.000
1.047 180 1	1.001	.995	1.005	1.008	1.010	1.010	1.010	1.013	1.015	1.016	1.016	1.013	1.000
1.173 182 0	1.002	1.001	1.004	1.005	1.008	1.009	1.009	1.010	1.012	1.016	1.015	1.012	1.001
1.307 188 0	.991	.998	1.000	1.000	1.004	1.006	1.008	1.007	1.006	1.011	1.012	1.010	1.001
1.439 198 0	1.003	1.001	1.004	1.007	1.011	1.014	1.014	1.015	1.014	1.013	1.015	1.017	1.003

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.93x10 FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 200 0	.818	.816	.838	.848	.782	.727	.793	.923	.985	.997	1.006	1.010	1.013
.641 202 0	.835	.822	.857	.891	.889	.908	.954	.973	.977	.977	.974	.975	.981
.711 186 0	.856	.826	.862	.947	.990	.997	.999	1.000	1.001	.998	.999	1.005	1.008
.838 184 0	.873	.883	.896	.961	1.000	1.003	1.002	1.000	.999	1.001	.998	1.000	1.007
.966 178 0	.926	.889	.861	.939	.994	1.009	1.010	1.006	1.003	1.003	1.001	1.001	1.008
1.047 178 0	.933	.771	.913	1.005	1.011	1.012	1.012	1.012	1.016	1.011	1.002	1.001	1.001
1.173 164 0	1.029	.804	.917	1.001	1.007	1.008	1.007	1.007	1.011	1.009	1.003	1.002	1.001
1.307 166 0	1.018	.877	.890	.995	1.011	1.009	1.009	1.009	1.012	1.010	1.004	1.005	1.000
1.439 200 0	.999	.976	.969	1.011	1.013	1.015	1.014	1.014	1.013	1.014	1.011	1.006	1.004

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.94x10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VINF) --

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 116 0	-.040	-.017	.016	.028	.032	.103	.171	.173	.166	.133	.101	.073	.049
.395 120 0	-.232	-.149	.023	.153	.172	.246	.271	.241	.210	.178	.124	.088	.048
.438 116 0	-.311	-.166	.121	.268	.329	.371	.355	.308	.254	.201	.147	.087	.038
.493 120 0	-.410	-.254	.224	.468	.465	.437	.400	.352	.301	.241	.181	.127	.077
.571 194 0	-.355	-.316	.136	.469	.477	.415	.364	.320	.271	.219	.163	.103	.055
.711 192 0	.170	.221	.300	.354	.365	.348	.322	.286	.247	.206	.160	.108	.056
.841 214 0	.250	.266	.327	.365	.371	.359	.336	.302	.255	.209	.158	.104	.055
.961 212 0	.329	.338	.359	.373	.372	.358	.334	.302	.259	.212	.162	.107	.055
1.055 212 0	.374	.356	.371	.378	.372	.350	.321	.284	.243	.196	.147	.095	.042
1.221 214 0	.419	.395	.400	.392	.381	.357	.328	.291	.249	.203	.156	.103	.052
1.307 192 0	.423	.402	.393	.381	.375	.352	.319	.280	.235	.188	.138	.089	.043
1.439 194 0	.425	.405	.395	.381	.373	.351	.317	.281	.236	.187	.141	.092	.044

LOCAL FLOW FIELD DATA

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MACH = .799 RE = 7.93X10 FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 136 0	.127	.168	.217	.243	.290	.348	.340	.326	.285	.249	.220	.204	.203
.438 132 0	.127	.176	.274	.341	.432	.478	.503	.482	.435	.384	.327	.288	.259
.495 136 0	-.152	.130	.405	.488	.541	.560	.530	.486	.453	.412	.363	.314	.253
.571 196 0	-.261	-.030	.345	.502	.546	.544	.497	.438	.391	.343	.292	.244	.197
.711 190 0	-.084	.120	.367	.498	.545	.513	.448	.403	.367	.313	.260	.214	.160
.841 216 0	.178	.255	.385	.456	.465	.448	.418	.383	.341	.292	.240	.189	.137
.961 210 0	.269	.319	.403	.443	.446	.429	.401	.367	.325	.277	.226	.176	.120
1.055 210 0	.346	.376	.410	.425	.415	.389	.360	.326	.289	.246	.198	.147	.090
1.221 216 0	.427	.404	.414	.410	.400	.376	.352	.319	.280	.234	.184	.133	.076
1.307 190 0	.432	.418	.408	.396	.391	.373	.343	.301	.259	.215	.168	.119	.067
1.439 196 0	.432	.410	.411	.401	.392	.372	.343	.308	.264	.216	.170	.115	.060

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.91x10⁶ FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 198 0	-.187	-.141	-.188	-.291	-.227	-.204	-.214	-.231	-.189	-.115	-.029	.018	.018
.641 204 0	-.110	-.037	.165	.186	.150	.189	.220	.172	.134	.111	.086	.061	.036
.711 188 0	-.266	-.107	.370	.535	.456	.430	.384	.312	.241	.181	.126	.084	.054
.838 182 0	-.131	.096	.389	.493	.476	.423	.372	.313	.258	.210	.154	.105	.064
.966 180 1	.135	.233	.351	.402	.414	.393	.356	.316	.267	.216	.167	.114	.066
1.047 180 1	.208	.273	.345	.376	.370	.346	.317	.281	.238	.201	.153	.097	.060
1.173 182 0	.299	.312	.338	.350	.356	.341	.312	.280	.242	.201	.157	.103	.054
1.307 188 0	.332	.354	.358	.355	.353	.335	.310	.276	.235	.190	.146	.095	.057
1.439 198 0	.371	.364	.365	.363	.357	.340	.314	.281	.240	.196	.149	.098	.056

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.93x10 FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 200 0	-.071	-.064	-.074	-.115	-.051	.107	.163	.127	.105	.091	.074	.057	.043
.641 202 0	-.053	.004	.047	.043	.058	.157	.229	.242	.211	.166	.123	.073	.035
.711 186 0	-.073	.028	.072	.108	.131	.192	.224	.200	.173	.141	.103	.070	.038
.838 184 0	-.068	-.032	.156	.268	.270	.259	.233	.215	.201	.172	.124	.078	.043
.966 178 0	-.059	.034	.210	.297	.316	.307	.278	.253	.221	.181	.134	.087	.046
1.047 178 0	-.114	.186	.251	.294	.290	.276	.257	.225	.183	.143	.095	.055	.017
1.173 184 0	.020	.149	.253	.298	.290	.277	.248	.218	.187	.146	.102	.061	.014
1.307 186 0	.074	.194	.292	.335	.314	.296	.271	.235	.194	.154	.113	.073	.025
1.439 200 0	.200	.265	.313	.354	.341	.318	.286	.249	.209	.166	.120	.074	.028

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.94X10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 116 0	.000	-.021	-.067	-.076	-.074	-.015	.192	.420	.483	.545	.597	.643	.678
.395 120 0	.000	-.232	-.143	-.069	.084	.309	.410	.447	.479	.516	.536	.554	.557
.438 116 0	.000	-.147	-.168	-.020	.187	.320	.376	.426	.466	.496	.524	.532	.542
.495 120 0	.000	-.035	.172	.263	.290	.330	.355	.376	.393	.417	.438	.458	.478
.571 194 0	.000	.045	.240	.325	.333	.353	.389	.421	.439	.454	.478	.487	.500
.711 192 0	.000	.125	.236	.276	.299	.333	.371	.407	.430	.446	.466	.474	.481
.841 214 0	-.000	.126	.207	.255	.287	.317	.354	.393	.418	.434	.452	.461	.464
.961 212 0	.000	.099	.177	.229	.266	.300	.337	.374	.404	.424	.441	.448	.451
1.055 212 0	.000	.138	.188	.244	.289	.325	.355	.387	.413	.436	.446	.448	.449
1.221 214 0	.000	.122	.166	.224	.273	.315	.346	.377	.404	.427	.440	.442	.443
1.307 192 0	.000	.103	.148	.206	.254	.295	.329	.362	.391	.416	.437	.438	.434
1.439 194 0	.000	.097	.142	.201	.251	.295	.327	.358	.391	.421	.435	.438	.429

LOCAL FLOW FIELD DATA

*6 -1

MACH = .799 RE = 7.93×10^6 FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 136 0	.000	-.022	-.073	-.083	-.036	.178	.395	.453	.498	.545	.592	.617	.623
.438 132 0	-.000	-.023	-.099	-.076	.035	.275	.377	.406	.460	.519	.560	.569	.572
.495 136 0	.000	-.224	-.103	.090	.258	.333	.367	.404	.421	.439	.443	.438	.461
.571 196 0	-.000	-.095	-.024	.169	.278	.315	.345	.395	.437	.467	.491	.501	.515
.711 190 0	-.000	.202	.258	.322	.330	.353	.377	.400	.432	.462	.479	.490	.495
.841 216 0	.000	.181	.270	.285	.300	.328	.361	.391	.424	.456	.462	.468	.478
.961 210 0	-.000	.141	.227	.252	.276	.308	.339	.373	.412	.435	.449	.461	.465
1.055 210 0	.000	.171	.221	.267	.308	.344	.373	.399	.426	.446	.462	.468	.459
1.221 216 0	.000	.129	.179	.239	.290	.330	.359	.386	.411	.434	.454	.460	.449
1.307 190 0	.000	.108	.157	.216	.265	.309	.345	.377	.405	.430	.449	.449	.448
1.439 196 0	.000	.108	.152	.210	.261	.305	.340	.371	.403	.429	.443	.454	.460

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.91x10 FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 198 0	.000	-.168	-.269	-.089	-.008	-.016	.000	.126	.433	.735	.807	.795	.793
.641 204 0	.000	-.137	-.278	-.193	-.086	.088	.311	.462	.537	.578	.607	.630	.650
.711 188 0	.000	-.085	-.029	-.020	.101	.284	.376	.439	.496	.554	.597	.628	.649
.838 182 0	-.000	.184	.266	.336	.348	.351	.387	.436	.475	.512	.552	.571	.576
.966 180 1	-.000	.210	.272	.299	.323	.350	.383	.423	.457	.488	.516	.531	.534
1.047 180 1	.000	.196	.264	.297	.322	.347	.380	.418	.453	.478	.501	.515	.501
1.173 182 0	.000	.152	.203	.253	.296	.332	.364	.398	.431	.460	.477	.486	.477
1.307 188 0	.000	.129	.180	.236	.284	.321	.357	.391	.422	.453	.472	.478	.464
1.439 198 0	.000	.110	.166	.225	.274	.316	.353	.389	.420	.442	.464	.476	.453

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.93X10⁴ FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (V_{THETA}/V_{INF})

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 200 0	.000	-.029	.032	.005	-.055	.067	.277	.450	.607	.707	.763	.815	.844
.641 202 0	.000	-.043	.114	.229	.331	.432	.460	.468	.497	.527	.567	.638	.687
.711 186 0	-.000	-.010	.111	.239	.297	.411	.466	.475	.508	.554	.600	.638	.667
.838 184 0	.000	.004	.125	.282	.331	.354	.373	.426	.456	.489	.518	.538	.557
.966 178 0	.000	-.038	.079	.240	.281	.335	.363	.388	.427	.464	.492	.509	.522
1.047 178 0	-.000	.264	.259	.309	.348	.386	.417	.444	.477	.494	.507	.513	.511
1.173 184 0	.000	.192	.237	.287	.325	.360	.397	.423	.453	.473	.488	.497	.496
1.307 186 0	.000	.073	.174	.254	.303	.340	.373	.410	.448	.466	.476	.479	.480
1.439 200 0	.000	.184	.207	.249	.285	.321	.358	.394	.426	.453	.468	.471	.468

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.94X10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

(VC / VINF * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 116 0	.096	.066	.166	.196	.193	.249	.618	1.091	1.228	1.348	1.456	1.555	1.634
.395 120 0	.557	.662	.349	.403	.459	.949	1.182	1.220	1.257	1.313	1.323	1.347	1.345
.438 116 0	.748	.534	.496	.647	.910	1.177	1.244	1.264	1.276	1.287	1.307	1.297	1.305
.495 120 0	.985	.616	.679	1.291	1.319	1.317	1.285	1.238	1.189	1.159	1.140	1.142	1.165
.571 194 0	.854	.767	.663	1.371	1.398	1.310	1.281	1.271	1.239	1.213	1.214	1.198	1.209
.711 192 0	.409	.611	.918	1.078	1.134	1.159	1.181	1.195	1.191	1.182	1.183	1.168	1.163
.841 214 0	.601	.709	.930	1.071	1.127	1.151	1.173	1.192	1.177	1.158	1.151	1.136	1.123
.961 212 0	.791	.845	.963	1.052	1.100	1.122	1.141	1.155	1.155	1.139	1.130	1.107	1.092
1.055 212 0	.900	.919	1.000	1.081	1.132	1.148	1.151	1.154	1.153	1.148	1.128	1.102	1.084
1.221 214 0	1.006	.995	1.041	1.086	1.127	1.143	1.145	1.143	1.141	1.137	1.121	1.092	1.072
1.307 192 0	1.017	.998	1.010	1.040	1.089	1.103	1.101	1.099	1.097	1.097	1.102	1.074	1.050
1.439 194 0	1.022	1.002	1.009	1.035	1.082	1.103	1.096	1.094	1.098	1.108	1.099	1.075	1.036

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.93x10 FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

(VC / VIN * SIN ALPHA)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 136 0	.305	.406	.549	.616	.702	.939	1.252	1.342	1.380	1.441	1.517	1.562	1.574
.438 132 0	.305	.428	.700	.839	1.042	1.327	1.511	1.515	1.522	1.551	1.560	1.534	1.509
.495 136 0	.366	.622	1.004	1.192	1.441	1.566	1.550	1.520	1.486	1.447	1.376	1.297	1.265
.571 196 0	.628	.239	.833	1.272	1.472	1.510	1.456	1.418	1.409	1.392	1.373	1.341	1.326
.711 190 0	.203	.565	1.079	1.427	1.531	1.497	1.406	1.364	1.363	1.343	1.310	1.284	1.250
.841 216 0	.428	.752	1.131	1.292	1.331	1.335	1.328	1.316	1.309	1.301	1.252	1.213	1.196
.961 210 0	.647	.838	1.112	1.225	1.260	1.269	1.262	1.258	1.262	1.239	1.207	1.186	1.154
1.055 210 0	.831	.993	1.119	1.206	1.242	1.249	1.247	1.238	1.237	1.225	1.208	1.179	1.124
1.221 216 0	1.027	1.019	1.084	1.141	1.187	1.202	1.209	1.203	1.196	1.186	1.178	1.150	1.096
1.307 190 0	1.038	1.037	1.051	1.084	1.136	1.165	1.170	1.160	1.156	1.156	1.151	1.117	1.090
1.439 196 0	1.039	1.020	1.053	1.088	1.132	1.156	1.160	1.159	1.158	1.154	1.141	1.126	1.115

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.91x10⁶ FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

(VC / VINP * SIN ALPHAINP)

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 198 0	.449	.527	.788	.732	.545	.493	.514	.633	1.137	1.789	1.941	1.911	1.906
.641 204 0	.265	.341	.778	.644	.415	.502	.915	1.186	1.330	1.416	1.474	1.521	1.564
.711 188 0	.640	.328	.891	1.288	1.122	1.240	1.292	1.294	1.325	1.400	1.467	1.523	1.567
.838 182 0	.314	.499	1.132	1.434	1.418	1.322	1.291	1.290	1.300	1.331	1.378	1.395	1.393
.966 180 1	.324	.754	1.067	1.204	1.263	1.265	1.258	1.268	1.273	1.283	1.304	1.306	1.294
1.047 180 1	.499	.808	1.045	1.153	1.180	1.177	1.191	1.211	1.230	1.246	1.259	1.259	1.213
1.173 182 0	.719	.834	.949	1.040	1.112	1.144	1.153	1.169	1.187	1.207	1.207	1.194	1.154
1.307 188 0	.797	.905	.963	1.025	1.089	1.117	1.136	1.150	1.162	1.181	1.188	1.173	1.123
1.439 198 0	.892	.915	.965	1.028	1.082	1.116	1.135	1.155	1.164	1.162	1.172	1.169	1.098

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.93X10 FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

(VC / VINF * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.371 200 0	.170	.169	.194	.276	.180	.304	.772	1.124	1.481	1.714	1.843	1.963	2.032
.641 202 0	.128	.104	.296	.559	.808	1.106	1.235	1.267	1.299	1.328	1.394	1.543	1.655
.711 186 0	.176	.071	.319	.630	.781	1.090	1.242	1.239	1.289	1.374	1.464	1.544	1.606
.838 184 0	.163	.077	.479	.936	1.026	1.055	1.057	1.147	1.197	1.246	1.280	1.308	1.344
.966 178 0	.143	.123	.540	.918	1.015	1.093	1.100	1.115	1.157	1.197	1.226	1.242	1.260
1.047 178 0	.273	.775	.868	1.025	1.088	1.141	1.177	1.197	1.228	1.236	1.239	1.241	1.229
1.173 184 0	.048	.584	.834	.995	1.047	1.092	1.127	1.145	1.179	1.191	1.199	1.203	1.193
1.307 186 0	.177	.499	.817	1.010	1.048	1.084	1.108	1.136	1.173	1.180	1.175	1.164	1.156
1.439 200 0	.480	.776	.902	1.040	1.069	1.087	1.102	1.121	1.142	1.159	1.162	1.145	1.127

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.94x10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 116 0	.983	.976	.978	.987	.964	.834	.695	.784	.885	.866	.859	.857	.874
.395 120 0	.969	.887	.895	.920	.838	.745	.848	.854	.859	.866	.875	.868	.857
.438 116 0	.972	.908	.836	.907	.853	.847	.878	.862	.855	.851	.847	.849	.855
.495 120 0	.997	.863	.789	.833	.849	.853	.862	.868	.864	.868	.879	.894	.909
.571 194 0	.972	.867	.746	.820	.877	.871	.856	.849	.854	.855	.854	.854	.847
.711 192 0	.906	.881	.867	.875	.879	.878	.871	.866	.869	.870	.869	.872	.861
.841 214 0	.915	.890	.869	.878	.883	.883	.877	.869	.874	.878	.875	.873	.867
.961 212 0	.900	.895	.887	.886	.887	.892	.889	.881	.881	.884	.881	.881	.874
1.055 212 0	.885	.900	.895	.880	.870	.871	.872	.872	.873	.873	.873	.881	.881
1.221 214 0	.883	.903	.896	.888	.877	.875	.874	.874	.875	.872	.874	.883	.883
1.307 192 0	.903	.916	.906	.903	.895	.888	.888	.890	.890	.888	.883	.893	.886
1.439 194 0	.907	.919	.912	.908	.903	.896	.894	.892	.889	.884	.887	.894	.890

LOCAL FLOW FIELD DATA

MACH = .799 RE = 7.93x10⁶ FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

AXIAL VELOCITY RATIO -- (VX / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 136 0	.885	.885	.926	.965	.836	.658	.754	.772	.772	.767	.741	.712	.714
.438 132 0	.877	.873	.907	.958	.795	.764	.823	.831	.829	.814	.775	.743	.734
.495 136 0	.931	.841	.866	.821	.814	.843	.846	.850	.843	.836	.815	.788	.789
.571 196 0	.972	.877	.849	.860	.881	.885	.873	.867	.857	.844	.825	.806	.793
.711 190 0	1.008	.937	.894	.926	.937	.922	.901	.887	.875	.862	.855	.841	.830
.841 216 0	.968	.952	.932	.927	.922	.917	.911	.905	.889	.869	.876	.877	.864
.961 210 0	.976	.947	.930	.930	.927	.919	.921	.915	.897	.892	.896	.887	.878
1.055 210 0	.955	.897	.919	.901	.903	.903	.899	.896	.897	.893	.887	.887	.892
1.221 216 0	.925	.945	.937	.928	.916	.917	.912	.907	.904	.901	.891	.893	.904
1.307 190 0	.940	.951	.944	.939	.930	.916	.914	.916	.915	.908	.901	.909	.893
1.439 196 0	.940	.949	.946	.940	.926	.913	.910	.906	.901	.901	.898	.895	.877

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.91x10⁶ FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 198 0	1.434	1.261	.719	.411	.424	.524	.646	.602	.869	1.211	1.192	1.099	1.077
.641 204 0	1.302	1.283	1.317	1.102	1.199	1.261	1.352	1.404	1.337	1.248	1.189	1.156	1.134
.711 188 0	1.253	1.121	1.103	1.239	1.113	1.132	1.188	1.176	1.169	1.151	1.133	1.111	1.083
.838 182 0	1.218	1.144	1.106	1.142	1.127	1.113	1.113	1.107	1.109	1.105	1.097	1.087	1.063
.966 180 1	1.049	1.067	1.078	1.075	1.073	1.074	1.064	1.056	1.059	1.061	1.052	1.047	1.030
1.047 180 1	1.033	1.012	1.020	1.022	1.001	.994	.994	.983	.968	.970	.977	.986	1.009
1.173 182 0	1.002	1.004	.994	.998	.990	.979	.975	.970	.963	.957	.958	.966	.989
1.307 188 0	.968	.975	.975	.977	.973	.966	.960	.957	.953	.947	.947	.949	.953
1.439 198 0	.970	.967	.966	.969	.960	.948	.946	.938	.935	.932	.932	.931	.941

LOCAL FLOW FIELD DATA

MACH = .802 RE = 7.93x10⁴ FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.571 200 0	.708	.711	.762	.810	.744	.633	.618	.800	1.002	1.048	1.039	1.040	1.034
.641 202 0	.759	.738	.798	.873	.863	.875	.927	.945	.960	.982	1.013	1.046	1.063
.711 186 0	.784	.739	.773	.880	.938	.943	.935	.932	.924	.933	.944	.955	.965
.838 184 0	.825	.834	.824	.877	.919	.922	.926	.929	.927	.919	.919	.915	.906
.966 178 0	.911	.837	.754	.839	.907	.914	.921	.923	.928	.926	.927	.926	.914
1.047 178 0	.956	.957	.776	.923	.926	.917	.914	.915	.911	.925	.940	.939	.937
1.173 184 0	1.061	.681	.799	.924	.925	.916	.914	.915	.912	.920	.929	.929	.930
1.307 186 0	1.009	.818	.766	.906	.927	.918	.916	.916	.909	.914	.925	.930	.928
1.439 200 0	.941	.921	.887	.923	.917	.911	.908	.906	.904	.907	.914	.921	.923

LOCAL VORTICITY X 100.

*6 -1

MACH = .802 RE = 7.94x10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

THETA 176.25 168.75 161.25 153.75 146.25 138.75 131.25 123.75 116.25 108.75 101.25 93.75

R/D

.3550	-8.898	2.084	21.363	29.360	119.424	125.606	56.574	25.680	13.223	1.329	.238	-7.101
.4165	71.153	112.217	64.845	65.237	73.343	16.582	-8.588	-2.076	.213	-3.330	.505	1.709
.4665	63.749	253.178	219.904	106.292	42.978	5.211	-14.468	-26.193	-32.650	-34.286	-32.162	-23.618
.5330	48.313	195.925	136.314	32.294	9.918	10.327	14.755	15.883	13.726	12.870	12.855	13.323
.6410	22.313	92.233	63.317	7.430	-3.705	-.873	.725	1.225	1.994	.908	-.413	.941
.7760	10.400	19.996	14.438	7.973	3.710	1.713	.826	.264	.998	-.070	-.635	-.144
.9010	1.377	6.979	5.831	2.885	1.370	.499	-.669	-1.910	-.618	-.778	-1.518	-.860
1.0080	5.813	13.881	10.515	10.578	10.161	8.951	6.580	4.717	4.240	3.632	1.714	.901
1.1380	-3.272	2.120	1.373	1.536	.824	1.071	.383	.255	.018	.432	.147	.170
1.2640	-5.063	-3.158	-3.132	-2.011	-3.716	-3.655	-3.335	-2.908	-2.560	-.846	-.083	-.408
1.3730	-2.509	-.203	.358	2.607	1.583	.884	.523	.229	1.194	1.359	.881	1.022

LOCAL VORTICITY X 100.

MACH = .799 RE = 7.93x10 FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.4165	19.526	22.464	10.792	52.333	79.807	45.181	-2.695	-17.889	-8.312	-3.148	-.384	.198
.4665	20.428	25.461	63.655	118.936	86.826	27.827	5.232	-2.777	-20.380	-38.540	-45.394	-44.175
.5530	109.332	145.576	70.251	43.047	16.953	-4.381	-5.932	6.234	11.933	16.011	23.093	22.185
.6410	92.419	147.765	88.864	42.625	15.400	3.196	2.457	3.863	1.578	1.500	3.000	1.490
.7760	35.730	52.757	31.538	10.448	-.723	-4.302	.176	2.026	.107	-.148	-.431	-1.162
.9010	11.585	19.835	10.942	3.004	.199	-1.272	-1.234	-.773	-1.763	-2.054	-.040	-.601
1.0080	13.518	19.050	12.361	12.437	12.694	12.434	10.578	7.615	5.367	4.940	4.591	.989
1.1380	-.953	1.201	.674	.986	.446	1.141	.637	.453	.071	.101	.268	-.795
1.2640	-4.797	-3.510	-3.907	-3.165	-4.025	-2.471	-1.688	-.496	.053	.089	-.910	-.874
1.3730	-1.500	1.333	.737	2.397	1.843	.910	.021	.268	.793	.870	.868	2.318

LOCAL VORTICITY x 100.

MACH = .802 RE = 7.91x10 FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.6060	21.167	19.727	-41.732	-31.843	14.224	81.206	114.539	95.185	22.115	-25.884	-32.346	-29.258
.6760	39.974	144.693	96.945	45.961	73.950	54.254	5.205	-9.142	-3.517	4.228	11.180	15.441
.7745	74.904	152.977	101.825	53.570	29.994	6.972	-2.096	-3.090	-2.903	-4.287	-2.377	-2.006
.9020	39.708	52.989	21.566	2.588	-.865	.439	-.883	-1.629	-1.102	-2.758	-3.217	-1.988
1.0065	15.850	20.471	13.382	7.891	3.210	1.922	1.539	.886	1.187	-.804	-2.365	-2.901
1.1100	4.359	2.718	-.975	-.458	-.211	.025	-.794	-1.657	-.378	-1.303	-3.503	-1.626
1.2400	1.940	1.455	1.356	2.852	1.609	1.082	1.154	.738	.929	1.519	.435	.879
1.3730	.322	-.117	1.059	2.087	1.594	1.638	1.678	1.343	.489	.235	.526	1.768

G

LOCAL VORTICITY X 100.

46 -1

MACH = .802 RE = 7.93X10 FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

THETA 176.25 168.75 161.25 153.75 146.25 138.75 131.25 123.75 116.25 108.75 101.25 93.75

R/D

.6960	6.611	16.033	51.636	126.556	182.503	130.729	49.411	-3.926	-36.949	-50.245	-48.452	-37.124
.6760	27.748	19.193	12.239	11.393	26.366	28.145	17.973	12.812	15.187	20.303	16.988	10.944
.7745	18.252	33.108	30.091	19.901	15.149	-1.087	-4.939	-.169	-2.821	-7.538	-9.268	-9.570
.9020	9.278	31.082	17.528	1.014	.238	1.232	1.738	.414	.153	-1.432	-.938	.410
1.0065	85.218	100.963	56.133	29.687	24.565	20.848	21.433	20.005	16.179	9.934	7.093	4.256
1.1100	32.308	10.759	9.373	1.656	.762	.221	.179	-.561	-.616	-.730	.841	1.027
1.2400	9.455	1.942	2.574	-1.544	.386	-.841	-.614	1.353	1.893	1.074	.615	-.578
1.3730	24.628	26.575	12.532	.500	-.616	-.707	-.979	-1.517	-.818	.492	1.257	.202

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = .802 RE = 7.94X10 FT ALPHA = 24.580 X/D = 3.500 TEST NO. = 35

THETA	176.25	166.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.3530	-.042	.010	.101	.139	.565	.595	.268	.122	.063	.006	.001	-.034	1.7934
.4165	.212	.335	.194	.195	.219	.049	-.026	-.006	.001	-.010	.002	.005	1.1695
.4665	.371	1.122	.975	.471	.190	.023	-.064	-.116	-.145	-.152	-.143	-.105	2.4283
.5330	.326	1.323	.920	.218	.067	.070	.100	.107	.093	.087	.087	.090	3.4871
.6410	.334	1.379	.947	.111	-.055	-.013	.011	.018	.030	.014	-.006	.014	2.7834
.7760	.175	.336	.243	.134	.062	.029	.014	.004	.017	-.001	-.011	-.002	.9999
.9010	.025	.126	.105	.052	.025	.009	-.012	-.034	-.011	-.014	-.027	-.016	.2268
1.0080	.092	.219	.166	.167	.160	.141	.104	.074	.067	.057	.027	.014	1.2899
1.1380	-.103	.067	.043	.048	.026	.034	.012	.008	.001	.014	.005	.005	.1592
1.2640	-.092	-.057	-.057	-.036	-.067	-.066	-.060	-.053	-.046	-.015	-.002	-.007	-.5594
1.3730	-.076	-.006	.011	.079	.048	.027	.016	.007	.036	.041	.027	.031	.2394
RSUM	1.222	4.854	3.648	1.578	1.240	.897	.362	.132	.104	.026	-.041	-.004	14.0175

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = .799 RE = 7.93x10 FT ALPHA = 24.580 X/D = 4.100 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.4165	.058	.067	.032	.156	.238	.135	-.008	-.053	-.025	-.009	-.001	.001	.5906
.4665	.091	.113	.282	.527	.385	.123	.023	-.012	-.090	-.171	-.201	-.196	.8735
.5330	.738	.983	.474	.291	.114	-.030	-.040	.042	.081	.108	.156	.150	3.0671
.6410	1.382	2.210	1.329	.638	.230	.048	.037	.058	.024	.022	.045	.022	6.0448
.7760	.601	.887	.530	.176	-.012	-.072	.003	.034	.002	-.002	-.007	-.020	2.1187
.9010	.209	.357	.197	.054	.004	-.023	-.022	-.014	-.032	-.037	-.001	-.011	.6817
1.0080	.213	.301	.195	.196	.200	.196	.167	.120	.085	.078	.072	.016	1.8409
1.1380	-.030	.038	.021	.031	.014	.036	.020	.014	.002	.003	.008	-.025	.1332
1.2640	-.087	-.064	-.071	-.057	-.073	-.045	-.031	-.009	.001	.002	-.016	-.016	-.4656
1.3730	-.045	.040	.022	.072	.056	.027	.001	.008	.024	.026	.026	.070	.3280
RSUM	3.130	4.933	3.013	2.084	1.156	.396	.150	.188	.071	.020	.081	-.009	15.2130

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = .802 RE = 7.91X10 FT ALPHA = 24.580 X/D = 4.800 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.6060	.150	.139	-.295	-.225	.101	.574	.810	.673	.156	-.183	-.229	-.207	1.4642
.6760	.315	1.141	.765	.362	.583	.428	.041	-.072	-.028	.033	.088	.122	3.7791
.7745	1.228	2.508	1.669	.878	.492	.114	-.034	-.051	-.048	-.070	-.039	-.033	6.6145
.9020	.764	1.020	.415	.050	-.017	.008	-.017	-.031	-.021	-.053	-.062	-.038	2.0176
1.0065	.215	.278	.182	.107	.044	.026	.021	.012	.016	-.011	-.032	-.039	.8189
1.1100	.102	.063	-.023	-.011	-.005	.001	-.019	-.039	-.009	-.030	-.082	-.038	-.0886
1.2400	.054	.040	.038	.079	.045	.030	.032	.020	.026	.042	.012	.024	.4416
1.3730	.010	-.004	.032	.063	.048	.049	.051	.041	.015	.007	.016	.053	.3812
RSUM	2.637	5.186	2.782	1.304	1.290	1.231	.885	.553	.108	-.265	-.327	-.156	15.4284

LOCAL CIRCULATION STRENGTH X 100.

MACH = .802 RE = 7.93X10 FT ALPHA = 24.580 X/D = 6.500 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.6060	.048	.127	.365	.895	1.290	.924	.349	-.028	-.261	-.355	-.343	-.262	2.7501
.6760	.219	.151	.097	.090	.208	.222	.142	.101	.120	.160	.134	.086	1.7295
.7745	.299	.543	.493	.326	.248	-.018	-.081	-.003	-.046	-.124	-.152	-.157	1.3297
.9020	.179	.598	.337	.020	.005	.024	.033	.008	.003	-.028	-.018	.008	1.1684
1.0065	1.158	1.372	.763	.403	.334	.283	.291	.272	.220	.135	.096	.058	5.3850
1.1100	.753	.251	.218	.039	.018	.005	.004	-.013	-.014	-.017	.020	.024	1.2871
1.2400	.262	.054	.071	-.043	.011	-.023	-.017	.037	.052	.030	.017	-.016	.4352
1.3730	.744	.803	.379	.015	-.019	-.021	-.030	-.046	-.025	.015	.038	.006	1.8591
RSUM	3.662	3.899	2.723	1.745	2.095	1.396	.692	.329	.048	-.184	-.208	-.253	15.9441

SECTION V

$M_{\infty}=1.96$, $\alpha=10.0^{\circ}$, $Re=9.8 \times 10^6 ft^{-1}$,

$X/D = 3.5, 4.1, 4.4, 4.8, 6.5$

LOCAL FLOW FIELD DATA

MACH = 1.957 RE = 9.80x10 FT ALPHA = 9.950 X/D = 3.500 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 1 0	1.890	1.898	1.527	1.257	1.171	1.373	1.773	1.891	1.705	1.853	1.997	2.000	1.962
.395 13 0	1.991	1.965	1.966	1.995	2.001	2.002	2.005	2.006	2.010	2.013	2.004	2.000	2.020
.438 1 0	1.918	1.918	1.934	1.950	1.956	1.962	1.974	1.990	1.997	1.999	2.001	2.007	2.020
.495 13 0	1.936	1.944	1.952	1.953	1.958	1.961	1.954	1.956	1.960	1.969	1.984	1.995	2.007
.564 17 0	1.961	1.949	1.953	1.972	1.984	1.984	1.974	1.967	1.976	1.994	2.011	2.018	2.021
.685 53 0	1.928	1.922	1.926	1.939	1.949	1.951	1.951	1.957	1.963	1.968	1.974	1.982	1.981
.824 57 0	1.926	1.920	1.931	1.949	1.953	1.962	1.973	1.976	1.986	1.999	1.995	1.982	1.979
.940 93 0	1.918	1.906	1.919	1.933	1.933	1.958	1.985	1.995	2.013	2.043	2.025	2.009	2.010
1.027 93 0	1.976	1.979	1.969	1.969	1.972	1.967	1.977	1.988	2.001	2.007	2.007	1.998	1.977
1.161 57 0	1.972	1.989	1.971	1.967	1.962	1.956	1.966	1.992	2.019	2.020	2.020	2.011	1.987
1.283 53 0	1.955	1.963	1.961	1.950	1.952	1.956	1.971	1.988	2.008	2.014	1.997	1.996	1.977
1.432 17 0	1.965	1.973	1.952	1.939	1.956	1.989	1.986	1.984	1.995	2.006	2.002	1.991	2.012

LOCAL FLOW FIELD DATA

MACH = 1.964 RE = 9.79x10⁶ FT ALPHA = 9.950 X/D = 4.100 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 9 0	1.380	1.272	.683	.798	.702	.726	1.411	1.878	1.843	1.889	1.688	1.512	1.453
.438 5 0	1.322	1.507	1.729	1.539	1.485	1.825	1.776	1.492	1.322	1.261	1.235	1.120	.972
.495 9 0	1.099	1.164	1.344	1.470	1.492	1.491	1.519	1.572	1.637	1.586	1.724	1.903	1.933
.564 21 1	1.855	1.779	1.648	1.605	1.625	1.676	1.667	1.754	1.940	2.006	2.000	2.007	2.009
.685 49 0	1.909	1.898	1.905	1.928	1.949	1.953	1.951	1.954	1.963	1.968	1.973	1.974	1.971
.824 61 0	1.924	1.921	1.927	1.948	1.950	1.957	1.970	1.973	1.977	1.988	1.985	1.964	1.958
.940 89 0	1.923	1.913	1.919	1.934	1.945	1.972	2.001	2.004	2.002	2.018	1.999	1.984	1.987
1.027 89 0	1.974	1.978	1.969	1.965	1.964	1.962	1.974	1.982	1.987	1.991	1.994	1.991	1.964
1.161 61 0	1.965	1.987	1.967	1.959	1.955	1.949	1.954	1.976	1.999	2.000	2.003	1.998	1.982
1.283 49 0	1.963	1.976	1.961	1.948	1.951	1.952	1.954	1.969	1.994	1.994	1.983	1.982	1.977
1.432 21 1	1.978	1.973	1.960	1.941	1.951	1.972	1.979	1.981	1.978	1.993	2.005	2.017	1.996

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.81x10 FT ALPHA = 9.950 X/D = 4.400 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 25 1	1.492	1.498	1.616	1.591	1.490	1.450	1.446	1.456	1.467	1.455	1.431	1.390	1.354
.685 45 0	1.468	1.474	1.509	1.530	1.519	1.516	1.514	1.491	1.454	1.402	1.374	1.362	1.342
.824 65 0	1.619	1.575	1.530	1.489	1.484	1.294	1.205	1.263	1.318	1.394	1.514	1.629	1.757
.940 85 0	1.795	1.858	1.919	1.935	1.938	1.969	1.990	1.986	1.989	2.011	2.018	1.992	1.983
1.027 85 0	1.954	1.966	1.960	1.973	1.976	1.966	1.975	1.990	1.997	1.998	1.990	1.979	1.966
1.161 65 0	1.960	1.982	1.963	1.955	1.953	1.947	1.949	1.971	1.996	1.994	1.994	1.986	1.958
1.283 45 0	1.959	1.981	1.963	1.951	1.952	1.951	1.952	1.972	1.995	1.989	1.980	1.981	1.967
1.432 25 1	1.953	1.950	1.941	1.930	1.935	1.949	1.952	1.953	1.963	1.969	1.965	1.972	2.005

LOCAL FLOW FIELD DATA

MACH = 1.969 RE = 9.81X10 FT ALPHA = 9.950 X/D = 4.800 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 29 O	2.404	2.297	1.842	1.621	1.752	1.721	1.929	2.210	2.246	2.235	2.262	2.223	2.155
.665 41 O	2.326	2.339	1.983	1.964	1.959	2.059	2.288	2.352	2.307	2.263	2.222	2.169	2.134
.824 69 O	1.929	1.934	1.919	1.928	1.952	1.966	1.951	1.924	1.893	1.852	1.821	1.797	1.773
.940 81 O	1.753	1.756	1.769	1.779	1.788	1.790	1.768	1.737	1.718	1.706	1.683	1.659	1.641
1.027 81 O	1.671	1.669	1.681	1.698	1.694	1.685	1.664	1.635	1.615	1.601	1.590	1.574	1.564
1.161 69 O	1.599	1.610	1.631	1.645	1.634	1.599	1.574	1.559	1.549	1.537	1.526	1.508	1.484
1.283 41 O	1.583	1.597	1.588	1.601	1.607	1.583	1.430	1.193	1.364	1.503	1.453	2.038	1.868
1.432 29 O	1.959	1.962	1.952	1.937	1.950	1.968	1.971	1.968	1.961	1.966	1.975	1.989	1.970

LOCAL FLOW FIELD DATA

MACH = 1.961 RE = 9.78X10 FT ALPHA = 9.950 X/D = 6.500 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 33 0	1.788	1.700	1.534	1.449	1.445	1.697	1.932	1.920	1.844	1.818	1.831	1.840	1.831
.633 97 0	1.909	1.844	1.687	1.560	1.785	2.001	2.026	2.025	2.016	2.028	2.042	2.030	2.013
.685 37 0	1.929	1.900	1.648	1.575	1.850	2.046	2.085	2.044	2.028	2.048	2.053	2.042	2.027
.765 101 0	1.918	1.928	1.776	1.708	1.880	2.017	2.027	2.024	2.029	2.030	2.017	1.994	1.976
.824 73 0	1.939	1.941	1.898	1.925	2.007	2.047	2.054	2.046	2.056	2.046	2.019	1.982	1.965
.904 105 0	1.920	1.945	1.949	1.962	1.990	1.994	2.020	2.030	2.027	2.018	2.001	1.986	1.978
.940 77 0	1.922	1.937	1.973	1.992	2.013	2.022	2.030	2.042	2.051	2.035	2.007	1.981	1.977
.999 109 0	1.944	1.968	2.000	2.014	2.007	2.018	2.042	2.047	2.034	2.029	2.019	1.978	1.984
1.027 77 0	1.972	2.024	2.013	2.008	2.003	1.994	2.018	2.028	2.016	2.006	1.997	1.981	1.982
1.161 73 0	2.016	2.032	2.031	2.011	2.017	2.051	2.042	2.033	2.026	2.008	2.008	2.035	1.961
1.283 37 0	2.049	2.057	2.032	2.037	2.099	2.072	2.033	2.025	2.015	2.013	2.027	1.996	1.963
1.432 33 0	2.090	2.099	2.083	2.110	2.090	2.058	2.026	1.988	1.999	2.049	2.017	1.991	2.008
1.538 97 0	2.084	2.052	2.159	2.127	2.102	2.072	2.022	2.009	2.055	2.038	2.025	1.992	2.001
1.680 101 0	2.186	2.145	2.139	2.124	2.108	2.085	2.084	2.102	2.089	2.079	2.055	2.003	1.982
1.798 105 0	2.121	2.098	2.104	2.092	2.088	2.077	2.064	2.064	2.052	2.032	2.002	1.981	1.952
1.923 109 0	2.074	2.055	2.054	2.051	2.048	2.035	2.014	2.018	2.010	1.975	1.950	1.942	1.914

LOCAL FLOW FIELD DATA

MACH = 1.957 RE = 9.60×10^5 FT $\alpha = -1$ ALPHA = 9.950 X/D = 3.500 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315	1 0 4.055	4.525	3.947	4.330	11.810	14.971	14.859	13.978	15.390	14.332	14.499	15.003	15.389
.395	13 0 .893	4.717	7.933	10.648	12.079	12.773	13.181	13.543	13.931	14.367	14.598	14.609	15.511
.438	1 0 4.501	4.524	6.308	8.511	10.199	11.157	11.779	12.141	12.506	12.927	13.304	13.569	13.772
.495	13 0 6.236	6.631	7.902	9.085	10.127	10.765	11.266	11.651	11.890	12.146	12.416	12.671	12.747
.564	17 0 7.151	7.225	7.848	8.585	9.295	10.016	10.675	11.125	11.538	11.903	12.336	12.633	12.647
.685	53 0 8.165	8.277	8.502	8.862	9.385	9.975	10.469	10.744	11.000	11.204	11.729	12.170	12.163
.824	57 0 9.197	9.349	9.552	9.683	9.853	10.185	10.434	10.534	10.651	10.760	10.998	11.465	11.901
.940	93 0 9.047	9.116	9.320	9.551	9.868	10.064	10.176	10.172	9.970	9.802	10.700	11.523	11.610
1.027	93 0 9.351	8.825	8.986	9.242	9.411	9.601	9.891	10.012	10.275	10.566	10.675	10.511	10.624
1.161	57 0 9.759	9.113	9.127	9.157	9.296	9.449	9.747	9.907	10.057	10.062	10.206	10.430	10.426
1.283	53 0 9.290	9.056	9.109	9.070	9.334	9.682	9.603	9.536	9.886	10.166	10.336	10.450	10.634
1.432	17 0 8.976	9.247	9.570	9.573	9.285	9.288	9.565	9.831	10.097	10.302	10.255	10.415	10.418

LOCAL FLOW FIELD DATA

MACH = 1.964 RE = 9.79X10 FT ALPHA = 9.950 X/D = 4.100 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395	9 0 11.091	6.987	19.108	25.085	20.484	14.333	13.801	14.635	16.559	16.260	19.128	22.260	23.914
.438	5 0 16.332	14.743	12.684	10.168	11.954	15.506	17.582	21.901	24.766	25.988	26.407	28.024	28.544
.495	9 0 23.957	23.903	24.005	24.267	24.450	23.813	21.577	19.034	17.252	16.556	12.850	12.148	12.386
.564	21 1 7.796	10.217	14.777	18.013	18.694	17.618	15.964	13.693	11.831	11.986	12.206	12.403	12.638
.685	49 0 8.091	8.248	8.660	9.120	9.790	10.393	10.829	11.077	11.252	11.479	11.834	12.135	12.180
.824	61 0 9.009	9.109	9.360	9.520	9.866	10.277	10.612	10.680	10.667	10.754	10.999	11.246	11.570
.940	89 0 8.831	8.878	9.059	9.296	9.417	9.562	9.671	9.749	9.921	9.821	10.566	11.256	11.315
1.027	89 0 9.320	8.756	8.908	9.114	9.397	9.730	9.970	10.061	10.284	10.560	10.593	10.290	10.561
1.161	61 0 9.731	9.195	9.210	9.310	9.400	9.491	9.624	10.116	10.149	10.025	10.183	10.431	10.490
1.283	49 0 9.472	9.247	9.246	9.194	9.302	9.485	9.536	9.541	9.921	10.008	10.174	10.692	10.773
1.432	21 1 9.121	9.442	9.707	9.811	9.653	9.648	9.754	10.181	10.520	10.509	10.563	10.873	11.064

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.000 RE = 9.01×10^6 FT ALPHA = 9.950 X/D = 4.400 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564	25 1 19.897	19.076	17.203	15.477	15.285	19.010	23.496	24.597	24.529	24.938	25.375	25.883	26.029
.685	45 0 20.795	20.725	21.022	22.219	23.753	24.319	23.703	22.959	22.998	23.735	24.041	23.780	23.375
.824	65 0 18.559	19.413	20.728	21.985	22.387	25.366	25.624	23.045	21.968	20.321	17.020	13.635	11.181
.940	85 0 11.057	9.975	9.540	9.888	10.113	10.349	10.495	10.522	10.613	10.549	10.551	11.002	11.478
1.027	85 0 8.962	8.688	8.784	9.129	9.396	9.737	10.165	10.239	10.374	10.543	10.613	10.574	10.790
1.161	65 0 9.722	9.238	9.223	9.229	9.415	9.549	9.849	10.004	10.132	10.026	10.155	10.317	10.254
1.283	45 0 9.561	9.266	9.262	9.209	9.350	9.469	9.575	9.604	9.905	9.919	10.084	10.640	10.468
1.432	25 1 9.378	9.525	9.914	9.944	9.793	9.707	9.994	10.173	10.303	10.434	10.479	10.784	10.990

LOCAL FLOW FIELD DATA

MACH = 1.969 RE = 9.81x10 FT ALPHA = 9.950 X/D = 4.800 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.964 29 0	2.427	3.952	4.882	4.542	4.883	4.544	7.601	10.374	11.546	11.901	11.773	11.752	11.935
.685 41 0	1.626	1.682	4.929	3.618	7.929	11.695	10.602	10.390	10.195	10.117	10.442	10.978	11.306
.824 69 0	12.802	12.337	12.017	12.315	13.276	14.202	14.752	14.976	14.978	14.998	14.940	14.727	14.327
.940 81 0	16.687	16.629	16.508	16.535	17.047	17.665	18.253	18.400	18.208	17.996	17.722	17.325	16.709
1.027 81 0	18.136	18.050	17.506	17.320	17.885	18.263	18.602	18.748	18.543	18.156	17.811	17.325	16.788
1.161 69 0	20.233	20.061	19.182	18.461	18.843	19.517	19.609	19.728	19.643	19.287	18.857	18.169	17.363
1.283 41 0	20.172	20.231	19.818	19.146	19.071	19.748	22.467	26.675	19.991	17.505	17.336	9.176	11.592
1.432 29 0	9.454	9.615	9.862	9.989	9.796	9.755	9.841	10.284	10.575	10.515	10.508	10.788	11.006

LOCAL FLOW FIELD DATA

MACH = 1.961 RE = 9.78X10 FT ALPHA = 9.950 X/D = 6.500 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.964 33 0	.788	1.989	4.284	3.752	5.534	12.211	15.205	16.377	17.512	18.229	18.935	19.146	18.953
.633 97 0	1.545	.627	1.555	8.440	10.952	11.126	12.363	13.739	14.802	15.916	16.763	16.976	16.863
.685 37 0	1.001	2.910	2.743	9.232	11.225	10.708	11.575	12.828	13.941	14.807	15.254	15.347	15.450
.765 101 0	3.357	3.691	6.781	10.814	11.411	11.257	12.070	12.767	13.532	14.188	14.603	14.675	14.740
.624 73 0	2.502	3.255	7.103	10.221	10.645	10.912	11.773	12.371	13.017	13.463	13.737	13.731	13.799
.904 105 0	5.244	5.832	7.519	9.433	10.058	10.697	11.632	12.351	12.739	13.032	13.622	13.609	13.301
.940 77 0	5.030	5.558	7.028	8.795	9.748	10.406	11.269	11.941	12.323	12.655	13.254	13.390	13.069
.999 109 0	5.735	5.979	7.034	8.513	9.521	10.626	11.393	11.882	12.095	12.200	12.398	12.310	12.575
1.027 77 0	5.949	5.586	6.483	7.748	9.060	9.857	10.459	10.942	11.501	11.958	12.192	12.373	12.518
1.161 73 0	6.454	6.466	6.913	7.810	8.807	9.519	9.915	10.420	10.826	11.075	11.437	11.976	11.206
1.283 37 0	5.998	6.426	6.943	7.484	8.425	9.094	9.781	10.276	10.771	11.123	11.629	11.628	11.202
1.432 33 0	5.782	6.041	6.629	7.044	8.048	8.897	9.487	9.856	10.538	11.295	11.174	11.143	11.196
1.538 97 0	6.111	5.482	5.402	6.580	7.750	8.373	9.038	9.382	9.983	10.389	10.337	10.249	10.515
1.680 101 0	4.910	5.022	5.914	6.741	7.556	8.079	8.421	8.953	9.678	9.897	9.971	10.091	10.247
1.798 105 0	6.116	6.288	6.674	7.058	7.636	8.108	8.523	9.069	9.643	9.789	9.912	10.004	10.090
1.923 109 0	7.613	7.493	7.756	8.162	8.705	8.995	9.207	9.784	10.132	10.204	10.277	10.189	10.361

LOCAL FLOW FIELD DATA

MACH = 1.957 RE = 9.60x10 FT ALPHA = 9.950 X/D = 3.500 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 1 0	180.0	-154.0	-156.9	58.7	61.7	83.9	87.5	68.4	50.2	64.2	84.2	87.2	87.8
.395 13 0	.0	80.7	78.6	68.6	65.5	65.8	67.7	70.8	74.6	79.5	84.2	89.1	93.8
.438 1 0	.0	22.2	44.2	50.9	54.5	57.3	61.0	65.4	70.5	75.4	80.1	84.3	88.9
.495 13 0	.0	15.9	32.6	40.8	47.9	54.1	58.6	63.0	68.0	73.1	78.5	83.8	89.0
.564 17 0	.0	8.8	25.6	35.2	41.9	48.9	55.6	60.8	66.4	72.8	79.5	86.0	91.5
.685 53 0	.0	8.1	20.7	30.9	39.1	46.4	53.2	59.8	66.5	72.9	79.8	86.8	92.4
.824 57 0	.0	6.8	17.7	27.0	34.8	42.9	50.4	56.6	63.5	71.3	78.4	86.7	94.2
.940 93 0	.0	6.3	16.2	26.8	35.0	41.6	48.6	55.0	62.1	70.4	79.2	87.0	93.3
1.027 93 0	.0	6.4	14.7	23.8	32.7	41.7	49.8	58.0	67.0	74.3	79.7	85.9	93.2
1.161 57 0	.0	6.8	14.0	23.0	31.5	39.9	49.3	59.0	67.0	72.8	78.9	86.9	95.4
1.283 53 0	.0	9.2	16.1	23.0	31.2	40.8	50.4	59.9	68.3	74.5	81.0	86.7	93.3
1.432 17 0	.0	8.0	14.9	22.2	32.3	43.5	52.1	60.0	66.5	73.5	80.0	84.9	90.4

LOCAL FLOW FIELD DATA

MACH = 1.964 $Re = 9.79 \times 10^6$ $\alpha = 9.950$ $X/D = 4.100$ TEST NO. = 35

CROSSFLOW DIRECTION (THETA) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 9 0	.0	-42.7	-10.9	-4.7	-6.7	91.8	87.2	67.0	61.9	65.7	49.8	43.4	47.2
.438 5 0	.0	22.0	32.8	41.0	63.1	61.9	37.5	24.4	28.4	33.6	35.5	36.4	35.9
.495 9 0	.0	4.6	17.6	20.5	17.4	15.0	17.7	24.6	32.6	36.5	56.6	77.3	83.0
.564 21 1	.0	20.8	26.2	25.9	25.7	27.0	30.8	38.7	60.5	72.6	77.5	83.4	89.0
.685 49 0	.0	13.1	24.2	33.7	41.1	47.2	53.8	60.3	66.2	72.0	78.4	84.5	89.9
.824 61 0	.0	6.7	17.9	28.0	36.0	43.4	50.3	56.1	62.6	69.6	77.0	84.7	92.3
.940 89 0	.0	5.6	16.3	27.1	34.5	40.4	47.3	54.0	61.0	68.8	77.8	85.5	92.3
1.027 89 0	.0	7.0	15.3	24.8	33.9	42.3	49.6	56.9	65.5	72.8	77.7	83.5	91.5
1.161 61 0	.0	7.1	14.0	22.8	31.5	39.4	48.1	56.3	64.1	70.5	76.4	84.3	93.9
1.283 49 0	.0	8.4	15.5	22.3	30.6	40.4	50.4	59.1	68.1	74.6	81.6	88.7	98.0
1.432 21 1	.0	6.6	12.8	21.2	30.4	39.1	46.8	56.0	62.2	70.6	79.0	84.9	90.7

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.81x10 FT ALPHA = 9.950 X/D = 4.400 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 25 1	.0	7.9	16.1	26.7	32.1	33.2	24.5	22.9	27.5	29.9	31.8	34.1	35.9
.685 45 0	.0	5.7	12.7	16.8	18.4	19.2	20.4	22.6	25.3	28.4	31.3	33.7	35.4
.824 65 0	.0	3.5	8.6	12.4	16.7	20.3	19.5	24.3	30.9	34.6	40.0	51.5	72.6
.940 85 0	.0	9.4	16.2	27.1	35.5	43.0	48.6	53.7	60.3	67.2	74.7	83.6	91.1
1.027 85 0	.0	9.0	16.9	26.5	34.6	43.7	51.6	58.7	66.9	73.8	79.5	86.0	92.2
1.161 65 0	.0	6.3	13.9	22.6	31.3	39.1	47.8	55.6	63.6	69.8	75.6	83.1	92.1
1.283 45 0	.0	7.7	14.7	22.4	30.9	40.2	50.2	58.6	67.0	73.5	80.3	87.2	96.0
1.432 25 1	.0	4.6	13.5	19.9	28.5	37.7	46.6	55.8	61.9	68.4	75.9	83.6	90.9

LOCAL FLOW FIELD DATA

+8 -1

MACH = 1.000 RE = 9.61X10 FT ALPHA = 9.950 X/D = 4.600 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 29 0	180.0	-138.9	-154.3	-149.8	-27.1	31.9	83.4	93.0	96.5	95.3	94.3	93.4	92.4
.685 41 0	.0	-65.4	80.4	110.8	62.9	58.8	70.4	76.0	76.5	78.2	79.0	81.6	83.3
.824 69 0	.0	.5	8.8	22.1	32.1	36.4	36.8	37.7	38.8	40.2	43.3	46.8	49.7
.940 81 0	.0	.1	6.0	14.9	21.8	25.2	27.0	28.3	30.2	32.7	35.5	38.0	40.2
1.027 81 0	.0	4.3	8.5	15.5	21.8	26.0	27.6	29.7	33.5	36.8	39.1	40.9	43.8
1.161 69 0	.0	4.2	8.1	13.5	19.3	22.4	24.6	27.4	30.6	33.0	35.0	37.1	40.3
1.283 41 0	.0	5.8	9.6	13.7	18.5	21.3	22.1	22.5	31.5	37.8	39.9	83.2	91.3
1.432 29 0	.0	6.5	13.1	21.3	30.0	38.3	45.9	54.9	60.8	67.8	75.7	82.3	89.8

LOCAL FLOW FIELD DATA

MACH = 1.961 RE = 9.78x10⁴ FT ALPHA = 9.950 X/D = 6.500 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 33 0	.0	-65.0	-35.1	16.8	76.9	92.4	85.9	76.7	71.2	71.1	73.6	76.1	77.5
.633 97 0	.0	110.8	-34.2	29.4	55.3	69.0	74.5	79.0	82.2	84.5	86.4	87.6	88.6
.685 37 0	-180.0	179.4	124.9	47.4	51.4	64.4	72.5	75.4	79.4	83.6	85.9	87.7	89.5
.765 101 0	.0	52.3	71.9	58.8	54.7	62.6	70.6	75.5	79.5	82.5	84.9	87.0	88.9
.824 73 0	.0	47.7	65.3	54.3	53.0	61.0	67.4	71.6	76.6	80.1	82.8	85.7	89.4
.904 105 0	.0	28.8	46.3	52.4	55.8	60.1	66.2	72.2	75.7	78.1	81.3	83.9	87.4
.940 77 0	.0	26.3	44.0	49.8	53.6	57.7	64.2	70.1	74.4	77.1	80.6	84.4	89.3
.999 109 0	.0	23.8	38.5	48.8	55.5	60.7	67.4	72.9	75.4	78.1	82.2	85.6	90.5
1.027 77 0	.0	22.1	35.7	45.5	52.7	59.9	67.4	72.7	76.4	80.2	84.0	89.4	93.8
1.161 73 0	.0	14.5	27.1	35.3	47.3	62.2	65.2	67.6	70.9	74.0	78.7	87.4	89.2
1.283 37 0	.0	17.2	24.8	39.6	60.8	63.0	65.8	68.5	71.3	77.6	85.3	88.3	94.0
1.432 33 0	.0	12.7	26.2	48.2	54.7	59.0	61.3	63.6	70.5	80.9	84.1	86.8	89.2
1.538 97 0	.0	10.7	38.0	46.0	51.6	55.2	56.0	62.5	77.2	80.0	83.4	88.3	93.9
1.680 101 0	.0	17.9	30.2	38.7	45.9	50.8	59.7	69.1	73.7	76.4	79.7	86.1	92.2
1.798 105 0	.0	8.2	21.6	30.6	39.8	47.8	55.5	61.3	66.1	70.3	75.2	79.5	84.4
1.923 109 0	.0	11.8	20.6	30.0	37.3	43.9	52.4	58.6	62.6	66.9	71.3	74.0	78.9

LOCAL FLOW FIELD DATA

MACH = 1.957 RE = 9.80x10⁶ FT ALPHA = 9.950 X/D = 3.500 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA		180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D	RUN NO.													
.315	1 0	.006	.003	.023	.039	.074	.049	.007	.029	.092	.024	-.032	-.035	-.021
.395	13 0	-.007	.003	-.003	-.019	-.022	-.021	-.022	-.022	-.024	-.025	-.022	-.024	-.041
.438	1 0	.021	.020	.009	-.000	-.004	-.007	-.012	-.019	-.022	-.024	-.025	-.031	-.039
.495	13 0	.020	.013	.007	.006	.001	.000	.003	.002	-.001	-.007	-.017	-.022	-.026
.564	17 0	.005	.008	.004	-.005	-.012	-.013	-.009	-.004	-.009	-.019	-.028	-.032	-.034
.665	53 0	.020	.022	.017	.009	.003	.002	.002	.000	-.004	-.008	-.012	-.017	-.016
.824	57 0	.025	.027	.020	.010	.008	.001	-.003	-.003	-.010	-.018	-.019	-.015	-.014
.940	93 0	.028	.033	.024	.018	.017	.004	-.009	-.012	-.021	-.037	-.032	-.025	-.023
1.027	93 0	.001	-.002	.002	-.000	-.001	.002	-.003	-.011	-.021	-.022	-.021	-.017	-.010
1.161	57 0	.001	-.006	.002	.004	.006	.011	.005	-.013	-.025	-.026	-.027	-.023	-.011
1.283	53 0	.005	-.000	.004	.008	.007	.005	-.002	-.014	-.024	-.026	-.019	-.017	-.007
1.432	17 0	-.003	-.005	.005	.011	.001	-.013	-.013	-.011	-.017	-.024	-.021	-.017	-.020

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.984 RE = 9.79X10 FT ALPHA = 9.950 X/D = 4.100 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	160.00	172.50	185.00	197.50	210.00	222.50	235.00	247.50	260.00	272.50	285.00	297.50	310.00
R/D RUN NO.													
.395 9 0	.489	.420	.478	.384	.321	.184	.137	.068	.112	.084	.213	.353	.419
.438 5 0	.560	.381	.140	.092	.043	.033	.143	.354	.506	.581	.617	.747	.865
.495 9 0	.642	.614	.472	.368	.351	.344	.304	.251	.205	.188	.092	.013	.004
.564 21 1	.051	.081	.154	.207	.207	.176	.149	.083	.006	-.020	-.019	-.022	-.024
.685 49 0	.026	.032	.029	.015	.003	.002	.003	.002	-.001	-.004	-.008	-.010	-.008
.824 61 0	.026	.027	.023	.011	.008	.004	-.002	-.001	-.005	-.012	-.013	-.005	-.002
.940 89 0	.027	.031	.026	.019	.014	-.000	-.014	-.015	-.016	-.026	-.019	-.011	-.012
1.027 89 0	.002	-.001	.003	.002	.003	.005	-.000	-.007	-.011	-.012	-.012	-.011	-.001
1.161 61 0	.006	-.006	.004	.009	.011	.015	.011	-.002	-.014	-.015	-.017	-.016	-.011
1.283 49 0	.003	-.004	.005	.012	.009	.009	.009	-.001	-.014	-.013	-.009	-.011	-.009
1.432 21 1	-.004	.000	.007	.016	.010	-.000	-.003	-.005	-.005	-.014	-.018	-.026	-.009

LOCAL FLOW FIELD DATA

+8 -1

MACH = 1.958 RE = 9.81X10 FT ALPHA = 9.950 X/D = 4.400 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA		180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D	RUN NO.													
.564	25 1	.348	.359	.240	.158	.125	.154	.347	.422	.408	.421	.441	.466	.486
.685	45 0	.353	.361	.353	.343	.352	.360	.360	.381	.417	.446	.463	.477	.497
.824	65 0	.259	.295	.333	.361	.360	.510	.531	.444	.389	.310	.214	.148	.085
.940	85 0	.086	.055	.026	.018	.017	.002	-.007	-.005	-.008	-.019	-.023	-.012	-.007
1.027	85 0	.016	.007	.009	.001	-.000	.006	.002	-.008	-.013	-.013	-.008	-.004	.000
1.161	65 0	.007	-.004	.006	.010	.012	.016	.013	.000	-.013	-.013	-.013	-.010	.002
1.283	45 0	.001	-.007	.003	.009	.008	.009	.009	-.003	-.016	-.013	-.008	-.009	-.004
1.432	25 1	.003	.006	.011	.018	.014	.006	.006	.005	.001	-.003	-.004	-.009	-.022

LOCAL FLOW FIELD DATA

MACH = 1.969 RE = 9.81X10⁶ FT ALPHA = 9.950 X/D = 4.800 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.964 29 0	-.201	-.186	-.121	-.109	-.099	-.070	-.081	-.148	-.156	-.149	-.148	-.136	-.116
.695 41 0	-.141	-.142	-.082	-.094	-.084	-.098	-.135	-.140	-.125	-.111	-.103	-.093	-.084
.624 69 0	.046	.047	.054	.044	.030	.026	.039	.056	.074	.090	.098	.109	.123
.940 81 0	.165	.162	.154	.148	.146	.146	.155	.173	.185	.194	.208	.223	.236
1.027 81 0	.230	.229	.217	.202	.204	.212	.225	.245	.261	.272	.279	.289	.294
1.161 69 0	.284	.274	.260	.247	.252	.280	.299	.309	.319	.329	.336	.349	.365
1.263 41 0	.269	.274	.285	.275	.269	.293	.405	.535	.343	.226	.284	-.042	.057
1.432 29 0	.004	.003	.010	.018	.011	.002	.000	.001	.004	.002	-.004	-.013	.003

LOCAL FLOW FIELD DATA

MACH = 1.961 RE = 9.78X10 FT ALPHA = 9.950 X/D = 6.500 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 33 0	.034	.041	.053	.031	-.007	-.040	-.052	-.020	.000	-.003	-.014	-.019	-.014
.633 97 0	-.008	-.008	-.017	-.020	-.007	-.041	-.051	-.059	-.066	-.076	-.080	-.073	-.067
.685 37 0	-.009	-.016	-.011	-.029	-.026	-.054	-.066	-.068	-.075	-.083	-.084	-.078	-.071
.765 101 0	-.006	-.007	-.004	-.019	-.018	-.040	-.052	-.058	-.065	-.066	-.060	-.048	-.042
.824 73 0	-.006	-.005	-.014	-.027	-.037	-.047	-.059	-.064	-.072	-.070	-.059	-.043	-.036
.904 105 0	.003	-.002	-.009	-.015	-.024	-.034	-.049	-.060	-.063	-.057	-.048	-.037	-.033
.940 77 0	-.005	-.002	-.017	-.024	-.032	-.043	-.056	-.065	-.068	-.062	-.051	-.041	-.038
.999 109 0	-.005	-.010	-.023	-.031	-.028	-.036	-.052	-.059	-.056	-.054	-.050	-.032	-.034
1.027 77 0	-.025	-.038	-.034	-.030	-.031	-.037	-.054	-.058	-.051	-.045	-.044	-.042	-.030
1.161 73 0	-.040	-.045	-.038	-.028	-.035	-.060	-.053	-.049	-.046	-.039	-.041	-.052	-.021
1.283 37 0	-.058	-.056	-.039	-.043	-.079	-.064	-.049	-.045	-.042	-.042	-.051	-.035	-.015
1.432 33 0	-.072	-.073	-.069	-.083	-.073	-.062	-.047	-.029	-.038	-.062	-.044	-.032	-.032
1.538 97 0	-.068	-.069	-.101	-.091	-.079	-.063	-.040	-.038	-.064	-.054	-.045	-.029	-.032
1.680 101 0	-.107	-.090	-.088	-.084	-.076	-.069	-.070	-.075	-.068	-.063	-.051	-.026	-.010
1.798 105 0	-.083	-.072	-.077	-.072	-.068	-.062	-.055	-.056	-.050	-.040	-.022	-.003	.013
1.923 109 0	-.056	-.051	-.050	-.048	-.044	-.036	-.025	-.027	-.023	-.004	.011	.018	.034

LOCAL FLOW FIELD DATA

MACH = 1.957 RE = 9.60x10⁴ FT ALPHA = 9.950 X/D = 3.500 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 1 0	.916	.923	.955	.995	.982	.475	.768	.974	.849	.909	.974	.974	.953
.395 13 0	1.016	1.008	.990	.991	.993	.996	.999	1.000	1.002	1.004	.998	.986	.968
.438 1 0	.998	.996	.993	.992	.992	.993	.997	1.004	1.006	1.004	.999	.994	.991
.495 13 0	1.003	.997	.993	.989	.984	.983	.991	.995	.990	.986	.982	.985	.992
.564 17 0	1.015	1.006	.999	1.002	1.000	.999	.997	.994	.995	.998	.997	.994	.996
.685 53 0	1.002	1.000	.996	.994	.992	.992	.992	.993	.993	.990	.984	.985	.987
.824 57 0	1.003	.997	.996	.998	.996	.994	.996	1.000	.998	.995	.988	.977	.973
.940 93 0	1.004	.996	.995	.999	.999	1.001	1.006	1.012	1.017	1.019	1.003	.999	1.006
1.027 93 0	1.022	1.016	1.013	1.007	1.009	1.009	1.011	1.006	1.002	1.006	1.010	1.007	.997
1.161 57 0	1.006	1.010	1.009	1.006	1.004	1.005	1.004	1.002	1.009	1.009	1.005	1.004	1.002
1.283 53 0	1.003	1.003	1.008	1.006	1.004	1.006	1.011	1.006	1.007	1.013	1.010	1.009	1.007
1.432 17 0	.999	.999	.997	.994	.994	1.004	1.004	1.002	1.003	1.002	1.006	1.004	1.024

B

LOCAL FLOW FIELD DATA

MACH = 1.004 RE = 9.79X10 FT ALPHA = 9.950 X/D = 4.100 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 9 0	.971	.768	.423	.418	.350	.287	.597	1.036	1.077	1.091	1.030	.983	.987
.438 5 0	.971	1.017	.961	.656	.542	.678	1.038	.958	.913	.912	.913	.892	.827
.495 9 0	.784	.831	.906	.946	.953	.944	.929	.925	.943	.848	.863	.941	.962
.564 21 1	.953	.909	.867	.896	.924	.942	.885	.880	.968	.999	.993	.992	.989
.685 49 0	.992	.985	.983	.981	.985	.988	.990	.992	.996	.996	.992	.990	.991
.824 61 0	1.001	1.001	.998	1.000	.995	.993	.997	1.001	1.000	.995	.989	.980	.974
.940 89 0	1.007	1.004	.999	1.004	1.010	1.012	1.018	1.022	1.017	1.015	1.002	.998	1.002
1.027 89 0	1.022	1.017	1.015	1.009	1.008	1.011	1.015	1.010	1.006	1.010	1.015	1.013	.999
1.161 61 0	1.007	1.013	1.009	1.007	1.008	1.009	1.008	1.008	1.010	1.009	1.009	1.006	.993
1.283 49 0	1.008	1.010	1.012	1.008	1.005	1.007	1.011	1.004	1.007	1.010	1.004	1.000	1.010
1.432 21 1	1.001	.999	1.001	.997	.997	1.003	1.007	1.005	1.001	1.000	1.003	1.003	1.016

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.81x10⁺⁶ FT ALPHA = 9.950 X/D = 4.400 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 25 1	.957	.979	.974	.812	.657	.657	.894	1.000	.998	.997	.988	.959	.935
.685 45 0	.931	.948	.985	1.003	.999	1.002	1.003	.996	.990	.955	.937	.937	.933
.824 65 0	1.005	.994	.984	.964	.955	.881	.800	.781	.783	.781	.795	.834	.888
.940 85 0	.945	.972	.994	.996	.997	1.005	1.011	1.011	1.009	1.012	1.011	1.001	.998
1.027 85 0	1.017	1.013	1.009	1.007	1.011	1.010	1.012	1.010	1.008	1.012	1.014	1.010	.998
1.161 65 0	1.004	1.010	1.009	1.008	1.010	1.011	1.008	1.009	1.013	1.010	1.009	1.006	.999
1.283 45 0	1.002	1.012	1.014	1.012	1.008	1.008	1.010	1.007	1.009	1.010	1.008	1.009	1.003
1.432 25 1	.997	.996	.999	1.000	.999	.998	1.004	1.004	1.005	1.004	.999	.993	1.012

LOCAL FLOW FIELD DATA

*6 -1

MACH = 1.000 RE = 9.81X10 FT ALPHA = 9.950 X/D = 4.800 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 29 0	.896	.828	.553	.415	.324	.553	.733	.873	.885	.901	.943	.937	.912
.685 41 0	1.078	1.094	.795	.741	.757	.844	1.039	1.124	1.126	1.108	1.072	1.023	.998
.824 69 0	1.062	1.073	1.064	1.052	1.054	1.067	1.075	1.076	1.070	1.038	1.006	.993	.987
.940 81 0	1.040	1.038	1.045	1.049	1.058	1.060	1.043	1.028	1.023	1.020	1.009	1.000	.995
1.027 81 0	1.029	1.025	1.022	1.022	1.019	1.019	1.011	1.001	.997	.995	.990	.980	.973
1.161 69 0	1.006	1.010	1.016	1.017	1.012	1.002	.993	.988	.987	.985	.980	.973	.960
1.283 41 0	.993	.989	.994	.998	.999	.996	.933	.789	.781	.799	.815	.984	.990
1.432 29 0	.992	.995	.999	.996	.998	1.005	1.005	1.001	.998	1.000	1.001	.997	1.010

LOCAL FLOW FIELD DATA

MACH = 1.961 RE = 9.78X10 FT ALPHA = 9.950 X/D = 6.500 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 33 0	.836	.745	.599	.503	.451	.394	.323	.284	.235	.194	.163	.122	.083
.633 97 0	.900	.817	.628	.514	.448	.347	.254	.225	.195	.161	.127	.093	.060
.685 37 0	.925	.868	.600	.510	.475	.364	.285	.219	.180	.153	.129	.109	.086
.765 101 0	.916	.928	.741	.641	.634	.566	.446	.324	.211	.107	.005	.007	.001
.824 73 0	.942	.947	.863	.866	.935	.984	.961	.936	.924	.915	.908	.903	.897
.904 105 0	.936	.959	.957	.965	.981	.959	.956	.937	.925	.927	.929	.941	.939
.940 77 0	.929	.960	.977	.983	.994	.972	.946	.939	.943	.935	.927	.918	.918
.999 109 0	.951	.970	.981	.979	.975	.971	.958	.943	.935	.932	.930	.922	.926
1.027 77 0	.950	.987	.986	.989	.982	.949	.934	.938	.941	.945	.935	.918	.951
1.161 73 0	.963	.969	.989	.989	.979	.955	.959	.957	.957	.951	.945	.953	.939
1.283 37 0	.958	.977	.993	.990	.970	.974	.962	.959	.957	.956	.950	.955	.959
1.432 33 0	.982	.990	.976	.976	.982	.967	.968	.962	.951	.957	.962	.960	.982
1.538 97 0	.987	.937	.989	.977	.982	.985	.979	.967	.958	.961	.970	.966	.969
1.680 101 0	1.004	.997	.995	.988	.991	.980	.978	.987	.990	.993	.991	.990	1.000
1.798 105 0	.999	1.004	.994	.994	1.000	1.002	1.002	1.000	1.001	1.002	1.003	1.007	1.013
1.923 109 0	.992	.985	.982	.984	.994	.995	.996	.996	.996	.994	.996	1.003	1.006

LOCAL FLOW FIELD DATA

MACH = 1.957 RE = 9.80×10^6 FT ALPHA = 9.950 X/D = 3.500 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 1 0	-.069	-.070	-.054	.029	.068	.022	.010	.087	.156	.104	.026	.013	.010
.395 13 0	.016	.013	.027	.068	.088	.091	.088	.078	.065	.046	.026	.004	-.018
.438 1 0	.078	.072	.078	.093	.103	.105	.099	.088	.073	.057	.040	.024	.005
.495 13 0	.108	.110	.115	.119	.117	.109	.101	.091	.077	.061	.043	.024	.004
.564 17 0	.125	.124	.123	.122	.121	.115	.105	.094	.080	.062	.040	.015	-.006
.685 53 0	.141	.141	.137	.131	.126	.119	.109	.094	.076	.057	.036	.012	-.009
.824 57 0	.158	.159	.156	.149	.140	.129	.115	.101	.083	.060	.039	.011	-.015
.940 93 0	.155	.155	.154	.147	.139	.130	.118	.102	.082	.058	.035	.011	-.012
1.027 93 0	.163	.153	.151	.147	.138	.125	.111	.093	.071	.050	.034	.013	-.010
1.161 57 0	.170	.158	.154	.146	.137	.125	.110	.089	.069	.052	.034	.010	-.017
1.283 53 0	.161	.155	.152	.145	.138	.127	.107	.084	.064	.048	.028	.011	-.011
1.432 17 0	.156	.160	.160	.153	.136	.118	.103	.086	.070	.051	.031	.016	-.001

LOCAL FLOW FIELD DATA

MACH = 1.964 RE = 9.79x10⁶ FT ALPHA = 9.950 X/D = 4.100 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 9 0	.153	.066	.143	.215	.157	-.004	.009	.096	.129	.112	.193	.234	.227
.438 5 0	.217	.200	.171	.114	.079	.121	.226	.286	.284	.272	.265	.257	.234
.495 9 0	.271	.282	.303	.320	.332	.328	.298	.258	.224	.201	.113	.045	.026
.564 21 1	.131	.156	.205	.245	.257	.245	.214	.173	.100	.063	.046	.025	.004
.685 49 0	.139	.137	.135	.130	.128	.122	.111	.095	.079	.062	.041	.020	.001
.824 61 0	.155	.155	.153	.145	.138	.129	.118	.104	.086	.065	.043	.018	-.008
.940 69 0	.152	.151	.149	.143	.134	.127	.115	.101	.085	.063	.039	.016	-.008
1.027 89 0	.162	.152	.150	.144	.136	.125	.113	.096	.074	.055	.039	.020	-.005
1.161 61 0	.169	.159	.155	.149	.139	.127	.114	.098	.078	.059	.042	.018	-.012
1.283 49 0	.165	.160	.155	.147	.139	.125	.105	.085	.065	.047	.026	.004	-.026
1.432 21 1	.159	.163	.164	.158	.144	.130	.116	.099	.085	.061	.035	.017	-.002

LOCAL FLOW FIELD DATA

MACH = 1.999 $Re = 9.81 \times 10^5$ FT $\alpha = 9.950$ $x/D = 4.400$ TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VINF) --

THETA		180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D	RUN NO.													
.964	25 1	.287	.273	.250	.210	.188	.225	.299	.317	.306	.302	.298	.289	.279
.685	45 0	.296	.294	.297	.310	.326	.331	.321	.303	.292	.285	.276	.265	.252
.824	65 0	.283	.289	.299	.307	.306	.304	.293	.266	.247	.229	.190	.131	.054
.940	85 0	.182	.165	.155	.151	.142	.131	.121	.109	.092	.072	.049	.021	-.004
1.027	85 0	.155	.149	.146	.142	.135	.122	.110	.093	.071	.051	.034	.013	-.007
1.161	65 0	.168	.160	.155	.147	.139	.128	.114	.098	.079	.061	.044	.022	-.007
1.283	45 0	.166	.160	.156	.148	.139	.125	.106	.087	.068	.049	.030	.009	-.019
1.432	25 1	.163	.164	.166	.161	.148	.133	.119	.099	.084	.067	.044	.021	-.003

LOCAL FLOW FIELD DATA

MACH = 1.969 RE = 9.81x10 FT ALPHA = 9.950 X/D = 4.800 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 29 0	-.047	-.056	-.074	-.061	.071	.062	.015	-.010	-.024	-.021	-.016	-.013	-.009
.685 41 0	.031	.013	.014	-.022	.063	.108	.067	.048	.045	.039	.037	.029	.017
.824 69 0	.219	.212	.203	.195	.194	.197	.203	.202	.197	.191	.179	.165	.151
.940 81 0	.268	.268	.265	.259	.257	.260	.262	.258	.249	.239	.225	.212	.197
1.027 81 0	.282	.280	.270	.263	.260	.257	.255	.249	.235	.220	.208	.196	.181
1.161 69 0	.304	.303	.290	.276	.272	.272	.266	.259	.249	.238	.226	.211	.191
1.283 41 0	.302	.303	.293	.281	.274	.275	.288	.296	.229	.201	.188	.019	-.004
1.432 29 0	.164	.166	.166	.160	.146	.133	.119	.103	.089	.069	.045	.025	.001

LOCAL FLOW FIELD DATA

MACH = 1.001 RE = 9.78x10⁶ FT ALPHA = 9.950 X/D = 6.500 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 33 0	.013	.013	.052	.052	.018	-.008	.019	.064	.094	.097	.087	.076	.067
.633 97 0	.027	-.004	.020	.111	.102	.070	.058	.046	.035	.027	.018	.012	.007
.685 37 0	-.017	-.050	-.025	.095	.117	.082	.062	.057	.045	.029	.019	.011	.002
.765 101 0	.058	.039	.035	.089	.111	.091	.071	.056	.044	.033	.023	.013	.005
.824 73 0	.043	.038	.051	.102	.112	.094	.080	.069	.054	.041	.030	.018	.002
.904 105 0	.090	.088	.090	.100	.099	.094	.083	.067	.055	.047	.036	.025	.011
.940 77 0	.087	.086	.088	.100	.102	.098	.087	.072	.059	.050	.038	.023	.003
.999 109 0	.099	.095	.097	.099	.095	.091	.078	.062	.054	.044	.029	.016	-.002
1.027 77 0	.104	.092	.093	.096	.097	.087	.071	.057	.048	.036	.022	.002	-.014
1.161 73 0	.114	.111	.109	.112	.105	.079	.074	.070	.062	.054	.039	.010	.003
1.283 37 0	.107	.110	.112	.102	.074	.074	.071	.067	.061	.042	.017	.006	-.013
1.432 33 0	.104	.106	.107	.085	.084	.082	.081	.077	.062	.032	.020	.011	.003
1.538 97 0	.110	.096	.078	.083	.087	.086	.089	.076	.040	.032	.021	.005	-.013
1.660 101 0	.091	.087	.093	.096	.095	.092	.076	.058	.049	.042	.032	.012	-.007
1.798 105 0	.111	.113	.112	.110	.106	.098	.086	.078	.070	.058	.044	.032	.017
1.923 109 0	.136	.131	.129	.126	.123	.115	.099	.090	.082	.070	.057	.048	.034

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.957 RE = 9.60X10 FT ALPHA = 9.950 X/D = 3.500 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 1 0	.000	-.034	-.023	.048	.127	.204	.242	.220	.188	.216	.252	.262	.266
.395 13 0	.000	.081	.135	.173	.192	.204	.213	.224	.235	.247	.253	.255	.271
.438 1 0	-.000	.029	.076	.115	.144	.163	.180	.193	.207	.219	.230	.237	.242
.495 13 0	.000	.031	.074	.103	.130	.151	.166	.180	.191	.201	.212	.220	.223
.564 17 0	.000	.019	.059	.086	.108	.132	.153	.169	.184	.199	.213	.222	.222
.685 53 0	.000	.020	.052	.079	.102	.125	.145	.161	.175	.186	.201	.212	.212
.824 57 0	.000	.019	.050	.076	.097	.120	.140	.153	.166	.178	.188	.199	.206
.940 93 0	.000	.017	.045	.074	.098	.116	.133	.146	.155	.164	.165	.202	.203
1.027 93 0	-.000	.017	.040	.065	.088	.111	.132	.148	.166	.179	.184	.184	.185
1.161 57 0	-.000	.019	.038	.062	.084	.105	.128	.148	.163	.169	.176	.183	.181
1.283 53 0	.000	.025	.044	.061	.084	.110	.129	.144	.162	.173	.179	.183	.185
1.432 17 0	.000	.022	.043	.062	.086	.112	.132	.149	.162	.174	.177	.182	.183

LOCAL FLOW FIELD DATA

*6 -1

MACH = 1.984 RE = 9.79X10 FT ALPHA = 9.950 X/D = 4.100 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 9 0	.000	-.061	-.027	-.018	-.018	.115	.192	.227	.242	.249	.228	.221	.245
.438 5 0	.000	.081	.110	.099	.155	.226	.173	.129	.154	.181	.189	.189	.169
.495 9 0	-.000	.023	.096	.120	.104	.088	.095	.118	.143	.149	.172	.202	.211
.564 21 1	-.000	.059	.101	.119	.124	.125	.127	.138	.177	.200	.208	.215	.221
.665 49 0	.000	.032	.061	.087	.111	.132	.151	.167	.179	.189	.201	.210	.211
.824 61 0	.000	.018	.049	.077	.100	.122	.142	.154	.165	.176	.187	.194	.200
.940 89 0	.000	.015	.044	.073	.092	.108	.125	.139	.152	.162	.181	.196	.197
1.027 89 0	-.000	.019	.041	.066	.091	.114	.132	.147	.164	.176	.181	.179	.183
1.161 61 0	-.000	.020	.039	.062	.085	.104	.126	.147	.160	.166	.174	.182	.182
1.283 49 0	-.000	.023	.043	.060	.082	.107	.127	.142	.161	.169	.176	.187	.186
1.432 21 1	.000	.019	.037	.061	.084	.106	.124	.147	.162	.173	.182	.190	.193

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.81X10⁶ ALPHA = 9.950 X/D = 4.400 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (V_{THETA}/V_{INF})

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 25 1	-.000	.038	.082	.105	.118	.147	.136	.134	.160	.174	.184	.196	.202
.685 45 0	.000	.029	.067	.094	.108	.115	.119	.126	.138	.154	.168	.177	.180
.824 65 0	.000	.017	.046	.067	.092	.113	.104	.120	.148	.158	.160	.164	.173
.940 85 0	-.000	.027	.051	.077	.101	.123	.137	.148	.161	.171	.179	.191	.200
1.027 85 0	.000	.024	.044	.071	.093	.117	.139	.153	.167	.177	.182	.184	.187
1.161 65 0	-.000	.018	.038	.062	.085	.104	.126	.144	.159	.165	.172	.179	.178
1.283 45 0	.000	.022	.041	.061	.083	.106	.128	.143	.160	.167	.174	.186	.181
1.432 25 1	.000	.013	.040	.058	.081	.103	.126	.146	.158	.169	.177	.187	.193

LOCAL FLOW FIELD DATA

MACH = 1.989 RE = 9.81x10⁶ FT ALPHA = 9.950 X/D = 4.800 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 29 0	.000	-.049	-.035	-.035	-.036	.039	.130	.191	.213	.220	.219	.217	.217
.685 41 0	.000	-.029	.085	.059	.122	.178	.187	.192	.187	.185	.190	.198	.204
.824 69 0	.000	.002	.032	.079	.122	.145	.152	.156	.158	.161	.169	.176	.177
.940 81 0	-.000	.000	.028	.069	.103	.122	.134	.139	.145	.153	.161	.165	.166
1.027 81 0	.000	.021	.040	.073	.104	.125	.134	.142	.156	.165	.169	.170	.174
1.161 69 0	.000	.022	.041	.066	.095	.112	.122	.135	.147	.154	.158	.159	.162
1.283 41 0	.000	.031	.050	.068	.092	.107	.117	.123	.141	.156	.157	.162	.194
1.432 29 0	.000	.019	.039	.062	.085	.105	.123	.146	.160	.169	.177	.187	.191

LOCAL FLOW FIELD DATA

MACH = 1.961 RE = 9.78x10⁴ FT ALPHA = 9.950 X/D = 6.500 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (V_{THETA}/V_{INF})

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.864 33 0	-.000	-.029	-.037	.016	.077	.193	.260	.271	.275	.283	.299	.306	.304
.633 97 0	-.000	.010	-.014	.062	.148	.182	.210	.237	.257	.278	.294	.297	.294
.685 37 0	-.000	.001	.035	.103	.147	.171	.198	.220	.241	.260	.269	.270	.271
.765 101 0	-.000	.050	.106	.148	.157	.176	.201	.217	.234	.247	.255	.255	.255
.824 73 0	.000	.042	.110	.142	.149	.169	.193	.208	.224	.234	.239	.238	.238
.904 105 0	-.000	.049	.094	.130	.146	.162	.188	.208	.218	.224	.236	.236	.231
.940 77 0	-.000	.043	.085	.118	.138	.155	.179	.199	.211	.218	.229	.232	.227
.999 109 0	-.000	.042	.077	.113	.138	.163	.186	.201	.206	.210	.216	.213	.219
1.027 77 0	-.000	.037	.067	.097	.127	.149	.170	.185	.197	.207	.212	.216	.218
1.161 73 0	-.000	.029	.056	.080	.114	.150	.160	.170	.180	.187	.197	.211	.194
1.283 37 0	.000	.034	.052	.085	.133	.145	.158	.169	.180	.191	.204	.203	.194
1.432 33 0	.000	.024	.053	.095	.118	.136	.147	.155	.174	.198	.196	.195	.197
1.538 97 0	.000	.018	.061	.086	.110	.123	.132	.147	.173	.181	.181	.179	.184
1.680 101 0	.000	.028	.054	.076	.098	.112	.131	.151	.167	.172	.175	.177	.179
1.798 105 0	.000	.016	.045	.065	.088	.108	.126	.142	.157	.163	.168	.171	.174
1.923 109 0	.000	.027	.049	.073	.094	.110	.128	.147	.158	.163	.168	.169	.174

LOCAL FLOW FIELD DATA

MACH = 1.957 RE = 9.80x10 FT ALPHA = 9.950 X/D = 3.500 TEST NO. = 35

(VC / VINF * SIN ALPHAINF)

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 1 0	.401	.449	.341	.325	.835	1.187	1.400	1.370	1.415	1.388	1.466	1.518	1.538
.395 13 0	.091	.476	.799	1.078	1.223	1.292	1.334	1.371	1.411	1.455	1.474	1.474	1.572
.438 1 0	.449	.452	.632	.855	1.025	1.122	1.188	1.230	1.269	1.311	1.349	1.378	1.403
.495 13 0	.623	.664	.792	.909	1.014	1.077	1.127	1.166	1.191	1.219	1.251	1.280	1.292
.564 17 0	.721	.726	.788	.866	.940	1.013	1.076	1.118	1.162	1.204	1.253	1.285	1.288
.685 53 0	.814	.824	.848	.886	.941	1.000	1.049	1.078	1.105	1.127	1.180	1.227	1.226
.824 57 0	.914	.927	.950	.968	.986	1.021	1.049	1.060	1.075	1.089	1.112	1.154	1.196
.940 93 0	.898	.902	.925	.952	.983	1.010	1.028	1.031	1.016	1.007	1.093	1.171	1.180
1.027 93 0	.944	.891	.905	.931	.949	.966	.998	1.013	1.043	1.074	1.085	1.066	1.071
1.161 57 0	.981	.921	.918	.920	.933	.946	.978	1.003	1.025	1.026	1.040	1.061	1.054
1.283 53 0	.932	.911	.916	.909	.936	.972	.968	.966	1.007	1.038	1.050	1.061	1.073
1.432 17 0	.904	.932	.959	.956	.932	.941	.969	.994	1.024	1.048	1.042	1.056	1.061

LOCAL FLOW FIELD DATA

MACH = 1.964 RE = 9.79X10 FT ALPHA = 9.950 X/D = 4.100 TEST NO. = 33

(VC / VIN * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 9 0	.887	.523	.840	1.251	.916	.669	1.113	1.426	1.588	1.584	1.730	1.860	1.935
.438 5 0	1.256	1.247	1.179	.877	1.005	1.481	1.646	1.815	1.869	1.888	1.885	1.844	1.671
.495 9 0	1.569	1.640	1.838	1.979	2.013	1.964	1.812	1.645	1.536	1.446	1.189	1.196	1.229
.564 21 1	.758	.967	1.325	1.579	1.650	1.589	1.439	1.279	1.176	1.214	1.234	1.255	1.279
.685 49 0	.803	.815	.856	.907	.980	1.041	1.084	1.109	1.129	1.153	1.190	1.221	1.224
.824 61 0	.895	.904	.930	.952	.987	1.029	1.067	1.074	1.074	1.086	1.109	1.127	1.157
.940 89 0	.878	.880	.899	.927	.942	.964	.982	.991	1.008	1.003	1.072	1.136	1.143
1.027 89 0	.940	.884	.897	.917	.945	.978	1.005	1.016	1.040	1.069	1.073	1.042	1.061
1.161 61 0	.976	.930	.926	.933	.941	.949	.984	1.019	1.029	1.017	1.034	1.058	1.058
1.283 49 0	.952	.933	.929	.920	.932	.951	.956	.961	1.006	1.014	1.028	1.080	1.089
1.432 21 1	.919	.949	.973	.978	.965	.971	.983	1.027	1.059	1.063	1.072	1.107	1.119

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 0.81X10⁶ FT ALPHA = 9.950 X/D = 4.400 TEST NO. = 35

(VC / VINF * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.364 25 1	1.659	1.597	1.521	1.358	1.283	1.556	1.901	1.994	2.000	2.018	2.028	2.022	1.995
.685 45 0	1.711	1.710	1.761	1.875	1.987	2.027	1.979	1.899	1.869	1.878	1.873	1.841	1.793
.824 65 0	1.637	1.678	1.753	1.819	1.847	1.879	1.798	1.687	1.664	1.609	1.438	1.216	1.049
.940 85 0	1.052	.970	.946	.984	1.007	1.040	1.060	1.062	1.072	1.072	1.074	1.111	1.156
1.027 85 0	.897	.873	.881	.919	.947	.978	1.023	1.035	1.051	1.068	1.073	1.066	1.083
1.161 65 0	.975	.933	.926	.925	.943	.954	.985	1.007	1.027	1.016	1.029	1.043	1.029
1.283 45 0	.961	.937	.932	.924	.938	.949	.960	.968	1.005	1.005	1.019	1.075	1.054
1.432 25 1	.941	.954	.990	.990	.977	.973	1.002	1.020	1.036	1.051	1.054	1.087	1.118

LOCAL FLOW FIELD DATA

MACH = 1.969 RE = 9.81x10⁶ FT ALPHA = 9.950 X/D = 4.800 TEST NO. = 35

(VC / VINF * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 29 0	.272	.433	.473	.407	.439	.423	.756	1.109	1.242	1.276	1.270	1.257	1.256
.685 41 0	.179	.186	.498	.365	.794	1.202	1.152	1.144	1.114	1.094	1.119	1.161	1.186
.824 69 0	1.269	1.225	1.188	1.220	1.323	1.419	1.466	1.476	1.463	1.445	1.425	1.394	1.346
.940 81 0	1.552	1.549	1.545	1.552	1.604	1.661	1.701	1.696	1.667	1.641	1.603	1.554	1.490
1.027 81 0	1.632	1.623	1.583	1.577	1.624	1.652	1.668	1.662	1.631	1.589	1.553	1.501	1.450
1.161 69 0	1.761	1.756	1.695	1.643	1.669	1.702	1.692	1.691	1.677	1.639	1.596	1.528	1.446
1.283 41 0	1.745	1.760	1.719	1.672	1.671	1.710	1.799	1.852	1.555	1.469	1.415	.947	1.122
1.432 29 0	.947	.964	.986	.994	.979	.981	.990	1.033	1.060	1.055	1.058	1.090	1.105

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.961 RE = 9.78X10 FT ALPHA = 0.950 X/D = 6.500 TEST NO. = 35

(VC / VINF * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 33 0	.075	.184	.371	.312	.460	1.121	1.506	1.611	1.681	1.731	1.802	1.827	1.804
.633 97 0	.154	.061	.143	.736	1.039	1.130	1.262	1.399	1.501	1.617	1.706	1.722	1.704
.685 37 0	.100	.288	.249	.810	1.087	1.099	1.199	1.313	1.419	1.514	1.560	1.564	1.567
.765 101 0	.334	.369	.644	.999	1.116	1.146	1.231	1.300	1.379	1.444	1.480	1.478	1.477
.824 73 0	.251	.326	.701	1.014	1.081	1.119	1.209	1.267	1.336	1.377	1.394	1.379	1.379
.904 105 0	.522	.584	.755	.950	1.020	1.085	1.187	1.263	1.301	1.327	1.379	1.372	1.339
.940 77 0	.502	.557	.711	.893	.995	1.063	1.153	1.225	1.267	1.294	1.344	1.348	1.314
.999 109 0	.574	.603	.714	.867	.967	1.081	1.166	1.216	1.234	1.243	1.259	1.236	1.265
1.027 77 0	.602	.573	.663	.791	.923	1.000	1.067	1.120	1.172	1.215	1.236	1.248	1.262
1.161 73 0	.660	.663	.709	.796	.898	.980	1.017	1.065	1.105	1.124	1.160	1.223	1.123
1.283 37 0	.619	.664	.713	.769	.879	.941	1.001	1.049	1.097	1.132	1.187	1.178	1.124
1.432 33 0	.603	.631	.690	.739	.839	.919	.972	.998	1.069	1.162	1.139	1.128	1.138
1.538 97 0	.637	.567	.574	.693	.811	.869	.924	.956	1.029	1.066	1.057	1.039	1.068
1.680 101 0	.525	.531	.624	.709	.791	.840	.875	.934	1.006	1.026	1.027	1.025	1.035
1.798 105 0	.644	.658	.700	.737	.797	.843	.883	.939	.995	1.004	1.008	1.008	1.010
1.923 109 0	.788	.773	.799	.840	.895	.921	.937	.996	1.029	1.026	1.026	1.015	1.025

LOCAL FLOW FIELD DATA

MACH = 1.957 $RE = 9.80 \times 10^6$ $\alpha = 9.950$ $X/D = 3.500$ TEST NO. = 35

AXIAL VELOCITY RATIO -- (V_X / V_{INF}) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 1 0	.978	.980	.854	.742	.690	.767	.912	.951	.889	.938	.980	.979	.966
.395 13 0	1.007	.997	.990	.991	.988	.985	.984	.983	.983	.982	.978	.977	.979
.438 1 0	.986	.986	.988	.988	.985	.983	.984	.988	.988	.987	.986	.986	.989
.495 13 0	.985	.986	.986	.983	.981	.979	.978	.978	.977	.979	.982	.984	.987
.564 17 0	.992	.989	.988	.992	.993	.991	.986	.982	.984	.987	.990	.991	.992
.685 33 0	.981	.979	.980	.982	.984	.982	.981	.981	.982	.983	.982	.983	.983
.824 57 0	.976	.973	.975	.980	.981	.982	.984	.985	.987	.991	.989	.983	.981
.940 93 0	.974	.971	.974	.977	.976	.983	.990	.993	.998	1.007	.999	.992	.992
1.027 93 0	.990	.992	.989	.988	.989	.987	.989	.992	.995	.995	.995	.993	.987
1.161 57 0	.986	.992	.988	.986	.985	.982	.984	.992	.999	.999	.998	.996	.989
1.283 53 0	.985	.988	.987	.984	.984	.984	.989	.994	.999	1.000	.995	.994	.988
1.432 17 0	.989	.989	.983	.979	.985	.994	.993	.991	.994	.996	.995	.993	.998

LOCAL FLOW FIELD DATA

MACH = 1.984 $RE = 9.79 \times 10^6$ FT $\alpha = 9.950$ $X/D = 4.100$ TEST NO. = 35

AXIAL VELOCITY RATIO -- (V_x / V_{INF}) --

THETA		180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D	RUN NO.													
.395	9 0	.782	.738	.419	.462	.424	.452	.783	.944	.923	.938	.862	.785	.754
.438	5 0	.740	.819	.905	.845	.820	.922	.897	.780	.700	.669	.656	.599	.531
.495	9 0	.610	.639	.713	.759	.765	.769	.792	.824	.855	.841	.901	.960	.967
.564	21 1	.957	.927	.868	.839	.843	.865	.869	.907	.970	.988	.985	.986	.986
.685	49 0	.976	.971	.971	.977	.981	.980	.979	.979	.981	.981	.982	.981	.980
.824	61 0	.976	.974	.975	.981	.980	.981	.984	.984	.985	.988	.986	.979	.976
.940	89 0	.977	.974	.975	.978	.982	.988	.996	.997	.996	1.001	.993	.986	.987
1.027	89 0	.990	.992	.989	.988	.987	.985	.988	.990	.991	.991	.991	.992	.983
1.161	61 0	.984	.992	.987	.984	.983	.981	.982	.987	.993	.994	.994	.993	.988
1.283	49 0	.986	.991	.987	.983	.983	.983	.984	.988	.994	.993	.989	.988	.989
1.432	21 1	.989	.986	.983	.977	.980	.987	.988	.988	.986	.990	.993	.995	.989

LOCAL FLOW FIELD DATA

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MACH = 1.959 RE = 9.81x10 FT ALPHA = 9.950 X/D = 4.400 TEST NO. = 35

AXIAL VELOCITY RATIO -- (VX / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 25 1	.792	.798	.849	.847	.811	.780	.755	.753	.757	.750	.739	.720	.706
.685 45 0	.779	.781	.792	.793	.780	.775	.779	.775	.761	.738	.725	.722	.717
.824 65 0	.843	.823	.800	.779	.775	.685	.648	.685	.713	.751	.812	.866	.917
.940 85 0	.930	.953	.972	.976	.976	.984	.989	.988	.989	.994	.996	.988	.983
1.027 85 0	.983	.987	.985	.988	.989	.985	.986	.990	.992	.992	.989	.987	.982
1.161 65 0	.983	.991	.986	.983	.982	.980	.980	.986	.993	.993	.993	.990	.983
1.283 45 0	.986	.993	.988	.985	.984	.983	.984	.989	.995	.993	.990	.989	.986
1.432 25 1	.985	.983	.979	.976	.978	.982	.983	.982	.985	.986	.985	.986	.995

LOCAL FLOW FIELD DATA

MACH = 1.969 RE = 9.81X10 FT ALPHA = 9.950 X/D = 4.800 TEST NO. = 35

AXIAL VELOCITY RATIO -- (VX / VIN) --

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 29 0	1.107	1.082	.937	.886	.929	.920	.979	1.047	1.050	1.046	1.053	1.044	1.027
.685 41 0	1.090	1.094	.998	.997	.985	1.004	1.063	1.078	1.070	1.060	1.049	1.034	1.025
.824 69 0	.965	.968	.964	.966	.969	.969	.962	.954	.945	.932	.923	.917	.911
.940 81 0	.895	.896	.901	.903	.904	.901	.891	.881	.876	.873	.867	.861	.858
1.027 81 0	.861	.861	.867	.874	.869	.865	.856	.846	.840	.837	.835	.832	.831
1.161 69 0	.826	.831	.842	.850	.845	.830	.820	.815	.812	.809	.808	.805	.799
1.283 41 0	.821	.825	.824	.832	.835	.823	.752	.637	.738	.805	.783	1.013	.945
1.432 29 0	.983	.984	.980	.975	.980	.986	.986	.984	.981	.982	.985	.988	.982

LOCAL FLOW FIELD DATA

MACH = 1.961 RE = 9.78X10 FT ALPHA = 9.950 X/D = 6.500 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 33 0	.947	.918	.855	.823	.820	.895	.957	.947	.920	.908	.908	.909	.908
.633 97 0	.984	.965	.913	.858	.928	.993	.994	.989	.982	.980	.979	.975	.971
.685 37 0	.990	.980	.898	.861	.946	1.004	1.011	.996	.988	.990	.989	.985	.980
.765 101 0	.985	.988	.935	.904	.955	.995	.995	.991	.990	.987	.981	.975	.970
.824 73 0	.991	.991	.972	.972	.994	1.003	1.002	.998	.998	.994	.985	.975	.970
.904 105 0	.982	.988	.988	.988	.993	.993	.996	.996	.994	.990	.983	.980	.979
.940 77 0	.985	.989	.997	.998	1.000	1.000	1.000	1.001	1.002	.996	.986	.978	.978
.999 109 0	.988	.994	1.001	1.001	.996	.996	1.000	.999	.995	.993	.989	.979	.980
1.027 77 0	.998	1.013	1.008	1.004	1.000	.995	.999	1.001	.996	.991	.988	.983	.982
1.161 73 0	1.008	1.011	1.010	1.003	1.002	1.009	1.005	1.001	.998	.993	.991	.997	.980
1.283 37 0	1.017	1.019	1.012	1.012	1.026	1.016	1.004	1.000	.996	.995	.997	.989	.981
1.432 33 0	1.030	1.031	1.026	1.033	1.025	1.014	1.005	.993	.993	1.005	.997	.990	.994
1.538 97 0	1.028	1.020	1.048	1.038	1.029	1.020	1.004	1.000	1.011	1.004	1.001	.993	.994
1.680 101 0	1.055	1.044	1.041	1.036	1.030	1.023	1.022	1.025	1.019	1.016	1.010	.996	.989
1.798 105 0	1.038	1.032	1.033	1.029	1.027	1.022	1.018	1.016	1.011	1.006	.996	.988	.981
1.923 109 0	1.019	1.015	1.013	1.012	1.010	1.005	.999	.998	.995	.985	.978	.976	.969

LOCAL VORTICITY X 100.

MACH = 1.937 RE = 9.60x10 FT ALPHA = 9.950 X/D = 3.500 TEST NO. = 35

THETA 176.25 166.75 161.25 153.75 146.25 138.75 131.25 123.75 116.25 108.75 101.25 93.75

R/D

.3550	18.067	53.464	83.599	55.231	11.475	6.548	30.003	38.239	8.818	-4.429	7.642	11.798
.4165	-15.168	-22.801	-14.025	-14.947	-13.934	-12.306	-11.191	-10.774	-10.795	-9.320	-6.290	-7.650
.4665	.687	4.949	5.536	2.506	.767	.556	-.542	-2.186	-2.944	-3.423	-2.937	-3.478
.5295	-1.269	-2.040	-1.251	-2.323	-3.745	-1.817	-.160	.225	1.226	2.207	2.902	3.186
.6245	.446	.096	.299	1.339	1.359	.850	.692	.361	-.556	-1.159	-1.153	.067
.7545	.394	.047	.094	.385	.558	.370	.017	-.590	-.889	-1.024	-2.118	-.790
.8820	.153	-.284	-.553	.422	.543	-.454	-.659	-1.693	-3.024	-1.633	-.122	.477
.9835	-.796	-.273	-1.646	-2.178	-1.506	-.343	.425	1.715	3.624	2.654	-2.352	-4.836
1.0940	-1.497	.202	-.238	-.523	-.961	-.660	-.562	-.397	-.504	-.589	-.586	-.613
1.2220	-.481	1.247	.347	.190	.602	.189	-.950	-.486	1.033	1.278	.655	.377
1.3575	-.180	.100	-.069	-.017	.088	.157	.367	.800	.714	.370	.752	.407

LOCAL VORTICITY X 100.

MACH = 1.984 RE = 9.79x10 FT ALPHA = 9.950 X/D = 4.100 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.4165	17.715	93.692	80.154	66.186	62.301	64.155	10.677	-35.421	-39.982	-1.810	-.885	-25.681
.4665	-12.463	-13.338	-1.008	-5.201	-26.041	-24.009	-8.454	-4.982	-8.213	-20.893	-6.558	13.584
.5295	14.159	23.388	16.399	13.224	12.528	6.686	.456	-2.784	12.524	5.745	2.488	7.020
.6245	1.680	2.695	1.601	1.087	1.680	2.015	2.537	-3.858	-1.802	.593	.617	.774
.7545	-.964	-1.477	-1.145	-.040	.220	-.107	-.640	-1.237	-1.316	-1.656	-2.052	-1.532
.8820	-.112	-.558	-.890	-.602	-1.162	-2.397	-2.632	-2.360	-2.796	-2.112	-.357	.169
.9835	-.321	.469	-1.120	-.677	1.502	2.638	2.714	3.028	3.861	2.849	-1.845	-4.331
1.0940	-1.429	.035	-.431	-.789	-1.208	-.936	-.288	-.470	-.927	-.545	-.097	-.515
1.2220	-.522	.740	.168	-.466	-.111	.157	-.391	-.325	.940	1.123	.809	-.117
1.3575	-.264	-.588	-.479	.011	-.051	-.575	-.013	.832	.463	.849	1.412	.900

LOCAL VORTICITY X 100.

+6 -1

MACH = 1.959 RE = 9.81X10 FT ALPHA = 9.950 X/D = 4.400 TEST NO. = 35

THETA 176.25 166.75 161.25 153.75 146.25 138.75 131.25 123.75 116.25 108.75 101.25 93.75

R/D

.6245	-2.496	-3.431	-3.332	1.190	7.065	9.817	2.679	-.791	.373	1.066	.444	-.193
.7545	-.028	-.055	.585	.904	2.332	-.595	-3.737	.905	3.041	-1.191	-5.350	-7.182
.8620	.329	2.662	3.824	3.269	3.818	5.681	5.958	4.657	3.293	1.548	.418	-.138
.9835	-2.416	-1.931	-1.101	-1.582	-1.482	.420	1.701	1.814	2.246	1.949	-.557	-2.390
1.0940	-1.545	-1.071	-1.194	-1.253	-1.760	-1.849	-1.679	-1.626	-1.409	-1.102	-1.082	-1.411
1.2220	-.477	.531	-.025	-.035	.022	.136	.087	.072	.741	.987	1.097	.319
1.3575	-.840	-.461	-.364	-.635	-.812	-.606	-.125	.463	.503	.651	.588	.862

LOCAL VORTICITY X 100.

MACH = 1.969 RE = 9.61X10 FT ALPHA = 9.950 X/D = 4.800 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.6245	-2.846	11.698	19.260	60.276	39.334	12.219	6.324	2.545	1.417	1.940	2.755	3.741
.7545	-.613	-2.278	-6.450	15.473	7.943	-5.120	-3.265	-1.079	-.602	.111	-.613	-1.650
.8620	-1.015	-1.289	-1.530	-.907	-.332	.297	-.206	-.557	.312	.189	-.225	-.622
.9835	2.790	4.204	2.375	2.638	3.322	3.735	3.057	3.444	4.580	4.535	3.566	3.076
1.0940	.021	-.977	-1.161	-.031	.066	-.159	.146	-.289	-.548	-.349	-.645	-1.357
1.2220	1.105	.724	.137	.634	1.330	1.877	.893	-5.131	-.656	1.275	-10.918	3.649
1.3575	-.577	-1.935	-1.673	-1.131	.180	2.323	4.167	.576	2.176	3.245	-6.370	1.764

LOCAL VORTICITY X 100.

MACH = 1.961 $Re = 9.78 \times 10^6$ FT ALPHA = 9.930 X/D = 8.500 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.5985	2.053	20.527	27.230	17.600	7.644	.249	.472	4.490	6.350	7.347	7.224	6.928
.6390	-11.248	17.059	53.759	15.955	-6.447	-2.974	-1.540	-2.353	-1.903	-2.647	-3.994	-3.455
.7250	1.469	23.187	44.300	19.233	.714	2.300	4.764	3.226	1.915	2.059	2.066	1.999
.7945	-4.024	2.469	16.567	5.674	-2.676	-1.326	-.381	-.567	-.237	-.868	-1.915	-2.356
.8640	.951	2.346	5.891	2.648	.256	.618	1.969	2.182	1.608	2.256	3.467	2.077
.9220	-1.699	-3.001	-2.227	-3.030	-1.942	-3.046	-3.823	-2.275	-.551	-.635	.057	-.108
.9695	-.009	.007	.963	1.891	4.565	4.900	3.693	2.670	.996	-1.636	-3.900	-3.797
1.0130	-3.133	-4.949	-8.688	-6.993	-8.464	-11.641	-12.425	-8.268	-2.555	-.281	1.910	2.788
1.0940	-1.752	-.792	-.476	-1.007	-1.233	.794	.062	-.229	-.821	-1.169	-1.453	.116
1.2220	.618	.990	1.008	1.773	2.079	1.836	2.379	2.246	1.972	2.156	1.030	1.211
1.3575	-.210	.200	.062	-.424	.333	.776	.246	.020	.152	.932	.794	1.202
1.4850	-1.259	-.186	.083	-.154	-.658	-.842	-1.359	-1.613	-1.425	-1.949	-1.935	-1.782
1.6090	.037	.181	.063	-.252	-.541	.133	.320	-.435	.452	.135	-.158	-.109
1.7390	-1.206	-1.458	-1.413	-1.357	-.694	-.778	-.945	-.661	-.609	-.485	-.527	-.453
1.8605	1.046	1.902	1.645	2.066	1.308	.694	1.644	1.746	1.014	.781	.866	.575

LOCAL CIRCULATION STRENGTH X 100.

*8 -1

MACH = 1.937 RE = 9.60x10 FT ALPHA = 9.950 X/D = 3.500 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.3550	.086	.253	.396	.261	.054	.031	.142	.181	.042	-.021	.036	.056	1.5168
.4165	-.045	-.068	-.042	-.045	-.042	-.037	-.033	-.032	-.032	-.028	-.019	-.023	-.4454
.4665	.003	.022	.025	.011	.003	.002	-.002	-.010	-.013	-.015	-.013	-.015	-.0023
.5295	-.008	-.012	-.008	-.014	-.023	-.011	-.001	.001	.007	.013	.018	.019	-.0174
.6245	.006	.001	.004	.017	.017	.011	.009	.005	-.007	-.015	-.015	.001	.0333
.7545	.007	.001	.002	.007	.010	.006	.000	-.010	-.016	-.018	-.037	-.014	-.0620
.8820	.003	-.005	-.009	.007	.009	-.008	-.011	-.029	-.052	-.028	-.002	.008	-.1164
.9835	-.011	-.004	-.023	-.031	-.021	-.005	.006	.024	.052	.038	-.034	-.069	-.0786
1.0940	-.037	.003	-.006	-.013	-.023	-.016	-.014	-.010	-.012	-.014	-.014	-.015	-.1693
1.2220	-.012	.031	.009	.005	.015	.005	-.024	-.012	.026	.032	.016	.009	.0994
1.3575	-.006	.003	-.002	-.001	.003	.005	.012	.027	.024	.012	.025	.014	.1177
RSUM	-.015	.227	.344	.205	.002	-.016	.084	.136	.019	-.043	-.036	-.029	.8758

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = 1.964 RE = 9.79X10 FT ALPHA = 9.950 X/D = 4.100 TEST NO. = 35

THETA	176.25	166.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.4165	.053	.280	.239	.198	.186	.191	.032	-.106	-.119	-.005	-.003	-.077	.8689
.4665	-.055	-.039	-.004	-.023	-.115	-.106	-.037	-.022	-.036	-.093	-.029	.060	-.5211
.5295	.086	.142	.100	.081	.076	.041	.003	-.017	.076	.035	.015	.043	.6810
.6245	.021	.034	.020	.014	.021	.025	.032	-.049	-.023	.007	.008	.010	.1211
.7545	-.017	-.026	-.020	-.001	.004	-.002	-.011	-.022	-.023	-.029	-.036	-.027	-.2088
.8820	-.002	-.010	-.015	-.010	-.020	-.041	-.045	-.040	-.046	-.036	-.006	.003	-.2696
.9835	-.005	.007	-.016	-.010	.021	.038	.039	.043	.055	.041	-.026	-.062	.1250
1.0940	-.035	.001	-.011	-.019	-.030	-.023	-.007	-.011	-.023	-.013	-.002	-.013	-.1857
1.2220	-.013	.018	.004	-.012	-.003	.004	-.010	-.008	.023	.028	.020	-.003	.0498
1.3575	-.009	-.020	-.016	.000	-.002	-.019	-.000	.028	.016	.029	.048	.030	.0842
RSUM	.025	.368	.281	.218	.139	.108	-.005	-.204	-.101	-.037	-.012	-.035	.7449

LOCAL CIRCULATION STRENGTH X 100.

MACH = 1.959 RE = 9.81x10 FT ALPHA = 9.950 X/D = 4.400 TEST NO. = 35

THETA	176.25	166.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.6245	-.031	-.043	-.042	.015	.089	.124	.034	-.010	.005	.013	.006	-.002	.1561
.7545	-.000	-.001	.010	.016	.041	-.010	-.065	.016	.053	-.021	-.094	-.126	-.1813
.8820	.006	.045	.065	.056	.065	.097	.102	.079	.056	.026	.007	-.002	.6023
.9835	-.034	-.028	-.016	-.023	-.021	.006	.024	.026	.032	.028	-.008	-.034	-.0475
1.0940	-.038	-.026	-.029	-.031	-.043	-.045	-.041	-.040	-.034	-.027	-.026	-.034	-.4149
1.2220	-.012	.013	-.001	-.001	.001	.003	.002	.002	.018	.025	.027	.008	.0858
1.3575	-.028	-.016	-.012	-.021	-.027	-.020	-.004	.016	.017	.022	.020	.029	-.0261
RSUM	-.139	-.055	-.024	.011	.104	.154	.051	.089	.147	.066	-.068	-.162	.1743

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = 1.969 RE = 9.81X10 FT ALPHA = 9.950 X/D = 4.800 TEST NO. = 35

THETA	176.25	166.75	161.25	155.75	146.25	136.75	131.25	125.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.6245	-.036	.147	.243	.759	.495	.154	.080	.032	.018	.024	.035	.047	1.9982
.7545	-.011	-.040	-.113	.270	.139	-.089	-.057	-.019	-.011	.002	-.011	-.029	.0325
.8820	-.017	-.022	-.026	-.015	-.006	.005	-.004	-.010	.005	.003	-.004	-.011	-.1004
.9835	.040	.060	.034	.038	.047	.053	.044	.049	.065	.065	.051	.044	.5893
1.0940	.001	-.024	-.028	-.001	.002	-.004	.004	-.007	-.013	-.009	-.016	-.033	-.1291
1.2220	.027	.018	.003	.016	.033	.047	.022	-.128	-.016	.032	-.271	.091	-.1263
1.3575	-.019	-.065	-.056	-.038	.006	.078	.140	.019	.075	.109	-.215	.059	.0925
RSUM	-.016	.074	.056	1.029	.717	.244	.229	-.062	.122	.227	-.431	.169	2.3567

LOCAL CIRCULATION STRENGTH X 100.

MACH = 1.961 RE = 9.78x10⁶ FT ALPHA = 9.950 X/D = 6.500 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.9985	.014	.141	.187	.121	.053	.002	.003	.031	.044	.051	.050	.048	.7441
.6590	-.064	.097	.307	.091	-.037	-.017	-.009	-.013	-.011	-.015	-.023	-.020	.2868
.7250	.014	.224	.428	.186	.007	.022	.046	.031	.019	.020	.020	.019	1.0366
.7945	-.031	.019	.129	.044	-.021	-.010	-.003	-.004	-.002	-.007	-.015	-.018	.0809
.8640	.011	.027	.068	.031	.003	.007	.023	.025	.019	.026	.040	.024	.3026
.9220	-.009	-.017	-.012	-.017	-.011	-.017	-.021	-.013	-.003	-.004	.000	-.001	-.1233
.9695	-.000	.000	.009	.018	.044	.047	.035	.025	.009	-.016	-.037	-.036	.0986
1.0130	-.015	-.023	-.041	-.043	-.040	-.035	-.059	-.039	-.012	-.001	.009	.013	-.3059
1.0940	-.043	-.019	-.012	-.025	-.030	.019	.002	-.006	-.020	-.029	-.035	.003	-.1945
1.2220	.020	.025	.025	.044	.052	.046	.059	.056	.049	.054	.026	.030	.4845
1.3575	-.007	.007	.002	-.014	.011	.026	.008	.001	.005	.031	.027	.041	.1376
1.4850	-.033	-.005	.002	-.004	-.017	-.022	-.036	-.042	-.037	-.051	-.051	-.047	-.3432
1.6090	.001	.007	.002	-.010	-.021	.005	.020	-.017	.017	.005	-.006	-.004	.0010
1.7390	-.041	-.050	-.048	-.046	-.024	-.027	-.032	-.023	-.021	-.017	-.018	-.015	-.3621
1.8605	.041	.074	.064	.080	.051	.027	.064	.068	.039	.030	.034	.022	.5925
RSUM	-.143	.507	1.111	.457	.019	.053	.100	.080	.095	.078	.020	.059	2.4365

SECTION VI $M_\infty=1.96, \alpha=14.5^\circ, Re=9.8 \times 10^6 ft^{-1},$ $X/D = 3.5, 4.1, 4.4, 4.8, 6.5$

LOCAL FLOW FIELD DATA

MACH = 1.963 RE = 9.80x10⁺⁶ FT ALPHA = 14.530 X/D = 3.500 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 2 1 2.040	1.999	1.924	1.790	1.682	1.573	1.550	1.466	1.307	1.546	1.922	1.768	1.611	
.395 14 0 2.017	1.985	1.992	1.831	1.783	1.953	2.128	2.169	2.104	2.068	2.031	1.989	2.047	
.438 2 1 1.939	1.937	1.967	2.049	2.100	2.178	2.187	2.133	2.084	2.066	2.057	2.014	2.041	
.495 14 0 1.918	1.922	1.932	1.974	2.008	2.016	2.015	2.006	1.997	2.002	1.984	2.022	2.104	
.564 18 0 1.949	1.933	1.937	1.969	2.000	2.019	2.033	2.033	2.027	2.024	2.022	2.027	2.090	
.685 54 0 1.922	1.911	1.917	1.938	1.950	1.951	1.967	1.981	1.981	1.977	1.963	2.016	2.052	
.824 58 0 1.924	1.922	1.926	1.939	1.949	1.960	1.971	1.979	1.982	1.976	1.955	1.989	2.010	
.940 94 0 1.924	1.929	1.926	1.936	1.963	1.973	1.985	2.004	2.013	2.015	2.030	2.044	2.034	
1.027 94 0 1.986	1.966	1.965	1.958	1.960	1.965	1.965	1.971	1.993	2.018	2.028	2.018	1.975	
1.161 58 0 1.972	1.962	1.961	1.960	1.972	1.974	1.976	1.994	2.021	2.018	2.015	2.010	1.983	
1.283 54 0 1.956	1.951	1.966	1.960	1.955	1.967	1.990	1.987	2.012	2.028	2.009	1.996	1.995	
1.432 18 0 1.959	1.940	1.944	1.939	1.958	1.973	1.983	1.992	1.996	2.005	1.993	1.973	2.000	

LOCAL FLOW FIELD DATA

+8 -1

MACH = 1.961 RE = 9.79X10 FT ALPHA = 14.530 X/D = 4.100 TEST NO. = 55

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 10 0	.857	.855	.792	.668	1.022	1.505	1.422	1.522	1.554	1.796	1.692	1.743	1.526
.438 6 0	.958	.971	1.333	1.234	1.138	1.275	1.329	1.579	1.807	1.754	1.542	1.341	1.225
.495 10 0	1.893	1.886	1.525	1.442	1.558	1.547	1.516	1.491	1.513	1.370	1.390	1.706	1.903
.564 22 0	1.925	1.936	1.966	1.724	1.503	1.461	1.528	1.594	1.740	1.933	2.004	2.004	1.983
.685 50 0	1.899	1.902	1.915	1.939	1.959	1.978	2.007	2.016	2.004	1.995	1.989	1.975	1.963
.824 62 0	1.911	1.909	1.914	1.932	1.942	1.943	1.962	1.972	1.970	1.959	1.939	1.925	1.963
.940 90 0	1.931	1.930	1.928	1.945	1.966	1.986	2.006	2.014	2.023	2.023	2.004	2.017	2.038
1.027 90 0	1.986	1.968	1.966	1.963	1.964	1.962	1.976	1.989	1.993	1.989	1.985	2.001	2.046
1.161 62 0	1.955	1.952	1.957	1.957	1.962	1.968	1.972	1.969	1.964	1.973	1.986	2.006	1.979
1.283 50 0	1.953	1.950	1.962	1.949	1.942	1.959	1.978	1.963	1.981	2.003	2.000	2.012	2.013
1.432 22 0	1.951	1.936	1.942	1.938	1.941	1.948	1.960	1.964	1.972	1.988	2.006	1.993	2.020

LOCAL FLOW FIELD DATA

*8 -1

MACH = 1.959 RE = 9.61x10 FT ALPHA = 14.530 X/D = 4.400 TEST NO. = 35

LOCAL MACH NO. -- (H) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.364 26 0	1.450	1.493	1.389	1.061	1.018	1.245	1.143	1.238	1.525	1.596	1.576	1.522	1.469
.685 46 0	1.464	1.489	1.551	1.643	1.670	1.623	1.560	1.530	1.496	1.469	1.445	1.406	1.366
.824 66 0	1.340	1.261	1.414	1.562	1.523	1.477	1.453	1.477	1.235	1.044	1.149	1.279	1.342
.940 86 0	1.938	1.940	1.717	1.544	1.474	1.608	1.866	2.004	2.022	2.011	1.991	1.979	2.002
1.027 86 0	1.978	1.960	1.958	1.961	1.965	1.965	1.973	1.986	1.990	1.987	1.987	1.983	1.981
1.161 66 0	1.954	1.947	1.955	1.953	1.953	1.964	1.970	1.962	1.954	1.962	1.958	1.972	1.970
1.283 46 0	1.957	1.951	1.961	1.948	1.946	1.964	1.977	1.968	1.983	1.995	1.986	2.008	2.026
1.432 26 0	1.960	1.942	1.943	1.937	1.949	1.958	1.957	1.954	1.962	1.978	1.984	2.002	2.012

LOCAL FLOW FIELD DATA

MACH = 1.956 $RE = 9.61 \times 10^6$ FT $\alpha = 14.530$ $X/D = 4.600$ TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 30 0	2.186	2.269	2.491	2.155	1.839	1.723	1.621	1.982	2.237	2.191	2.217	2.191	2.124
.685 42 0	2.112	2.246	2.404	2.030	1.635	1.726	1.612	2.195	2.402	2.320	2.228	2.215	2.209
.824 70 0	1.835	1.885	1.921	1.848	1.893	2.021	2.055	2.011	1.935	1.885	1.861	1.844	1.811
.940 82 0	1.727	1.764	1.773	1.834	1.883	1.916	1.879	1.824	1.785	1.750	1.704	1.695	1.678
1.027 82 0	1.672	1.690	1.729	1.769	1.789	1.782	1.737	1.712	1.673	1.647	1.638	1.620	1.575
1.161 70 0	1.605	1.632	1.703	1.718	1.715	1.700	1.645	1.608	1.589	1.580	1.567	1.548	1.516
1.283 42 0	1.597	1.626	1.667	1.663	1.659	1.656	1.610	1.559	1.550	1.586	1.142	1.354	1.792
1.432 30 0	1.486	1.457	1.538	1.635	1.610	1.421	1.330	1.634	1.972	1.962	1.952	1.967	2.040

LOCAL FLOW FIELD DATA

MACH = 1.956 RE = 9.78X10⁶ FT ALPHA = 14.530 X/D = 6.500 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 34 0	1.624	1.647	1.512	1.548	1.684	1.419	1.696	2.272	2.144	1.899	1.899	1.816	1.836
.633 98 0	1.955	1.960	1.964	1.835	1.821	1.934	2.047	2.104	2.158	2.191	2.170	2.139	2.160
.685 38 0	1.952	1.950	1.822	1.782	1.876	1.992	2.032	2.109	2.166	2.153	2.130	2.113	2.133
.765 102 0	1.972	1.899	1.634	1.661	1.880	1.986	2.044	2.125	2.145	2.119	2.083	2.028	2.028
.824 74 0	1.979	1.858	1.561	1.644	1.960	2.022	2.057	2.114	2.109	2.077	2.029	2.005	2.007
.904 106 0	1.968	1.851	1.749	1.803	1.974	2.035	2.061	2.097	2.104	2.074	2.023	2.023	2.028
.940 78 0	1.939	1.848	1.797	1.887	2.047	2.072	2.107	2.137	2.125	2.085	2.024	2.029	2.037
.999 110 0	1.897	1.872	1.893	1.967	2.042	2.030	2.053	2.074	2.070	2.040	1.983	2.009	2.028
1.027 78 0	1.923	1.994	1.973	1.972	2.043	2.063	2.096	2.089	2.083	2.053	2.015	1.988	2.050
1.161 74 0	1.876	1.980	1.950	1.955	2.097	2.073	2.042	2.033	2.058	2.006	1.985	2.001	1.971
1.263 38 0	1.994	1.941	1.905	2.116	2.101	2.072	2.039	2.029	2.046	1.995	1.991	2.018	1.963
1.432 34 0	2.016	2.003	2.081	2.097	2.081	2.043	2.015	1.995	1.999	1.986	2.016	1.972	1.986
1.538 98 0	2.182	2.133	2.128	2.102	2.081	2.054	2.028	2.013	2.003	2.045	2.022	1.986	1.994
1.680 102 0	2.197	2.160	2.129	2.088	2.066	2.032	1.999	2.025	2.097	2.058	2.029	1.996	1.982
1.798 106 0	2.167	2.151	2.127	2.089	2.077	2.031	2.033	2.117	2.089	2.056	2.013	1.977	1.954
1.923 110 0	2.126	2.108	2.090	2.071	2.067	2.058	2.059	2.046	2.025	1.980	1.947	1.916	1.907

LOCAL FLOW FIELD DATA

MACH = 1.963 RE = 9.80x10 FT ALPHA = 14.530 X/D = 3.500 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 2 1	5.206	6.185	9.511	14.090	15.609	18.068	19.779	15.064	15.484	26.300	24.829	24.060	26.457
.395 14 0	3.824	6.363	11.715	16.811	22.231	24.919	25.212	24.979	23.781	21.863	20.710	20.343	24.453
.438 2 1	.363	3.101	8.258	14.603	20.836	25.082	25.448	23.533	21.860	21.227	21.070	20.283	20.577
.495 14 0	5.687	7.039	9.664	12.931	16.402	18.626	19.631	19.694	19.271	18.898	18.177	19.475	20.795
.564 18 0	7.690	7.914	9.438	11.767	14.503	16.742	18.148	18.606	18.763	18.751	18.463	18.497	19.080
.685 54 0	10.217	10.526	11.343	12.510	14.026	15.393	16.516	17.150	17.372	17.502	17.782	18.596	18.844
.824 58 0	11.867	12.090	12.699	13.300	14.045	14.887	15.697	16.189	16.432	16.729	17.117	17.622	17.650
.940 94 0	12.774	13.016	13.432	13.649	13.979	14.424	14.992	15.385	15.496	15.997	16.731	16.924	16.548
1.027 94 0	12.895	12.660	13.008	13.314	13.785	14.306	14.532	14.929	15.680	16.298	16.447	16.229	15.669
1.161 58 0	13.160	13.173	13.251	13.410	13.851	14.343	14.419	14.657	15.372	15.607	15.769	15.693	14.955
1.283 54 0	13.105	13.126	13.347	13.478	13.794	14.331	14.480	14.509	14.963	15.508	15.562	15.309	15.099
1.432 18 0	13.575	13.588	13.995	14.130	14.007	14.096	14.532	14.876	15.118	15.458	15.426	15.274	14.848

LOCAL FLOW FIELD DATA

MACH = 1.961 RE = 9.79x10 FT ALPHA = 14.530 X/D = 4.100 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395	10 0 13.613	7.872	16.967	39.294	47.765	30.729	17.213	18.203	22.280	23.054	23.630	24.385	26.745
.438	6 0 14.147	12.933	9.934	13.377	25.860	35.815	34.701	31.265	29.822	29.184	29.262	29.333	28.960
.495	10 0 2.767	4.608	16.825	29.303	33.201	35.415	32.951	32.067	30.707	29.318	25.989	20.101	17.907
.564	22 0 4.351	5.483	8.791	17.857	25.109	26.455	26.423	25.098	21.892	19.341	18.707	18.327	17.847
.685	50 0 8.525	9.183	10.725	12.951	15.007	16.554	17.811	18.280	18.159	17.946	18.095	17.775	17.590
.824	62 0 10.920	11.319	12.096	13.107	14.329	15.453	16.350	16.742	16.947	17.057	17.297	16.993	17.025
.940	90 0 12.050	12.339	12.984	13.451	14.144	14.807	15.403	15.765	15.887	15.765	16.294	16.930	17.019
1.027	90 0 12.588	12.493	12.824	13.162	13.957	14.704	15.004	15.499	15.834	16.151	16.393	16.338	16.227
1.161	62 0 12.775	12.747	13.065	13.315	13.913	14.481	14.605	14.841	15.432	15.580	15.711	16.010	15.566
1.283	50 0 13.047	13.012	13.261	13.381	13.648	14.280	14.527	14.530	14.878	15.352	15.590	15.754	15.222
1.432	22 0 13.539	13.561	13.895	14.120	14.261	14.513	14.911	15.138	15.315	15.529	15.785	15.810	15.396

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LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.81X10 FT ALPHA = 14.530 X/D = 4.400 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564	26 0 16.094	13.320	8.348	16.987	38.661	30.895	24.382	25.902	28.145	29.381	29.553	30.046	29.685
.685	46 0 16.705	18.609	20.381	25.052	28.293	29.622	29.388	28.665	28.622	28.532	28.234	27.882	27.393
.824	66 0 25.066	26.870	24.802	24.300	26.260	27.532	28.055	27.758	31.451	32.914	27.700	25.056	23.441
.940	86 0 11.998	12.254	17.358	21.885	23.406	21.183	17.475	16.221	16.212	16.196	16.684	16.608	16.503
1.027	86 0 12.201	12.084	12.484	12.899	13.698	14.526	15.045	15.643	15.966	16.195	16.274	15.997	15.767
1.161	66 0 12.623	12.662	13.031	13.372	14.048	14.634	14.798	14.983	15.507	15.713	15.557	15.571	15.866
1.283	46 0 12.922	12.891	13.259	13.418	13.739	14.309	14.487	14.631	15.071	15.186	15.370	16.054	15.375
1.432	26 0 13.445	13.421	13.901	14.197	14.288	14.536	15.072	15.286	15.445	15.586	15.678	15.995	15.598

LOCAL FLOW FIELD DATA

MACH = 1.956 RE = 9.81x10⁶ FT ALPHA = 14.530 X/D = 4.800 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564	30 0 3.694	4.825	9.192	15.931	17.843	6.647	4.695	12.176	16.136	17.275	18.000	19.064	19.431
.685	42 0 .338	1.052	4.225	10.287	6.732	16.812	14.599	14.814	15.047	15.261	15.944	16.805	17.102
.824	70 0 12.269	11.778	10.979	13.736	19.147	19.708	19.390	19.236	19.337	19.541	19.742	19.806	19.463
.940	82 0 17.858	17.552	17.584	17.744	19.620	21.414	21.912	21.960	22.065	21.838	21.733	21.473	20.907
1.027	82 0 19.594	19.885	18.865	18.754	20.187	21.568	22.142	22.442	22.426	22.333	22.154	21.593	20.986
1.161	70 0 21.541	21.659	20.612	20.784	21.620	22.618	23.165	23.226	23.236	23.087	22.574	22.076	21.112
1.283	42 0 22.076	22.463	21.804	21.987	22.453	23.031	23.538	23.805	23.826	26.347	29.201	22.135	16.993
1.432	30 0 25.887	26.255	24.546	22.857	23.953	26.987	27.551	20.354	15.353	15.633	15.621	15.776	16.167

LOCAL FLOW FIELD DATA

MACH = 1.956 RE = 9.78X10 FT ALPHA = 14.530 X/D = 5.500 TEST NO. = 35

LOCAL ANGLE OF ATTACK		-- (ALPHA) -- DEG.												
THETA		180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.														
.364	34 0	1.772	1.945	2.315	2.050	4.422	9.400	19.888	22.911	24.312	25.568	26.128	26.269	26.265
.633	98 0	.184	1.812	5.960	5.957	7.571	15.991	18.945	20.255	21.717	22.530	22.588	23.306	24.418
.685	38 0	4.364	5.531	8.974	10.288	10.687	14.448	17.168	19.778	20.985	21.006	20.831	21.488	22.423
.765	102 0	2.620	6.052	7.962	16.273	19.048	16.439	17.878	19.549	20.262	20.531	20.449	20.787	21.968
.824	74 0	2.865	7.842	8.161	19.131	19.600	16.943	17.876	19.221	19.917	19.968	19.661	20.131	20.385
.904	106 0	1.758	5.428	15.402	21.388	19.675	17.323	17.718	18.698	19.037	18.865	18.656	19.606	20.032
.940	78 0	.123	4.932	14.104	19.577	18.605	17.075	17.206	17.965	18.460	18.440	18.200	18.878	19.146
.999	110 0	4.775	6.630	13.064	18.005	18.116	16.829	16.915	17.641	18.129	18.031	17.935	18.806	19.033
1.027	78 0	4.877	6.261	11.732	15.793	16.981	16.386	16.582	17.020	17.906	17.875	17.724	17.740	18.289
1.161	74 0	8.284	9.184	12.015	14.360	15.452	15.514	15.667	16.158	17.129	16.897	16.930	17.350	16.236
1.283	38 0	7.819	9.990	11.866	12.505	13.980	14.833	15.188	15.813	16.894	16.559	16.845	17.172	15.850
1.432	34 0	9.301	9.131	10.222	12.101	13.472	14.375	15.201	15.745	16.418	16.512	16.692	16.357	16.151
1.538	98 0	6.847	7.796	9.955	11.791	13.089	13.784	14.603	15.441	15.886	15.945	15.738	15.358	15.296
1.680	102 0	7.552	8.311	10.082	11.595	12.837	13.594	14.355	15.011	15.386	15.160	15.138	15.190	14.692
1.798	106 0	8.874	9.177	10.163	11.480	12.449	13.137	13.478	14.141	14.730	14.758	14.895	14.944	14.762
1.923	110 0	9.709	9.891	10.549	11.305	11.974	12.755	13.480	14.249	14.941	15.068	15.153	15.074	15.000

LOCAL FLOW FIELD DATA

MACH = 1.963 RE = 9.80x10⁶ FT ALPHA = 14.530 X/D = 3.500 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

		THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D	RUN NO.														
.315	2 1	180.0	-160.0	-127.6	-93.1	-59.1	-24.0	-9.2	-3.2	46.9	79.0	75.1	63.4	62.7	
.395	14 0	180.0	137.7	133.5	114.5	91.1	83.2	76.2	67.0	66.0	69.7	74.8	80.7	89.6	
.438	2 1	180.0	90.6	90.3	91.3	86.3	74.6	62.6	60.0	63.8	68.2	72.5	77.0	83.9	
.495	14 0	.0	34.3	52.0	59.5	61.0	60.5	60.0	61.0	63.9	68.1	72.5	80.8	87.0	
.564	18 0	.0	17.7	37.2	46.9	53.4	56.6	59.0	61.0	64.1	67.9	73.2	81.3	88.9	
.685	54 0	.0	13.7	26.3	35.8	43.6	49.5	54.8	59.6	64.0	69.0	75.2	84.2	90.8	
.824	58 0	.0	9.9	21.0	30.9	38.2	43.9	50.4	56.5	62.0	67.6	73.5	83.1	91.1	
.940	94 0	.0	9.9	18.8	27.6	35.2	41.8	48.5	55.1	61.4	69.3	77.9	84.0	89.1	
1.027	94 0	.0	7.8	18.2	27.1	36.5	44.6	51.6	58.5	66.4	74.1	79.5	84.6	90.7	
1.161	58 0	.0	7.5	17.1	25.0	33.7	42.3	49.7	57.3	65.6	72.2	78.0	83.2	90.5	
1.283	54 0	.0	8.2	17.9	25.1	33.6	42.3	50.4	59.0	67.5	73.1	78.8	84.1	89.9	
1.432	18 0	.0	6.6	16.4	23.4	33.5	42.6	50.4	57.5	64.6	71.6	77.5	83.4	88.6	

LOCAL FLOW FIELD DATA

MACH = 1.961 RE = 9.79X10⁶ FT ALPHA = 14.530 X/D = 4.100 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 10 0	.0	-9.5	-60.7	-24.4	-4.7	.1	23.0	52.9	69.7	71.5	61.5	59.6	55.4
.438 6 0	.0	31.0	63.6	57.0	31.8	15.0	21.4	37.6	41.1	40.3	38.9	41.1	47.0
.495 10 0	.0	53.6	66.3	66.8	58.4	44.0	31.2	30.1	33.5	36.2	44.3	64.0	78.7
.564 22 0	.0	35.0	56.3	54.6	49.5	44.5	44.3	45.1	50.4	62.3	70.8	76.9	82.9
.685 50 0	.0	20.6	34.3	43.7	50.5	53.7	56.2	59.1	62.6	67.1	72.4	78.2	85.8
.824 62 0	.0	12.7	24.7	34.0	41.1	46.0	51.0	55.9	60.8	65.8	71.4	78.1	88.0
.940 90 0	.0	9.7	20.3	30.3	38.1	44.0	49.6	55.2	61.2	66.4	73.0	82.7	91.1
1.027 90 0	.0	9.3	19.3	29.0	38.5	45.7	51.8	58.4	64.6	70.6	76.0	83.2	92.2
1.161 62 0	.0	7.4	18.0	26.1	34.5	42.2	49.1	55.7	62.0	69.1	77.0	83.9	90.6
1.283 50 0	.0	7.1	17.7	25.2	34.0	42.9	49.9	56.9	65.1	72.1	79.5	86.5	92.1
1.432 22 0	.0	5.5	15.9	22.9	31.9	40.6	47.9	53.9	60.8	69.1	76.8	82.8	88.1

LOCAL FLOW FIELD DATA

*6 -1

MACH = 1.959 RE = 9.81X10 FT ALPHA = 14.530 X/D = 4.400 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 26 0	.0	-.5	3.1	12.5	13.9	22.0	30.1	44.2	41.3	40.5	44.1	46.3	47.4
.685 46 0	.0	12.7	27.9	38.0	36.7	30.3	28.8	31.0	35.6	40.0	43.0	44.9	45.5
.824 66 0	.0	11.7	20.1	27.8	29.5	29.2	30.6	32.6	40.0	43.7	46.6	53.1	58.6
.940 86 0	.0	10.1	21.0	24.3	24.9	30.2	43.0	54.7	61.0	65.4	71.4	78.6	87.6
1.027 86 0	.0	9.9	20.9	31.5	40.6	47.2	53.0	59.1	64.9	70.9	76.0	82.3	90.4
1.161 66 0	.0	8.5	19.2	27.2	35.2	42.7	49.1	55.6	61.8	67.9	74.3	81.1	90.0
1.283 46 0	.0	7.3	18.1	25.2	33.9	43.2	50.5	57.1	64.4	70.6	77.8	86.2	92.9
1.432 26 0	.0	5.2	15.9	22.8	31.8	40.3	47.2	53.2	59.4	66.5	74.6	82.8	86.9

LOCAL FLOW FIELD DATA

MACH = 1.956 RE = 9.81X10⁴ FT ALPHA = 14.530 X/D = 4.800 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.964 30 0	-180.0	-143.3	-118.4	-91.3	-66.6	-76.7	101.1	79.2	78.8	61.3	63.1	84.1	85.0
.685 42 0	180.0	-130.1	-137.2	-136.0	26.9	30.1	46.5	67.7	74.6	77.0	78.3	61.2	84.3
.624 70 0	.0	7.1	21.6	44.1	49.4	44.4	44.7	46.3	47.5	50.0	54.7	58.9	61.4
.940 82 0	.0	5.6	13.1	26.1	35.1	38.2	36.9	37.0	38.8	41.4	45.9	49.5	51.5
1.027 82 0	.0	9.0	16.7	26.6	34.2	36.9	37.3	40.2	42.7	45.8	49.6	52.5	54.6
1.161 70 0	.0	8.0	16.0	21.8	27.4	32.3	33.6	35.8	38.8	42.4	46.1	48.4	50.9
1.283 42 0	.0	7.6	15.7	21.1	26.6	30.4	31.9	34.0	38.3	39.8	39.6	50.6	63.1
1.432 30 0	.0	3.1	12.6	19.0	23.1	23.6	26.4	41.3	59.8	66.0	72.4	81.4	89.3

LOCAL FLOW FIELD DATA

MACH = 1.956 RE = 9.78X10⁴ FT ALPHA = 14.530 X/D = 6.500 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 34 0 -180.0	-129.0	-43.9	50.0	134.4	80.1	84.6	83.4	75.9	75.7	79.5	79.4	81.0	
.633 98 0 -180.0	-97.9	-69.4	-35.5	57.7	73.0	69.2	72.9	79.5	83.1	85.1	86.3	87.7	
.685 38 0 180.0	-133.9	-89.2	-33.4	28.6	57.1	63.6	71.2	77.3	81.0	83.6	85.8	87.8	
.765 102 0 180.0	-168.5	-105.3	2.7	29.6	50.0	63.3	71.4	75.6	78.7	81.2	83.6	86.1	
.824 74 0 -180.0	170.4	114.0	38.7	37.5	48.1	60.2	67.4	71.7	75.0	78.3	83.0	87.4	
.904 106 0 .0	92.8	78.1	54.8	45.7	50.7	61.6	67.7	71.4	74.4	77.1	82.4	87.0	
.940 78 0 -180.0	96.3	74.5	55.3	47.8	51.8	60.4	65.5	69.2	72.1	75.5	82.8	88.8	
.999 110 0 .0	57.7	66.9	58.0	51.5	54.6	63.0	67.9	71.3	74.3	77.3	83.0	87.6	
1.027 78 0 .0	52.1	64.1	53.1	52.5	58.2	64.5	68.3	72.3	76.4	79.8	84.5	90.2	
1.161 74 0 .0	30.9	39.3	43.6	53.1	57.6	59.7	63.0	67.7	70.7	75.0	82.0	86.5	
1.283 38 0 .0	19.5	34.7	55.6	56.1	57.2	59.1	62.7	67.9	71.7	78.5	83.9	88.1	
1.432 34 0 .0	17.2	38.5	47.3	50.6	52.7	55.6	59.9	64.7	69.8	78.1	81.0	85.0	
1.538 98 0 .0	24.3	36.8	42.8	47.2	50.3	55.1	60.1	66.8	75.2	78.0	82.5	87.6	
1.680 102 0 .0	16.3	29.4	37.4	42.4	46.4	50.8	60.1	70.7	72.7	77.1	83.2	90.7	
1.798 106 0 .0	10.7	24.2	32.2	37.9	43.9	52.7	64.6	67.8	70.8	75.0	79.0	83.8	
1.923 110 0 .0	10.9	22.8	31.3	38.7	49.0	57.6	62.8	66.3	70.0	72.8	76.3	80.5	

LOCAL FLOW FIELD DATA

*6 -1

MACH = 1.963 RE = 9.60X10 FT ALPHA = 14.530 X/D = 3.500 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 2 1	-.046	-.038	-.052	-.108	-.133	-.077	-.003	.028	.073	.059	-.026	.055	.102
.395 14 0	-.034	-.017	-.060	-.105	-.129	-.135	-.132	-.106	-.075	-.056	-.037	-.032	-.104
.438 2 1	.005	.003	-.015	-.063	-.117	-.139	-.115	-.084	-.065	-.059	-.054	-.042	-.061
.495 14 0	.019	.016	.007	-.015	-.035	-.039	-.038	-.031	-.027	-.030	-.022	-.053	-.087
.564 18 0	.007	.012	.006	-.010	-.026	-.035	-.041	-.039	-.037	-.037	-.035	-.050	-.077
.685 54 0	.022	.024	.017	.006	-.001	-.002	-.012	-.018	-.018	-.018	-.021	-.046	-.057
.824 58 0	.024	.025	.020	.012	.006	-.003	-.010	-.014	-.018	-.019	-.015	-.031	-.036
.940 94 0	.017	.017	.020	.014	.000	-.007	-.013	-.020	-.026	-.033	-.040	-.044	-.040
1.027 94 0	-.010	-.002	-.001	.003	.002	.000	-.003	-.009	-.022	-.034	-.038	-.034	-.012
1.161 58 0	-.002	.001	.003	.005	-.000	-.001	-.004	-.016	-.033	-.032	-.031	-.027	-.012
1.283 54 0	.007	.007	-.001	.005	.008	.001	-.013	-.015	-.028	-.036	-.026	-.019	-.017
1.432 18 0	.002	.009	.009	.011	.002	-.006	-.012	-.016	-.020	-.026	-.019	-.007	-.021

LOCAL FLOW FIELD DATA

*8 -1

MACH = 1.961 RE = 9.79X10 FT ALPHA = 14.530 X/D = 4.100 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 10 0	.803	.745	.578	.472	.408	.061	.099	.094	.057	.038	.079	.169	.319
.438 6 0	.718	.680	.288	.166	.129	.176	.197	.177	.126	.178	.322	.486	.576
.495 10 0	.020	.018	.212	.272	.196	.228	.294	.329	.316	.381	.309	.099	-.000
.564 22 0	.010	.006	-.009	.099	.207	.228	.193	.162	.085	-.002	-.030	-.031	-.024
.685 50 0	.029	.025	.016	.005	-.006	-.016	-.026	-.027	-.022	-.019	-.017	-.008	-.011
.824 62 0	.027	.025	.020	.012	.006	.002	-.008	-.012	-.012	-.009	.000	.003	-.018
.940 90 0	.019	.020	.020	.011	.001	-.010	-.019	-.021	-.026	-.028	-.022	-.032	-.041
1.027 90 0	-.006	-.000	.001	.002	.002	.004	-.004	-.012	-.016	-.014	-.014	-.025	-.042
1.161 62 0	.005	.005	.004	.004	.002	.000	-.002	-.002	-.003	-.009	-.019	-.030	-.010
1.283 50 0	.008	.008	.003	.010	.013	.006	-.004	-.000	-.011	-.023	-.022	-.029	-.025
1.432 22 0	.004	.013	.011	.013	.010	.006	.001	.000	-.006	-.017	-.025	-.019	-.031

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.81x10 FT ALPHA = 14.530 X/D = 4.400 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.584 26 0	.318	.334	.235	.160	.326	.284	.216	.206	.260	.299	.313	.331	.352
.885 46 0	.341	.347	.303	.222	.200	.248	.313	.340	.356	.369	.390	.430	.467
.824 66 0	.457	.528	.404	.290	.327	.371	.393	.368	.580	.736	.559	.416	.359
.940 86 0	.018	.017	.126	.224	.267	.175	.037	-.020	-.027	-.023	-.017	-.010	-.022
1.027 86 0	-.004	.003	.003	.003	.001	.002	-.003	-.011	-.013	-.012	-.011	-.010	-.016
1.161 66 0	.006	.008	.005	.005	.005	.001	-.002	-.000	.001	-.001	-.002	-.012	-.011
1.283 46 0	.004	.006	.001	.010	.010	-.001	-.005	-.004	-.012	-.017	-.015	-.032	-.032
1.432 26 0	-.000	.010	.010	.013	.006	.001	.003	.004	-.001	-.008	-.018	-.024	-.028

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.956 RE = 9.81X10 FT ALPHA = 14.530 X/D = 4.800 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 30 0	-.164	-.184	-.226	-.200	-.133	-.054	-.063	-.109	-.160	-.153	-.159	-.150	-.129
.685 42 0	-.094	-.122	-.166	-.159	-.151	-.075	-.065	-.128	-.163	-.143	-.130	-.124	-.114
.824 70 0	.064	.055	.035	.008	-.029	-.034	-.029	-.006	.027	.047	.058	.066	.083
.940 82 0	.155	.144	.141	.093	.059	.050	.079	.112	.136	.158	.176	.183	.200
1.027 82 0	.204	.195	.167	.134	.122	.129	.163	.182	.211	.228	.231	.242	.268
1.161 70 0	.258	.240	.192	.180	.179	.187	.230	.264	.281	.286	.293	.308	.329
1.283 42 0	.270	.251	.220	.223	.221	.227	.265	.305	.309	.434	.581	.332	.034
1.432 30 0	.313	.331	.277	.226	.250	.365	.384	.163	-.005	-.001	.001	-.011	-.043

LOCAL FLOW FIELD DATA

*6 -1

MACH = 1.956 RE = 9.78X10 FT ALPHA = 14.530 X/D = 6.500 TEST NO. = 33

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 34 0	.009	.015	.037	.026	-.009	-.016	-.093	-.151	-.102	-.053	-.053	-.036	-.036
.633 98 0	-.048	-.040	-.038	-.018	-.010	-.037	-.090	-.109	-.127	-.133	-.122	-.120	-.128
.685 38 0	-.044	-.043	-.045	-.036	-.027	-.055	-.078	-.112	-.128	-.120	-.106	-.106	-.115
.765 102 0	-.049	-.047	-.080	-.061	-.046	-.053	-.084	-.113	-.115	-.103	-.085	-.070	-.074
.824 74 0	-.042	-.034	-.071	-.073	-.062	-.063	-.088	-.110	-.106	-.089	-.067	-.063	-.063
.904 106 0	-.023	-.015	-.050	-.053	-.054	-.063	-.085	-.101	-.099	-.082	-.058	-.061	-.062
.940 78 0	-.014	-.006	-.034	-.049	-.064	-.075	-.092	-.104	-.101	-.083	-.058	-.060	-.062
.999 110 0	.011	-.002	-.025	-.047	-.064	-.064	-.075	-.083	-.083	-.068	-.043	-.053	-.057
1.027 78 0	-.000	-.030	-.044	-.043	-.067	-.071	-.084	-.085	-.085	-.067	-.050	-.046	-.061
1.161 74 0	.001	-.012	-.008	-.026	-.076	-.073	-.058	-.057	-.068	-.044	-.036	-.047	-.020
1.283 38 0	-.040	-.010	-.014	-.087	-.079	-.067	-.050	-.050	-.060	-.042	-.044	-.044	-.014
1.432 34 0	-.063	-.051	-.078	-.081	-.072	-.053	-.039	-.033	-.037	-.035	-.045	-.022	-.027
1.538 98 0	-.116	-.094	-.088	-.078	-.067	-.052	-.040	-.037	-.038	-.056	-.042	-.023	-.027
1.680 102 0	-.118	-.103	-.091	-.074	-.063	-.047	-.032	-.050	-.079	-.061	-.047	-.027	-.010
1.798 106 0	-.106	-.097	-.087	-.073	-.066	-.051	-.054	-.082	-.069	-.052	-.030	-.009	.008
1.923 110 0	-.089	-.080	-.072	-.063	-.061	-.058	-.059	-.052	-.040	-.015	.003	.022	.032

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.963 RE = 9.80x10 FT ALPHA = 14.530 X/D = 3.500 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 2 1	.989	.949	.812	.544	.419	.439	.532	.512	.456	.619	.880	.857	.749
.395 14 0	.987	.989	.878	.585	.493	.625	.830	.986	.995	1.003	1.003	.954	.823
.438 2 1	.983	.976	.974	.959	.855	.884	.987	1.016	1.004	.995	.996	.968	.950
.495 14 0	.981	.982	.975	.978	.975	.974	.979	.984	.982	.982	.976	.938	.955
.564 18 0	1.005	.990	.981	.986	.987	.991	.996	.999	.998	.998	.996	.961	.971
.685 54 0	1.000	.988	.981	.985	.984	.980	.981	.983	.981	.977	.951	.957	.975
.824 58 0	1.007	1.006	.999	.998	.997	.991	.986	.987	.983	.971	.949	.957	.975
.940 94 0	1.001	1.006	1.006	1.006	1.014	1.010	1.010	1.018	1.016	1.000	1.003	1.010	1.008
1.027 94 0	1.020	1.010	1.012	1.011	1.011	1.013	1.007	1.001	1.000	1.003	1.006	1.005	1.002
1.161 58 0	1.011	1.004	1.008	1.010	1.016	1.017	1.013	1.008	1.000	1.000	.998	1.002	1.004
1.283 54 0	1.013	1.005	1.012	1.013	1.012	1.013	1.012	1.001	1.004	1.005	1.007	1.005	1.010
1.432 18 0	.999	.995	.998	1.000	1.001	.998	1.001	1.003	.999	.998	.999	1.001	1.012

LOCAL FLOW FIELD DATA

*6 -1

MACH = 1.961 RE = 9.79X10 FT ALPHA = 14.530 X/D = 4.100 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 10 0	.694	.658	.524	.416	.554	.585	.565	.645	.621	.858	1.094	1.044	.964
.438 6 0	.716	.701	.696	.495	.408	.533	.596	.822	1.052	1.072	.987	.917	.866
.495 10 0	.954	.939	.817	.800	.834	.865	.915	.930	.943	.842	.782	.860	.918
.564 22 0	.979	.982	.986	.881	.783	.762	.792	.824	.875	.953	.982	.986	.973
.685 50 0	.981	.976	.974	.983	.986	.987	1.001	1.010	1.007	1.002	.999	1.001	.974
.824 62 0	1.000	.993	.988	.994	.993	.983	.988	.989	.985	.980	.972	.960	.963
.940 90 0	1.003	1.006	.999	1.003	1.008	1.008	1.013	1.019	1.020	1.017	1.005	.995	1.000
1.027 90 0	1.019	1.008	1.007	1.007	1.005	1.009	1.009	1.006	1.005	1.004	.997	.992	1.013
1.161 62 0	1.009	1.007	1.011	1.011	1.013	1.017	1.018	1.012	1.002	1.003	.996	.995	1.005
1.283 50 0	1.012	1.006	1.010	1.009	1.008	1.012	1.016	1.006	1.004	1.005	1.001	1.002	1.013
1.432 22 0	.997	1.000	1.000	1.001	.999	1.000	1.008	1.007	1.004	.999	1.004	1.003	1.011

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.81x10 FT ALPHA = 14.530 X/D = 4.400 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 26 0	.863	.940	.697	.396	.494	.617	.485	.540	.880	1.036	1.027	.973	.929
.685 46 0	.911	.952	.977	.984	.989	1.000	1.006	1.002	.973	.952	.947	.943	.932
.824 66 0	.890	.869	.925	.977	.975	.968	.963	.964	.887	.811	.776	.778	.788
.940 86 0	1.012	1.011	.918	.851	.826	.857	.948	1.011	1.020	1.013	.999	1.000	1.002
1.027 86 0	1.016	1.005	1.003	1.008	1.009	1.011	1.008	1.007	1.009	1.007	1.009	1.007	.988
1.161 66 0	1.010	1.007	1.011	1.010	1.009	1.015	1.016	1.008	1.002	1.006	.998	.994	.989
1.283 46 0	1.011	1.002	1.008	1.009	1.007	1.009	1.016	1.008	1.006	1.009	1.001	.990	1.017
1.432 26 0	.999	.997	.999	.998	.998	1.002	1.005	1.002	1.002	.996	.990	1.001	1.003

LOCAL FLOW FIELD DATA

+8 -1

MACH = 1.956 RE = 9.61X10 FT ALPHA = 14.530 X/D = 4.000 TEST NO. = 55

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.964 30 0	.803	.827	.906	.628	.533	.597	.497	.733	.882	.848	.858	.853	.843
.685 42 0	.943	1.046	1.108	.636	.361	.556	.654	.939	1.116	1.076	.990	.982	1.009
.624 70 0	.972	1.027	1.036	.862	.837	1.006	1.077	1.070	1.034	1.007	.995	.988	.977
.940 82 0	.989	1.026	1.031	1.026	1.026	1.057	1.066	1.051	1.041	1.030	.991	.991	.995
1.027 82 0	.991	1.005	1.014	1.012	1.017	1.022	1.017	1.016	1.009	.998	.990	.983	.955
1.161 70 0	.991	1.001	1.026	1.027	1.020	1.014	1.006	1.006	1.003	.996	.989	.982	.969
1.283 42 0	.990	1.001	1.017	1.014	1.002	1.009	1.002	.987	.982	.917	.784	.767	.643
1.432 30 0	.902	.886	.921	.981	.983	.886	.800	.878	1.004	1.002	.993	.987	1.009

LOCAL FLOW FIELD DATA

MACH = 1.956 RE = 9.78X10⁴ FT ALPHA = 14.530 X/D = 6.500 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 34 0	.617	.647	.558	.573	.638	.425	.498	.965	.968	.779	.780	.724	.705
.633 98 0	.859	.885	.895	.779	.779	.808	.861	.875	.887	.911	.922	.886	.884
.685 38 0	.867	.868	.708	.683	.814	.893	.877	.876	.898	.915	.929	.903	.899
.765 102 0	.884	.793	.475	.527	.774	.893	.881	.898	.918	.921	.929	.898	.888
.824 74 0	.910	.775	.442	.495	.833	.912	.881	.894	.898	.908	.910	.890	.890
.904 106 0	.949	.811	.624	.671	.871	.928	.899	.900	.916	.926	.926	.919	.921
.940 78 0	.927	.824	.703	.770	.941	.944	.936	.943	.937	.936	.929	.925	.930
.999 110 0	.935	.869	.842	.881	.940	.925	.923	.924	.920	.923	.914	.925	.942
1.027 78 0	.937	.960	.897	.895	.926	.941	.946	.938	.926	.941	.939	.912	.957
1.161 74 0	.877	.997	.961	.921	.980	.956	.953	.945	.950	.943	.937	.928	.957
1.283 38 0	.936	.940	.880	.975	.978	.970	.971	.962	.956	.933	.924	.962	.959
1.432 34 0	.911	.924	.963	.968	.972	.976	.973	.961	.954	.943	.958	.961	.976
1.538 98 0	.965	.967	.980	.976	.981	.986	.984	.970	.951	.959	.968	.985	.974
1.680 102 0	.983	.983	.979	.977	.979	.977	.971	.958	.973	.970	.969	.979	1.004
1.798 106 0	.983	.989	.987	.979	.983	.961	.953	.990	.993	.995	.994	1.002	1.013
1.923 110 0	.984	.988	.986	.986	.987	.981	.980	.983	.988	.989	.987	.990	1.002

LOCAL FLOW FIELD DATA

MACH = 1.963 RE = 9.80x10⁶ FT ALPHA = 14.530 X/D = 3.500 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 2 1	-.093	-.102	-.100	-.012	.126	.247	.289	.216	.139	.073	.107	.172	.181
.395 14 0	-.068	-.083	-.141	-.115	-.007	.050	.106	.174	.170	.133	.095	.057	.003
.438 2 1	-.006	-.001	-.001	-.006	.024	.119	.210	.209	.170	.139	.111	.079	.038
.495 14 0	.098	.100	.102	.114	.139	.160	.171	.166	.147	.122	.095	.054	.019
.564 18 0	.133	.130	.130	.140	.151	.161	.164	.158	.143	.123	.093	.049	.006
.685 54 0	.175	.175	.174	.175	.175	.172	.164	.150	.131	.108	.078	.033	-.005
.824 58 0	.203	.204	.203	.196	.190	.185	.173	.155	.134	.110	.083	.037	-.006
.940 94 0	.219	.220	.218	.208	.198	.187	.173	.154	.130	.099	.061	.031	.004
1.027 94 0	.225	.218	.214	.203	.192	.176	.156	.135	.109	.078	.053	.027	-.003
1.161 58 0	.228	.226	.219	.210	.200	.184	.162	.138	.111	.084	.057	.032	-.002
1.283 54 0	.226	.224	.220	.211	.198	.184	.161	.130	.100	.079	.053	.027	.000
1.432 18 0	.234	.232	.231	.223	.202	.180	.161	.139	.113	.085	.058	.030	.006

LOCAL FLOW FIELD DATA

MACH = 1.961 RE = 9.79x10 FT ALPHA = 14.530 X/D = 4.100 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 10 0	.128	.073	.072	.250	.462	.433	.222	.161	.114	.118	.187	.195	.219
.438 6 0	.146	.116	.015	.092	.255	.424	.410	.359	.357	.348	.327	.288	.240
.495 10 0	.047	.047	.099	.159	.249	.360	.396	.387	.362	.313	.251	.138	.059
.564 22 0	.075	.078	.085	.164	.234	.264	.273	.264	.222	.153	.107	.072	.038
.685 50 0	.146	.147	.152	.161	.165	.170	.172	.164	.145	.121	.095	.063	.022
.624 62 0	.187	.189	.188	.187	.186	.184	.177	.162	.143	.120	.094	.060	.010
.940 90 0	.207	.209	.209	.200	.193	.185	.174	.157	.134	.110	.083	.037	-.006
1.027 90 0	.219	.214	.210	.199	.189	.177	.161	.141	.118	.093	.069	.033	-.011
1.161 62 0	.221	.219	.215	.207	.198	.186	.166	.145	.125	.096	.062	.030	-.003
1.283 90 0	.225	.223	.219	.209	.195	.181	.162	.137	.109	.083	.049	.017	-.010
1.432 22 0	.234	.232	.230	.223	.208	.190	.173	.154	.130	.096	.063	.034	.009

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.81X10⁶ FT ALPHA = 14.530 X/D = 4.400 TEST NO. = 55

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 26 0	.229	.194	.116	.206	.382	.351	.247	.227	.303	.329	.310	.295	.279
.685 46 0	.267	.262	.269	.300	.345	.380	.373	.353	.329	.305	.285	.268	.255
.824 66 0	.331	.330	.319	.317	.329	.338	.335	.328	.293	.253	.222	.192	.162
.940 86 0	.206	.208	.237	.293	.301	.276	.213	.163	.138	.118	.092	.057	.012
1.027 86 0	.212	.206	.202	.190	.180	.171	.157	.139	.118	.092	.068	.037	-.002
1.161 66 0	.218	.216	.213	.206	.198	.186	.168	.146	.126	.102	.073	.042	-.000
1.283 46 0	.224	.221	.218	.209	.196	.181	.160	.138	.113	.088	.056	.019	-.014
1.432 26 0	.232	.230	.230	.224	.209	.191	.177	.158	.136	.107	.072	.035	.015

LOCAL FLOW FIELD DATA

MACH = 1.956 RE = 9.81x10⁶ FT ALPHA = 14.530 X/D = 4.800 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 30 0	-.068	-.073	-.086	-.006	.117	.025	-.014	.040	.058	.048	.040	.036	.030
.685 42 0	-.006	-.013	-.060	-.131	.093	.232	.159	.103	.076	.065	.059	.047	.031
.824 70 0	.205	.198	.175	.165	.210	.245	.242	.231	.222	.210	.190	.169	.153
.940 82 0	.284	.282	.277	.263	.268	.283	.291	.286	.277	.261	.237	.218	.202
1.027 82 0	.304	.307	.287	.270	.270	.278	.279	.269	.255	.238	.219	.199	.181
1.161 70 0	.325	.327	.311	.305	.302	.299	.295	.284	.270	.254	.232	.216	.194
1.283 42 0	.331	.338	.324	.316	.308	.304	.300	.290	.274	.272	.259	.188	.117
1.432 30 0	.367	.366	.349	.329	.331	.338	.322	.234	.134	.110	.081	.041	.004

LOCAL FLOW FIELD DATA

MACH = 1.055 RE = 9.76X10 FT ALPHA = 14.530 X/D = 6.500 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 34 0	-.028	-.019	.023	.020	-.049	.023	.029	.048	.105	.105	.079	.078	.067
.633 98 0	-.003	-.004	.036	.081	.067	.080	.118	.105	.071	.049	.035	.027	.018
.685 38 0	-.076	-.067	.002	.141	.159	.137	.134	.113	.083	.059	.042	.028	.015
.765 102 0	-.046	-.101	-.033	.252	.277	.183	.141	.111	.090	.072	.055	.040	.026
.824 74 0	-.050	-.130	-.050	.229	.266	.198	.156	.132	.111	.091	.069	.043	.016
.904 106 0	.031	-.004	.051	.200	.236	.192	.149	.126	.108	.090	.073	.045	.019
.940 78 0	-.002	-.009	.062	.186	.219	.187	.152	.134	.117	.100	.080	.042	.007
.999 110 0	.082	.060	.087	.164	.198	.171	.135	.118	.103	.086	.068	.040	.014
1.027 78 0	.084	.068	.089	.164	.182	.153	.127	.112	.096	.074	.055	.029	-.001
1.161 74 0	.140	.138	.161	.179	.166	.148	.139	.129	.115	.097	.076	.042	.017
1.283 38 0	.137	.162	.166	.128	.140	.143	.138	.127	.112	.090	.058	.032	.009
1.432 34 0	.164	.153	.144	.147	.153	.154	.150	.138	.122	.099	.060	.044	.024
1.538 98 0	.126	.129	.145	.156	.159	.156	.147	.134	.109	.072	.057	.035	.011
1.660 102 0	.140	.146	.160	.163	.169	.165	.158	.132	.091	.080	.059	.031	-.003
1.798 106 0	.163	.165	.168	.174	.175	.167	.144	.109	.099	.086	.067	.050	.027
1.923 110 0	.176	.176	.175	.173	.167	.149	.128	.115	.106	.089	.077	.061	.042

LOCAL FLOW FIELD DATA

MACH = 1.963 RE = 9.80x10 FT ALPHA = 14.530 X/D = 3.500 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 2 1	.000	-.037	-.129	-.230	-.210	-.110	-.047	-.012	.149	.375	.402	.343	.351
.395 14 0	.000	.075	.148	.253	.358	.417	.432	.410	.383	.360	.348	.346	.424
.438 2 1	.000	.054	.144	.258	.369	.433	.405	.362	.346	.346	.352	.343	.358
.495 14 0	.000	.068	.131	.193	.250	.282	.295	.298	.299	.304	.299	.335	.368
.564 18 0	.000	.041	.098	.149	.203	.244	.272	.285	.295	.303	.308	.320	.339
.685 54 0	.000	.043	.086	.126	.167	.201	.233	.256	.270	.282	.296	.322	.331
.824 98 0	-.000	.036	.078	.117	.149	.178	.209	.234	.251	.267	.282	.303	.307
.940 94 0	-.000	.038	.074	.109	.139	.167	.195	.220	.238	.262	.287	.297	.291
1.027 94 0	-.000	.030	.070	.105	.142	.174	.197	.221	.250	.275	.284	.283	.272
1.161 98 0	.000	.030	.067	.098	.133	.167	.191	.215	.245	.260	.270	.272	.260
1.283 54 0	.000	.032	.071	.099	.132	.167	.194	.216	.242	.261	.267	.265	.263
1.432 18 0	.000	.027	.068	.096	.134	.165	.195	.218	.238	.256	.262	.263	.259

LOCAL FLOW FIELD DATA

*8 -1

MACH = 1.961 RE = 9.79x10 FT ALPHA = 14.530 X/D = 4.100 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 10 0	-.000	-.012	-.129	-.114	-.038	.001	.094	.213	.308	.353	.346	.332	.317
.438 6 0	-.000	.070	.133	.142	.158	.114	.161	.276	.311	.295	.264	.251	.258
.495 10 0	-.000	.063	.226	.371	.405	.348	.240	.224	.240	.229	.245	.284	.297
.564 22 0	.000	.054	.128	.231	.273	.259	.266	.265	.267	.291	.307	.310	.306
.685 30 0	.000	.055	.103	.154	.200	.231	.258	.273	.280	.287	.298	.300	.302
.624 62 0	.000	.043	.086	.126	.162	.191	.219	.240	.255	.268	.280	.283	.293
.940 90 0	.000	.036	.077	.117	.151	.179	.205	.226	.244	.253	.271	.293	.299
1.027 90 0	-.000	.035	.074	.111	.150	.182	.204	.229	.249	.264	.276	.283	.286
1.161 62 0	.000	.028	.070	.101	.136	.168	.192	.212	.235	.252	.266	.278	.270
1.283 30 0	.000	.028	.070	.098	.131	.168	.193	.210	.234	.255	.267	.275	.266
1.432 22 0	-.000	.022	.065	.095	.129	.162	.191	.211	.231	.252	.268	.273	.270

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.81X10 FT ALPHA = 14.530 X/D = 4.400 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 26 0	-.000	-.002	.006	.046	.094	.142	.143	.220	.266	.281	.300	.309	.303
.685 46 0	-.000	.059	.142	.234	.257	.223	.205	.212	.235	.256	.266	.267	.259
.824 66 0	.000	.069	.117	.167	.186	.189	.198	.210	.246	.241	.234	.255	.265
.940 86 0	.000	.057	.099	.132	.139	.161	.199	.231	.248	.257	.274	.282	.287
1.027 86 0	-.000	.036	.077	.116	.154	.184	.208	.233	.251	.265	.274	.275	.273
1.161 66 0	-.000	.032	.074	.105	.140	.172	.194	.214	.235	.251	.258	.267	.274
1.283 46 0	-.000	.028	.071	.099	.132	.170	.194	.213	.236	.250	.261	.280	.270
1.432 26 0	-.000	.021	.066	.095	.130	.162	.191	.211	.229	.247	.262	.277	.275

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.956 RE = 9.81X10 FT ALPHA = 14.530 X/D = 4.800 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 30 0	-.000	-.034	-.159	-.288	-.271	-.104	.072	.208	.293	.312	.328	.345	.346
.685 42 0	.000	-.015	-.056	-.126	.047	.135	.180	.251	.278	.280	.288	.305	.311
.824 70 0	.000	.025	.069	.160	.244	.240	.240	.242	.242	.251	.268	.280	.279
.940 82 0	.000	.028	.064	.129	.189	.223	.218	.216	.223	.230	.244	.255	.254
1.027 82 0	.000	.049	.086	.136	.184	.209	.213	.227	.235	.245	.257	.260	.255
1.161 70 0	.000	.046	.089	.122	.157	.189	.196	.205	.217	.231	.241	.243	.238
1.283 42 0	-.000	.045	.091	.122	.155	.179	.187	.196	.216	.227	.215	.229	.252
1.432 30 0	.000	.020	.078	.113	.142	.148	.160	.205	.230	.246	.256	.270	.285

LOCAL FLOW FIELD DATA

MACH = 1.956 RE = 9.78x10 FT ALPHA = 14.530 X/D = 6.500 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 34 0	-.000	-.024	-.024	.024	.050	.131	.309	.418	.419	.411	.425	.416	.421
.633 98 0	-.000	-.031	-.097	-.058	.106	.261	.311	.344	.383	.403	.404	.413	.435
.685 38 0	.000	-.069	-.149	-.093	.086	.211	.269	.333	.368	.372	.370	.380	.399
.765 102 0	.000	-.021	-.120	.012	.157	.218	.281	.331	.352	.359	.357	.359	.374
.824 74 0	-.000	.022	.112	.183	.204	.221	.273	.317	.336	.340	.336	.346	.353
.904 106 0	-.000	.091	.242	.284	.242	.235	.275	.308	.321	.321	.317	.338	.348
.940 78 0	-.000	.083	.223	.269	.242	.238	.267	.294	.309	.311	.308	.327	.334
.999 110 0	-.000	.095	.204	.263	.249	.241	.266	.289	.304	.305	.302	.324	.332
1.027 78 0	-.000	.087	.183	.218	.237	.246	.267	.281	.303	.306	.304	.305	.321
1.161 74 0	.000	.082	.131	.171	.221	.233	.238	.253	.280	.278	.283	.299	.280
1.283 38 0	-.000	.057	.115	.186	.208	.222	.229	.247	.276	.273	.286	.298	.273
1.432 34 0	-.000	.047	.114	.160	.186	.202	.220	.237	.258	.269	.285	.279	.280
1.538 98 0	-.000	.058	.108	.144	.172	.188	.210	.234	.254	.271	.270	.264	.266
1.680 102 0	-.000	.043	.090	.126	.134	.174	.194	.228	.260	.256	.259	.263	.255
1.798 106 0	-.000	.031	.075	.110	.137	.161	.189	.230	.244	.247	.252	.254	.253
1.923 110 0	-.000	.034	.073	.105	.134	.171	.202	.224	.240	.246	.249	.249	.251

LOCAL FLOW FIELD DATA

MACH = 1.963 RE = 9.80x10 FT ALPHA = 14.530 X/D = 3.500 TEST NO. = 35

(VC / VIN * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 2 1	.370	.434	.651	.919	.977	1.079	1.166	.862	.813	1.522	1.657	1.530	1.575
.395 14 0	.270	.445	.816	1.106	1.425	1.674	1.773	1.777	1.669	1.528	1.437	1.396	1.691
.438 2 1	.025	.214	.574	1.030	1.473	1.789	1.817	1.667	1.536	1.486	1.472	1.404	1.433
.495 14 0	.390	.483	.663	.895	1.140	1.293	1.360	1.361	1.329	1.306	1.252	1.351	1.471
.564 18 0	.532	.544	.649	.815	1.009	1.167	1.267	1.297	1.306	1.305	1.284	1.289	1.350
.685 54 0	.699	.718	.775	.858	.964	1.055	1.136	1.182	1.197	1.205	1.219	1.291	1.320
.824 58 0	.811	.826	.867	.911	.964	1.024	1.081	1.117	1.134	1.152	1.171	1.216	1.226
.940 94 0	.874	.891	.918	.935	.965	.998	1.040	1.072	1.082	1.117	1.171	1.189	1.160
1.027 94 0	.897	.876	.900	.918	.951	.987	1.003	1.032	1.089	1.139	1.152	1.134	1.083
1.161 58 0	.910	.909	.914	.924	.957	.991	.997	1.018	1.074	1.090	1.100	1.093	1.036
1.283 54 0	.903	.903	.922	.929	.949	.989	1.005	1.006	1.045	1.086	1.085	1.063	1.049
1.432 18 0	.934	.931	.959	.968	.964	.974	1.007	1.032	1.050	1.076	1.070	1.054	1.034

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.961 RE = 9.79X10 FT ALPHA = 14.530 X/D = 4.100 TEST NO. = 35

(VC / VINP * SIN ALPHAINP)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 10 0	.509	.296	.589	1.096	1.848	1.725	.960	1.063	1.308	1.483	1.567	1.536	1.536
.438 6 0	.581	.539	.532	.673	1.196	1.749	1.756	1.806	1.889	1.818	1.676	1.523	1.406
.495 10 0	.189	.314	.983	1.608	1.895	1.995	1.845	1.782	1.731	1.547	1.400	1.259	1.208
.564 22 0	.300	.378	.611	1.130	1.433	1.474	1.519	1.490	1.384	1.309	1.294	1.270	1.231
.685 50 0	.580	.625	.732	.888	1.032	1.142	1.235	1.270	1.257	1.240	1.248	1.222	1.205
.824 62 0	.745	.772	.825	.898	.982	1.058	1.123	1.153	1.166	1.170	1.179	1.154	1.169
.940 90 0	.825	.844	.887	.923	.975	1.025	1.072	1.098	1.109	1.101	1.131	1.178	1.191
1.027 90 0	.874	.864	.885	.908	.962	1.011	1.036	1.073	1.097	1.117	1.132	1.134	1.140
1.161 62 0	.881	.878	.901	.918	.959	1.000	1.009	1.024	1.063	1.076	1.089	1.115	1.076
1.283 90 0	.898	.895	.915	.919	.936	.982	1.005	1.001	1.030	1.068	1.083	1.099	1.062
1.432 22 0	.931	.929	.952	.966	.977	.996		1.042	1.057	1.076	1.099	1.097	1.077

LOCAL FLOW FIELD DATA

*6 -1

MACH = 1.959 RE = 9.81x10 FT ALPHA = 14.530 X/D = 4.400 TEST NO. = 35

(VC / VINP + SIN ALPHAINP)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.364 26 0	.912	.774	.464	.641	1.567	1.507	1.137	1.260	1.607	1.723	1.718	1.703	1.644
.685 46 0	1.063	1.070	1.212	1.516	1.716	1.757	1.699	1.639	1.611	1.587	1.554	1.506	1.451
.824 66 0	1.318	1.344	1.356	1.427	1.508	1.542	1.551	1.554	1.524	1.393	1.286	1.273	1.239
.940 86 0	.823	.641	1.097	1.281	1.322	1.274	1.162	1.127	1.132	1.127	1.154	1.145	1.145
1.027 86 0	.847	.834	.861	.889	.945	1.001	1.038	1.082	1.105	1.120	1.125	1.105	1.089
1.161 66 0	.870	.871	.898	.921	.967	1.009	1.022	1.032	1.065	1.081	1.070	1.075	1.094
1.283 46 0	.891	.887	.915	.922	.943	.987	1.003	1.010	1.044	1.055	1.065	1.118	1.077
1.432 26 0	.927	.920	.953	.971	.980	1.000	1.036	1.049	1.062	1.074	1.085	1.112	1.088

LOCAL FLOW FIELD DATA

MACH = 1.956 RE = 9.81x10⁴ FT ALPHA = 14.530 X/D = 4.800 TEST NO. = 35

(VC / VINF * SIN ALPHAINE)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 30 0	.273	.363	.719	1.149	1.178	.427	.291	.644	1.190	1.258	1.316	1.382	1.385
.685 42 0	.024	.079	.326	.726	.415	1.070	.959	1.081	1.149	1.146	1.173	1.229	1.248
.824 70 0	.816	.796	.751	.915	1.283	1.369	1.360	1.333	1.311	1.304	1.308	1.303	1.269
.940 82 0	1.133	1.129	1.135	1.168	1.307	1.436	1.450	1.428	1.416	1.386	1.356	1.336	1.294
1.027 82 0	1.213	1.240	1.195	1.206	1.303	1.384	1.397	1.403	1.381	1.362	1.347	1.305	1.246
1.161 70 0	1.296	1.317	1.291	1.308	1.356	1.409	1.411	1.394	1.383	1.369	1.334	1.295	1.224
1.283 42 0	1.320	1.357	1.343	1.351	1.375	1.407	1.410	1.395	1.392	1.410	1.342	1.179	1.110
1.432 30 0	1.462	1.460	1.424	1.387	1.435	1.472	1.431	1.239	1.060	1.075	1.071	1.087	1.136

LOCAL FLOW FIELD DATA

MACH = 1.956 RE = 9.78x10 FT ALPHA = 14.530 X/D = 6.500 TEST NO. = 35

(VC / VINP * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 34 0	.110	.122	.137	.123	.281	.528	1.239	1.678	1.722	1.689	1.724	1.688	1.699
.633 98 0	.013	.126	.414	.397	.502	1.088	1.324	1.432	1.551	1.619	1.615	1.651	1.734
.665 38 0	.302	.383	.595	.672	.720	1.003	1.199	1.402	1.506	1.503	1.482	1.520	1.591
.765 102 0	.185	.413	.494	1.004	1.270	1.136	1.252	1.394	1.449	1.458	1.439	1.441	1.493
.824 74 0	.200	.527	.491	1.171	1.336	1.181	1.255	1.367	1.413	1.404	1.367	1.389	1.406
.904 106 0	.123	.365	.988	1.383	1.347	1.211	1.246	1.326	1.351	1.328	1.297	1.360	1.390
.940 78 0	.008	.331	.921	1.305	1.301	1.206	1.225	1.287	1.318	1.303	1.267	1.313	1.333
.999 110 0	.326	.448	.883	1.234	1.268	1.177	1.190	1.245	1.278	1.261	1.235	1.303	1.325
1.027 78 0	.335	.438	.813	1.088	1.190	1.155	1.178	1.207	1.266	1.254	1.231	1.223	1.281
1.161 74 0	.560	.640	.827	.986	1.101	1.099	1.100	1.131	1.206	1.173	1.169	1.202	1.117
1.283 38 0	.547	.687	.805	.900	1.000	1.051	1.066	1.107	1.186	1.146	1.165	1.196	1.088
1.432 34 0	.655	.640	.731	.867	.959	1.012	1.061	1.092	1.139	1.141	1.163	1.127	1.119
1.538 98 0	.503	.565	.719	.845	.932	.973	1.023	1.076	1.103	1.119	1.098	1.062	1.061
1.680 102 0	.557	.607	.729	.829	.912	.956	.999	1.051	1.097	1.070	1.061	1.055	1.017
1.798 106 0	.649	.668	.735	.821	.887	.924	.947	1.015	1.049	1.042	1.039	1.033	1.014
1.923 110 0	.703	.713	.756	.805	.851	.904	.955	1.005	1.046	1.042	1.038	1.023	1.016

LOCAL FLOW FIELD DATA

MACH = 1.963 RE = 9.80x10 FT ALPHA = 14.530 X/D = 3.500 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 2 1	1.017	1.005	.975	.919	.878	.830	.813	.804	.736	.773	.898	.860	.794
.395 14 0	1.013	1.001	.987	.918	.875	.904	.945	.957	.950	.956	.954	.945	.933
.438 2 1	.994	.992	.992	.992	.971	.959	.958	.961	.961	.960	.959	.953	.958
.495 14 0	.982	.981	.978	.978	.972	.962	.956	.954	.954	.957	.956	.958	.972
.564 18 0	.989	.982	.980	.981	.979	.973	.970	.967	.965	.964	.965	.966	.979
.685 54 0	.973	.969	.969	.971	.968	.962	.961	.961	.960	.959	.954	.963	.971
.824 58 0	.968	.967	.966	.967	.967	.966	.965	.965	.965	.962	.954	.961	.966
.940 94 0	.967	.967	.964	.966	.973	.974	.974	.977	.979	.977	.978	.980	.980
1.027 94 0	.983	.978	.977	.974	.972	.971	.971	.971	.973	.977	.979	.978	.969
1.161 58 0	.977	.974	.973	.972	.974	.972	.973	.977	.980	.979	.977	.976	.973
1.283 54 0	.973	.971	.975	.973	.970	.971	.977	.976	.981	.982	.977	.975	.976
1.432 18 0	.971	.967	.966	.964	.970	.973	.974	.975	.975	.976	.973	.968	.979

LOCAL FLOW FIELD DATA

+6 -1
MACH = 1.961 RE = 9.79X10 FT ALPHA = 14.530 X/D = 4.100 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINf) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 10 0	.927	.936	.484	.336	.421	.728	.778	.811	.801	.874	.898	.850	.764
.438 6 0	.578	.588	.762	.710	.619	.608	.636	.746	.827	.817	.750	.680	.637
.495 10 0	.980	.977	.816	.719	.726	.704	.714	.714	.731	.691	.720	.863	.938
.564 22 0	.988	.989	.991	.880	.767	.743	.767	.798	.864	.936	.959	.962	.959
.685 50 0	.971	.970	.970	.969	.966	.964	.965	.964	.962	.961	.958	.956	.954
.824 62 0	.969	.967	.966	.967	.965	.960	.961	.962	.960	.957	.950	.947	.958
.940 90 0	.969	.968	.965	.968	.971	.973	.976	.976	.978	.979	.971	.971	.977
1.027 90 0	.982	.978	.976	.974	.971	.967	.969	.971	.971	.968	.966	.971	.983
1.161 62 0	.975	.974	.974	.973	.972	.971	.972	.970	.966	.968	.971	.975	.969
1.283 50 0	.972	.971	.974	.970	.967	.968	.973	.969	.973	.976	.974	.977	.979
1.432 22 0	.970	.966	.965	.964	.964	.965	.967	.967	.968	.971	.975	.972	.981

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.81×10^6 FT ALPHA = 14.530 X/D = 4.400 TEST NO. = 35

AXIAL VELOCITY RATIO -- (V_X / V_{INF}) --

	THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D	RUN NO.													
.964	26 0	.793	.820	.793	.813	.491	.632	.629	.663	.753	.768	.760	.739	.724
.695	46 0	.788	.797	.810	.814	.800	.775	.757	.752	.741	.732	.726	.714	.702
.624	66 0	.707	.666	.736	.793	.767	.742	.730	.741	.625	.540	.614	.683	.717
.940	86 0	.972	.971	.880	.800	.766	.825	.926	.972	.977	.974	.966	.963	.970
1.027	86 0	.982	.977	.975	.974	.973	.969	.969	.969	.969	.967	.967	.967	.968
1.161	66 0	.975	.973	.974	.972	.969	.970	.970	.968	.963	.964	.964	.968	.966
1.283	46 0	.974	.972	.974	.970	.968	.971	.974	.971	.972	.975	.972	.975	.983
1.432	26 0	.973	.967	.966	.963	.966	.968	.965	.963	.965	.966	.970	.973	.978

LOCAL FLOW FIELD DATA

MACH = 1.956 RE = 9.81X10 FT ALPHA = 14.530 X/D = 4.600 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 30 0	1.060	1.078	1.115	1.010	.918	.918	.889	.982	1.032	1.015	1.016	1.003	.985
.665 42 0	1.041	1.074	1.108	1.003	.882	.889	.924	1.025	1.072	1.053	1.030	1.021	1.017
.824 70 0	.942	.958	.972	.939	.927	.959	.969	.959	.937	.922	.914	.909	.901
.940 82 0	.882	.896	.898	.915	.920	.918	.905	.889	.877	.868	.853	.852	.850
1.027 82 0	.855	.860	.878	.891	.889	.879	.861	.852	.840	.832	.830	.827	.815
1.161 70 0	.824	.832	.861	.865	.859	.848	.828	.815	.808	.806	.805	.801	.796
1.283 42 0	.816	.824	.842	.839	.835	.830	.812	.793	.791	.714	.603	.727	.911
1.432 30 0	.756	.743	.782	.826	.811	.725	.688	.838	.968	.964	.961	.965	.983

LOCAL FLOW FIELD DATA

MACH = 1.996 RE = 9.78x10⁶ ALPHA = 14.530 X/D = 6.500 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 34 0	.892	.900	.849	.863	.910	.800	.859	.996	.956	.886	.882	.858	.864
.633 98 0	.998	.998	.994	.956	.947	.953	.968	.974	.977	.979	.974	.962	.958
.685 38 0	.994	.992	.946	.929	.957	.977	.974	.978	.985	.982	.978	.969	.967
.765 102 0	1.002	.976	.886	.863	.923	.966	.974	.985	.985	.977	.968	.952	.947
.824 74 0	1.004	.960	.858	.847	.942	.973	.976	.984	.978	.970	.960	.951	.950
.904 106 0	1.002	.963	.899	.886	.945	.974	.979	.983	.982	.975	.964	.958	.957
.940 78 0	.993	.962	.920	.921	.970	.985	.992	.996	.990	.980	.966	.963	.963
.999 110 0	.978	.967	.955	.953	.972	.976	.981	.983	.979	.972	.957	.960	.964
1.027 78 0	.984	1.002	.982	.965	.978	.986	.993	.989	.983	.975	.967	.959	.973
1.161 74 0	.964	.993	.975	.966	1.000	.993	.984	.980	.982	.969	.963	.965	.962
1.283 38 0	1.000	.978	.961	1.018	1.007	.996	.985	.980	.980	.967	.965	.971	.962
1.432 34 0	1.003	.999	1.017	1.015	1.005	.991	.980	.972	.969	.966	.973	.963	.970
1.538 98 0	1.051	1.036	1.028	1.016	1.005	.995	.985	.977	.972	.983	.978	.970	.973
1.680 102 0	1.054	1.042	1.029	1.014	1.004	.991	.979	.983	1.000	.991	.984	.975	.973
1.798 106 0	1.042	1.037	1.028	1.014	1.008	.993	.992	1.011	1.001	.992	.980	.971	.966
1.923 110 0	1.030	1.025	1.018	1.011	1.007	1.001	.999	.993	.984	.971	.962	.953	.951

LOCAL VORTICITY X 100.

MACH = 1.963 RE = 9.80x10 FT ALPHA = 14.530 X/D = 3.300 TEST NO. = 35

THETA 176.25 168.75 161.25 153.75 146.25 138.75 131.25 123.75 116.25 108.75 101.25 93.75

R/D

.3550	11.614	46.990	150.039	233.503	226.955	195.748	153.399	97.225	28.524	14.293	24.554	25.625
.4165	-6.353	-14.556	17.258	55.212	66.237	55.601	17.767	-11.923	-8.816	3.290	5.481	-19.727
.4665	6.457	6.173	-5.993	-14.738	-17.334	-17.325	-20.952	-18.575	-13.464	-14.706	-10.485	3.738
.5293	-3.766	-6.421	-3.294	-.642	1.765	4.352	4.939	4.484	5.149	5.472	-1.467	-6.105
.6245	.372	1.357	2.498	2.109	.971	.198	.403	.386	.117	-.772	-2.220	.352
.7545	.052	.456	1.059	1.629	1.098	.007	-.463	-.365	-.118	-.437	-4.681	-3.578
.8820	.978	1.134	-.497	-.080	.460	-.161	-.787	-.973	-.652	.898	-.112	-1.440
.9835	-1.423	-1.011	-.717	.683	2.658	2.620	1.731	2.824	4.011	2.260	-.540	-2.948
1.0940	-.522	-.075	-.614	-.785	-.610	-.752	-.350	-.279	-1.060	-.953	-.442	-1.599
1.2220	.240	.857	.795	.483	.485	.529	.449	.116	1.071	1.062	.506	.219
1.3575	-.522	-.169	-.129	-.352	.194	.322	.250	.084	.406	.299	.460	.691

LOCAL VORTICITY X 100.

+6 -1

MACH = 1.961 RE = 9.79x10 FT ALPHA = 14.530 X/D = 4.100 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.4165	5.292	77.422	209.186	219.356	125.317	6.184	23.267	25.100	2.050	-10.398	-36.732	-28.661
.4665	-5.867	15.726	110.338	170.661	176.405	84.884	5.655	-18.324	-27.697	-21.517	-14.138	4.510
.5295	.120	-3.140	-6.803	-5.290	.673	9.976	20.458	12.088	7.024	15.470	2.805	.208
.6245	1.772	2.876	9.275	4.195	4.479	8.118	7.871	3.805	-2.064	-.520	.069	-.784
.7545	.073	.242	.848	-.227	-.054	-.143	-1.319	-1.336	-.784	-.583	-1.933	-3.871
.8820	.231	-.115	-.241	.871	1.360	.826	-.206	-.443	-.555	-.716	-.587	.001
.9835	-.037	.367	-.880	.640	2.673	2.591	2.323	2.654	4.020	3.901	-1.664	-4.522
1.0940	-.948	-.469	-.830	-.959	-.972	-1.386	-1.497	-1.296	-1.327	-1.131	-.847	-2.252
1.2220	-.177	.349	.031	-.213	.456	.768	.476	.479	.852	.450	.322	.248
1.3575	-.512	-.418	-.327	-.459	-.152	.217	.573	.164	-.192	-.020	.589	1.486

LOCAL VORTICITY X 100.

+6 -1

MACH = 1.959 RE = 9.61x10 FT ALPHA = 14.550 X/D = 4.400 TEST NO. = 35

THETA 176.25 168.75 161.25 153.75 146.25 138.75 131.25 123.75 116.25 108.75 101.25 93.75

R/D

.6245	.776	11.466	56.256	76.433	32.965	5.021	7.119	13.241	4.916	-1.007	-1.223	-1.680
.7545	1.236	1.292	.756	1.924	3.168	1.868	2.602	.783	-.382	-2.353	-1.319	2.814
.8820	-2.587	1.030	1.535	-2.132	-5.084	-4.783	2.158	2.554	2.506	7.020	7.492	4.810
.9635	-.170	2.678	-.236	3.119	6.234	1.981	.603	2.222	3.654	3.114	-.502	-4.029
1.0940	-.682	-.069	-.818	-.970	-.658	-.969	-1.695	-1.534	-1.404	-1.409	-1.497	-1.487
1.2220	-.462	-.070	-.469	-.675	-.087	.527	.658	1.119	.973	.541	1.726	.704
1.3575	-.789	-.426	-.311	-.436	-.436	-.099	.334	.087	-.083	-.098	-.448	1.269

LOCAL VORTICITY X 100.

MACH = 1.956 RE = 9.81x10 FT ALPHA = 14.530 X/D = 4.800 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.6245	1.653	2.677	22.370	96.357	62.766	21.654	22.308	11.981	3.439	2.643	1.888	2.078
.7545	2.004	6.125	27.063	80.131	54.907	11.871	3.504	-.019	-.139	1.250	1.248	.555
.8820	-.297	-1.901	-3.515	1.199	3.984	2.821	-.482	-.360	-.742	-2.547	-2.116	-1.367
.9835	3.586	5.207	3.700	4.786	4.528	3.522	4.944	6.870	6.669	6.055	5.260	4.072
1.0940	.721	-1.503	-.566	-.601	.219	.925	-.713	-1.058	-.472	-.783	-.521	-.877
1.2220	.989	-.792	1.247	1.829	1.673	1.314	.529	1.010	2.482	-1.209	-6.295	-2.339
1.3575	-1.454	-4.302	-1.947	.195	-.601	-3.279	-4.991	-2.356	5.139	6.607	3.487	3.356

LOCAL VORTICITY X 100.

MACH = 1.956 RE = 9.78X10 FT ALPHA = 14.530 X/D = 6.500 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.5985	-.785	-2.983	-23.348	-16.570	53.053	41.560	2.115	-.206	5.368	5.509	11.586	16.173
.6590	-6.901	-9.096	1.881	-12.216	-11.772	-6.784	-5.314	-1.807	-3.068	-5.519	-4.313	-4.383
.7250	.738	27.281	73.701	34.483	2.754	5.353	5.350	2.365	2.261	3.878	3.628	2.133
.7945	-7.269	76.051	154.796	58.161	-2.761	-3.335	-1.696	-1.009	-.914	-1.999	-1.274	-1.048
.8640	-1.091	49.535	89.256	36.177	2.412	.372	2.197	1.234	-.192	-.755	-.428	2.290
.9220	-6.266	7.486	23.391	9.103	-.595	-3.247	-3.989	-4.139	-2.636	-2.148	-5.407	-6.011
.9695	.987	12.141	20.603	13.290	2.632	-.064	2.468	2.508	2.030	1.633	.011	1.562
1.0130	-6.180	-4.708	-9.164	-14.359	-2.134	3.398	.488	.292	3.794	5.356	-5.028	-10.704
1.0940	-1.112	1.382	2.880	-.695	-1.500	-1.283	-1.570	-1.010	-1.555	-1.465	-.907	-2.520
1.2220	-.075	-.193	1.438	4.225	.898	1.550	1.834	2.026	1.710	1.392	1.579	1.391
1.3575	.645	.196	-2.047	.569	.575	.950	1.034	.219	-.040	-.287	.645	1.168
1.4850	1.232	2.286	.573	-.257	-.366	-.092	.738	.681	.392	-.347	-1.477	-1.612
1.6090	-.419	-.132	-.372	-.364	-.505	-.666	-.683	-.112	.325	-.211	.111	-.463
1.7390	-.485	-.940	-1.186	-1.461	-1.630	-.985	-.752	-.861	-.450	-.291	-.511	-.558
1.8605	.535	.905	.744	.587	1.393	2.565	1.151	1.238	1.284	1.304	.835	.631

LOCAL CIRCULATION STRENGTH X 100.

+6 -1
MACH = 1.963 RE = 9.60X10 FT ALPHA = 14.530 X/D = 3.500 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.3550	.035	.222	.710	1.105	1.074	.927	.726	.460	.135	.068	.116	.121	5.7201
.4165	-.019	-.043	.052	.165	.198	.166	.053	-.036	-.026	.010	.016	-.059	.4760
.4665	.029	.027	-.027	-.065	-.077	-.077	-.093	-.082	-.060	-.065	-.046	.017	-.5194
.5295	-.023	-.039	-.020	-.004	.011	.027	.030	.027	.031	.033	-.009	-.037	.0273
.6245	.005	.017	.031	.027	.012	.002	.005	.005	.001	-.010	-.028	.004	.0727
.7545	.001	.008	.019	.028	.019	.000	-.008	-.006	-.002	-.008	-.082	-.063	-.0934
.8820	.017	.019	-.008	-.001	.008	-.003	-.013	-.017	-.011	.015	-.002	-.025	-.0210
.9835	-.020	-.014	-.010	.010	.038	.037	.025	.040	.057	.032	-.008	-.042	.1447
1.0940	-.013	-.002	-.015	-.019	-.015	-.018	-.009	-.007	-.026	-.023	-.011	-.039	-.1964
1.2220	.006	.021	.020	.012	.012	.013	.011	.003	.027	.026	.013	.005	.1692
1.3575	-.018	-.006	-.004	-.012	.007	.011	.008	.003	.014	.010	.015	.023	.0511
RSUM	.019	.210	.747	1.245	1.287	1.085	.736	.391	.140	.089	-.025	-.093	5.8309

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = 1.961 RE = 9.79X10 FT ALPHA = 14.530 X/D = 4.100 TEST NO. = 35

THETA	176.25	166.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.4165	.016	.231	.624	.655	.374	.018	.069	.075	.006	-.031	-.110	-.086	1.6422
.4665	-.026	.070	.489	.756	.782	.376	.025	-.081	-.123	-.095	-.063	.020	2.1301
.5295	.001	-.019	-.041	-.032	.004	.061	.125	.074	.043	.094	.017	.001	.3263
.6245	.022	.036	.117	.053	.056	.102	.099	.048	-.026	-.007	.001	-.010	.4923
.7545	.001	.004	.015	-.004	-.001	-.003	-.023	-.023	-.014	-.010	-.034	-.068	-.1588
.8820	.004	-.002	-.004	.015	.023	.014	-.004	-.008	-.009	-.012	-.010	.000	.0073
.9835	-.001	.005	-.013	.009	.038	.037	.033	.038	.057	.056	-.024	-.064	.1721
1.0940	-.023	-.011	-.020	-.023	-.024	-.034	-.037	-.032	-.032	-.028	-.021	-.055	-.3399
1.2220	-.004	.009	.001	-.005	.011	.019	.012	.012	.021	.011	.008	.006	.1004
1.3575	-.017	-.014	-.011	-.015	-.005	.007	.019	.006	-.006	-.001	.020	.050	.0320
RSUM	-.027	.308	1.156	1.408	1.259	.599	.319	.108	-.083	-.023	-.215	-.206	4.6039

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = 1.959 RE = 9.81X10 FT ALPHA = 14.530 X/D = 4.400 TEST NO. = 35

THETA	176.25	166.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.6245	.010	.144	.708	.963	.415	.063	.090	.167	.062	-.013	-.015	-.024	2.5703
.7545	.022	.023	.013	.034	.055	.033	.045	.014	-.007	-.041	-.023	.049	.2166
.8820	-.044	.018	.026	-.036	-.087	-.082	.037	.044	.043	.120	.128	.082	.2476
.9835	-.002	.038	-.003	.044	.089	.028	.009	.032	.052	.044	-.007	-.057	.2662
1.0940	-.017	-.002	-.020	-.024	-.016	-.024	-.041	-.037	-.034	-.034	-.037	-.036	-.3223
1.2220	-.011	-.002	-.012	-.017	-.002	.013	.016	.028	.024	.013	.043	.018	.1115
1.3575	-.027	-.014	-.010	-.015	-.015	-.003	.011	.003	-.003	-.003	-.015	.043	-.0484
RSLM	-.070	.205	.702	.949	.440	.029	.167	.249	.137	.086	.073	.074	3.0414

LOCAL CIRCULATION STRENGTH X 100.

*6 -1

MACH = 1.956 RE = 9.81x10 FT ALPHA = 14.530 X/D = 4.800 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.6245	.021	.034	.262	1.214	.790	.273	.281	.151	.043	.033	.024	.026	3.1714
.7545	.035	.107	.473	1.401	.960	.207	.061	-.000	-.002	.022	.022	.010	3.2948
.8820	-.005	-.032	-.060	.020	.068	.048	-.008	-.006	-.013	-.043	-.036	-.023	-.0911
.9835	.051	.074	.053	.068	.065	.050	.070	.098	.095	.086	.075	.058	.8442
1.0940	.018	-.037	-.014	-.015	.005	.023	-.017	-.026	-.012	-.019	-.013	-.021	-.1278
1.2220	.025	-.020	.031	.045	.042	.033	.013	.025	.062	-.030	-.156	-.058	.0109
1.3575	-.049	-.145	-.066	.007	-.020	-.111	-.168	-.079	.173	.223	.118	.113	-.0049
RSUM	.095	-.019	.699	2.740	1.909	.523	.232	.162	.347	.272	.033	.104	7.0975

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = 1.956 RE = 9.78X10 FT ALPHA = 14.530 X/D = 6.500 TEST NO. = 35

THETA	176.25	166.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.5985	-.003	-.021	-.161	-.114	.365	.286	.015	-.001	.037	.038	.080	.111	.6296
.6590	-.051	-.052	.011	-.070	-.067	-.039	-.030	-.010	-.018	-.032	-.025	-.025	-.4072
.7250	.007	.264	.712	.333	.027	.052	.052	.023	.022	.037	.035	.021	1.5846
.7945	-.057	.594	1.209	.454	-.022	-.026	-.013	-.008	-.007	-.016	-.010	-.008	2.0915
.8640	-.013	.571	1.028	.417	.028	.004	.025	.014	-.002	-.009	-.005	.026	2.0852
.9220	-.035	.041	.129	.050	-.003	-.018	-.022	-.023	-.015	-.012	-.030	-.033	.0307
.9695	.009	.116	.196	.127	.025	-.001	.024	.024	.019	.016	.000	.015	.5703
1.0130	-.029	-.022	-.043	-.068	-.010	.016	.002	.001	.018	.025	-.024	-.051	-.1841
1.0940	-.027	.034	.070	-.017	-.037	-.031	-.038	-.025	-.038	-.036	-.022	-.062	-.2286
1.2220	-.002	-.005	.036	.105	.022	.039	.046	.050	.042	.035	.039	.035	.4417
1.3575	.022	.007	-.069	.019	.019	.032	.035	.007	-.001	-.010	.022	.039	.1223
1.4850	.032	.060	.015	-.007	-.010	-.002	.019	.018	.010	-.009	-.039	-.042	.0459
1.6090	-.016	-.005	-.014	-.014	-.019	-.025	-.034	-.004	.012	-.008	.004	-.018	-.1406
1.7390	-.017	-.032	-.041	-.050	-.056	-.034	-.026	-.029	-.015	-.010	-.017	-.019	-.3458
1.8605	.021	.035	.029	.023	.054	.099	.045	.048	.050	.051	.032	.024	.5106
RSUM	-.160	1.584	3.109	1.189	.317	.352	.098	.085	.115	.061	.041	.014	6.8060

SECTION VII

$M_{\infty} = 1.96$, $\alpha = 20.3^{\circ}$, $Re = 9.8 \times 10^6 \text{ ft}^{-1}$,

$X/D = 3.5, 4.1, 4.4, 4.8, 6.5$

LOCAL FLOW FIELD DATA

MACH = 1.961 RE = 9.80x10 FT ALPHA = 20.250 X/D = 3.500 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA		180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D	RUN NO.													
.315	3 1	2.227	2.219	2.197	2.225	2.086	1.761	1.493	1.468	1.308	1.601	2.148	1.676	1.791
.395	15 0	2.527	2.342	1.834	1.719	1.852	2.009	1.729	1.938	2.213	2.225	2.175	2.166	2.211
.438	3 1	2.660	2.585	2.166	1.668	1.779	2.140	2.126	2.121	2.102	2.148	2.198	2.185	2.169
.495	15 0	2.271	2.105	1.678	1.556	2.090	2.417	2.273	2.114	2.077	2.096	2.098	2.124	2.114
.564	19 1	2.039	2.107	1.960	1.853	2.157	2.345	2.250	2.140	2.072	2.115	2.165	2.188	2.149
.685	55 0	1.901	1.918	1.955	1.981	2.002	2.047	2.057	2.038	2.017	2.022	2.062	2.047	1.993
.824	59 0	1.905	1.909	1.922	1.935	1.979	2.011	2.025	2.013	1.995	2.008	2.021	1.984	1.949
.940	95 0	1.908	1.907	1.923	1.956	1.980	2.012	2.029	2.037	2.021	2.067	2.054	2.021	2.006
1.027	95 0	1.950	1.936	1.951	1.961	1.968	1.991	1.994	1.974	2.001	2.056	2.032	2.005	1.955
1.161	59 0	1.961	1.944	1.968	1.968	1.951	1.974	1.987	1.957	1.984	2.028	1.997	1.974	1.945
1.283	55 0	1.969	1.950	1.970	1.975	1.952	1.969	1.973	1.976	2.005	2.009	1.988	1.961	1.936
1.432	19 1	1.947	1.937	1.949	1.942	1.926	1.947	1.966	1.991	2.024	2.016	1.992	1.962	1.932

LOCAL FLOW FIELD DATA

*6 -1

MACH = 1.962 RE = 9.79X10 FT ALPHA = 20.250 X/D = 4.100 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 11 0	.850	.829	.707	.991	1.699	1.555	1.136	.679	.681	1.046	1.822	1.596	1.420
.438 7 0	.634	.632	.641	.675	1.265	1.452	1.647	1.632	1.899	2.015	1.570	.947	.705
.495 11 0	2.225	1.955	.929	.888	1.160	1.543	1.698	1.763	1.602	1.406	1.298	1.540	1.816
.564 23 0	2.476	2.303	1.338	1.282	1.578	1.835	1.727	1.639	1.586	1.679	2.048	2.186	2.106
.685 51 0	1.974	1.903	1.842	1.915	1.888	1.973	2.078	2.072	2.037	2.018	2.029	2.023	2.000
.824 63 0	1.868	1.898	1.920	1.953	2.005	2.041	2.056	2.055	2.035	1.985	1.981	1.989	1.970
.940 91 0	1.882	1.895	1.933	1.973	2.019	2.058	2.092	2.112	2.093	2.043	2.053	2.049	2.014
1.027 91 0	1.931	1.920	1.949	1.971	1.988	2.021	2.027	2.024	2.010	2.004	2.029	2.032	1.987
1.161 63 0	1.939	1.921	1.953	1.963	1.958	1.996	2.014	1.983	1.952	1.970	2.024	1.989	1.962
1.283 51 0	1.959	1.939	1.965	1.975	1.967	1.996	2.002	1.971	1.956	1.985	2.011	1.975	1.958
1.432 23 0	1.943	1.923	1.943	1.944	1.937	1.962	1.973	1.967	1.982	2.030	2.014	1.977	1.961

LOCAL FLOW FIELD DATA

*6 -1

MACH = 1.956 RE = 9.81x10 FT ALPHA = 20.250 X/D = 4.400 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.964 27 1	1.424	1.311	1.160	1.119	1.437	1.228	.805	1.266	1.828	1.774	1.710	1.687	1.636
.685 47 0	1.605	1.487	1.392	1.446	1.590	1.821	1.930	1.834	1.681	1.609	1.535	1.520	1.495
.824 67 0	1.443	1.598	1.563	1.589	1.645	1.675	1.719	1.682	1.622	1.612	1.014	.995	1.347
.940 87 0	1.556	1.645	1.657	1.657	1.656	1.691	1.608	1.418	1.497	1.794	2.003	2.037	2.007
1.027 87 0	1.947	1.621	1.374	1.371	1.364	1.573	1.770	2.003	2.040	1.996	2.005	2.063	1.989
1.161 67 0	1.924	1.909	1.945	1.960	1.960	2.007	2.026	1.996	1.975	1.979	2.005	2.011	1.964
1.283 47 0	1.944	1.914	1.945	1.963	1.962	1.996	2.011	1.993	1.979	2.003	2.030	1.984	1.976
1.432 27 1	1.964	1.925	1.948	1.955	1.956	1.970	1.979	1.980	1.962	1.981	2.024	1.983	1.969

LOCAL FLOW FIELD DATA

MACH = 1.957 RE = 9.81x10 FT ALPHA = 20.250 X/D = 4.800 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 31 0	2.379	2.400	2.497	1.995	1.895	1.921	2.074	2.324	2.379	2.438	2.329	2.224	2.192
.665 43 0	2.514	2.234	1.995	1.907	1.866	1.750	2.152	2.551	2.577	2.504	2.420	2.362	2.344
.824 71 0	2.071	1.901	1.698	1.782	1.799	1.851	2.167	2.255	2.163	2.100	2.028	1.959	1.899
.940 83 0	1.806	1.865	1.857	2.041	2.151	2.054	2.003	1.980	1.932	1.864	1.804	1.759	1.726
1.027 83 0	1.721	1.769	1.903	2.034	1.970	1.877	1.832	1.882	1.835	1.767	1.709	1.669	1.644
1.161 71 0	1.647	1.702	1.792	1.879	1.822	1.771	1.752	1.764	1.737	1.680	1.616	1.581	1.581
1.283 43 0	1.652	1.667	1.700	1.785	1.715	1.674	1.675	1.704	1.685	1.628	1.537	1.388	1.171
1.432 31 0	1.634	1.650	1.667	1.691	1.648	1.630	1.646	1.627	1.464	1.525	1.927	2.016	1.928

LOCAL FLOW FIELD DATA

MACH = 1.960 RE = 9.78x10⁶ FT ALPHA = 20.250 X/D = 6.500 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 35 0	1.761	1.734	1.563	1.585	1.888	1.724	1.644	1.385	1.115	2.440	2.823	2.128	2.023
.633 99 0	1.833	1.872	1.812	1.617	1.734	1.455	1.680	2.158	2.326	2.287	2.431	2.518	2.400
.685 39 0	2.010	1.914	1.790	1.650	1.877	2.217	2.365	2.234	2.266	2.276	2.358	2.402	2.303
.765 103 0	2.154	1.835	1.568	1.662	1.941	2.145	2.257	2.206	2.191	2.276	2.321	2.259	2.147
.824 75 0	2.297	1.820	1.393	1.787	2.086	2.206	2.241	2.165	2.120	2.235	2.250	2.158	2.066
.904 107 0	2.035	1.621	1.328	1.894	2.180	2.232	2.215	2.105	2.166	2.267	2.215	2.107	2.033
.940 79 0	2.002	1.624	1.416	1.954	2.203	2.260	2.255	2.153	2.183	2.252	2.197	2.104	2.039
.999 111 0	1.663	1.595	1.693	2.025	2.160	2.229	2.192	2.066	2.165	2.222	2.151	2.076	2.021
1.027 79 0	1.789	1.629	1.695	2.070	2.126	2.150	2.148	2.044	2.049	2.159	2.097	2.060	2.011
1.161 75 0	1.884	1.722	1.739	1.986	2.075	2.191	2.095	2.013	2.018	2.098	2.056	2.025	1.969
1.283 39 0	1.933	1.891	1.926	2.021	2.112	2.151	2.097	1.989	1.958	2.111	2.052	2.017	1.975
1.432 35 0	1.996	1.965	2.056	2.082	2.054	2.037	2.069	1.960	1.924	2.069	2.023	1.984	1.972
1.538 99 0	2.074	2.042	2.106	2.096	2.098	2.103	2.056	2.031	2.060	2.031	2.014	1.985	1.959
1.680 103 0	2.104	2.084	2.087	2.078	2.048	2.027	2.033	1.997	2.047	2.040	2.010	1.968	1.955
1.798 107 0	2.145	2.096	2.089	2.054	2.036	2.052	2.049	2.055	2.041	2.048	2.033	1.995	1.956
1.923 111 0	2.154	2.112	2.102	2.076	2.054	2.060	2.076	2.095	2.052	2.036	1.995	1.946	1.906

LOCAL FLOW FIELD DATA

MACH = 1.961 RE = 9.60x10 FT ALPHA = 20.230 X/D = 3.500 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 3 1	8.192	8.955	11.054	14.199	16.277	16.887	9.394	2.364	19.669	36.225	31.471	33.589	33.131
.395 15 0	21.158	21.750	17.317	11.656	17.886	14.482	15.799	27.812	29.696	29.405	28.684	28.792	29.449
.438 3 1	20.833	21.696	20.117	8.930	19.100	26.018	26.939	27.737	26.976	27.908	27.999	27.613	27.342
.495 15 0	13.757	16.311	7.501	25.315	35.373	33.423	30.201	27.318	27.076	27.081	27.349	27.275	25.963
.564 19 1	7.233	10.444	13.758	22.913	32.343	32.576	29.581	27.222	25.550	26.042	26.983	26.647	25.423
.685 55 0	5.807	8.530	15.408	21.368	25.586	27.921	27.932	26.723	25.515	25.673	26.567	25.887	24.196
.824 59 0	12.650	13.624	16.359	19.301	21.651	23.403	24.453	24.512	24.325	25.098	25.380	24.412	23.098
.940 95 0	15.106	16.078	17.546	19.138	20.690	21.888	22.540	22.832	23.010	23.770	24.029	23.146	22.038
1.027 95 0	15.513	16.027	17.156	18.593	19.940	21.057	21.736	22.264	23.443	24.162	23.276	22.521	21.897
1.161 59 0	16.467	17.083	17.721	18.703	19.807	20.776	21.315	21.682	22.603	23.083	22.234	21.393	20.638
1.283 55 0	17.500	17.474	17.977	18.903	19.774	20.354	20.923	21.387	22.054	22.434	22.040	21.078	20.752
1.432 19 1	18.776	18.528	18.746	19.690	20.780	21.213	21.346	21.779	22.196	21.948	21.637	21.043	20.251

LOCAL FLOW FIELD DATA

MACH = 1.962 RE = 9.79X10⁶ FT ALPHA = 20.250 X/D = 4.100 TEST NO. = 35

LOCAL ANGLE OF ATTACK		-- (ALPHA) --													DEG.	
THETA		180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00		
R/D	RUN NO.															
.395	11 0 13.594	15.586	33.083	40.808	24.322	17.522	21.288	45.049	54.187	41.632	34.225	37.635	38.690			
.438	7 0 8.323	.856	17.395	33.089	39.411	35.912	27.104	24.564	28.099	33.035	38.338	47.472	59.467			
.495	11 0 17.650	18.448	7.135	41.416	46.500	44.547	42.043	39.865	38.398	36.870	34.213	30.207	28.437			
.564	23 0 17.651	19.122	8.117	36.441	41.874	41.249	40.085	38.024	32.676	28.545	26.803	26.195	25.529			
.685	51 0 4.799	8.994	17.839	25.524	31.448	33.100	29.958	27.492	26.008	25.262	25.671	25.605	24.626			
.824	63 0 8.339	11.142	17.196	21.268	23.377	25.234	26.166	25.923	25.186	24.192	24.904	24.936	23.600			
.940	91 0 12.717	14.030	17.082	19.800	21.499	22.536	23.485	23.845	23.581	23.069	23.671	23.634	22.537			
1.027	91 0 14.231	15.307	17.042	18.824	20.407	21.925	22.918	23.395	23.443	23.558	24.118	23.172	21.931			
1.161	63 0 15.586	16.570	17.557	18.801	20.045	21.236	21.818	22.163	22.556	22.837	22.971	21.928	21.018			
1.283	51 0 16.755	17.151	17.832	18.966	19.880	20.586	21.400	21.828	22.078	22.788	22.606	21.612	21.133			
1.432	23 0 18.160	18.123	18.495	19.601	20.745	21.351	21.607	21.971	22.326	22.611	22.231	21.479	20.724			

LOCAL FLOW FIELD DATA

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MACH = 1.956 RE = 9.81x10 FT ALPHA = 20.250 X/D = 4.400 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.964 27 1 4.252	19.119	39.005	45.979	38.232	33.753	60.685	46.576	34.533	34.948	37.069	37.543	36.991	
.685 47 0 5.893	6.497	20.295	36.122	40.530	40.241	38.082	35.911	35.538	34.768	34.478	34.566	34.206	
.624 67 0 10.929	16.513	27.473	34.220	35.379	35.886	36.443	35.913	34.857	33.605	40.050	36.719	29.412	
.940 67 0 15.914	20.644	26.035	29.875	31.750	31.831	35.251	34.391	29.652	25.219	23.735	23.770	23.006	
1.027 67 0 12.673	20.504	30.606	32.668	32.464	28.839	27.119	24.578	23.897	23.594	23.754	23.726	21.669	
1.161 67 0 15.226	16.206	17.503	18.983	20.218	21.515	22.163	22.659	22.931	22.967	23.020	22.308	21.147	
1.263 47 0 16.335	16.977	17.592	18.690	19.736	20.732	21.469	21.825	21.955	22.359	22.663	21.794	21.123	
1.432 27 1 17.695	17.850	18.470	19.576	20.680	21.407	21.910	22.253	22.500	22.570	22.602	21.696	20.945	

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.937 RE = 9.81X10 FT ALPHA = 20.250 X/O = 4.800 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/O RUN NO.													
.964 31 0 10.598	13.125	22.330	24.085	16.572	5.553	10.908	20.314	24.564	25.378	25.918	26.793	26.440	
.685 43 0 11.716	15.136	22.215	21.330	15.767	13.189	16.408	20.139	22.267	22.960	23.140	23.519	23.508	
.824 71 0 6.038	5.082	4.226	21.700	24.796	25.182	25.976	25.658	26.046	26.236	25.943	25.809	25.480	
.940 63 0 8.116	9.576	18.293	25.000	26.468	26.682	27.784	28.553	28.375	28.112	27.924	27.569	26.720	
1.027 63 0 14.175	15.697	20.312	24.687	26.420	26.880	27.818	29.334	29.246	29.061	28.853	28.412	28.300	
1.161 71 0 19.634	20.795	22.313	25.121	26.634	27.793	28.802	29.649	29.738	29.197	28.837	28.607	27.769	
1.283 43 0 22.247	23.447	24.433	25.867	27.476	28.562	29.629	29.924	29.877	29.381	29.769	31.108	27.009	
1.432 31 0 25.636	25.153	25.476	26.932	28.286	28.900	29.055	30.159	31.069	26.893	23.364	21.858	21.445	

LOCAL FLOW FIELD DATA

*6 -1

MACH = 1.960 RE = 9.78X10 FT ALPHA = 20.250 W/D = 0.500 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.964 35 0	2.871	3.183	4.397	3.391	10.235	15.630	14.450	9.956	26.136	33.925	34.590	35.815	33.930
.633 99 0	2.939	4.558	9.581	4.519	7.736	18.119	36.448	34.609	31.877	31.996	33.247	33.100	31.588
.685 39 0	7.594	8.255	11.296	6.407	12.172	25.088	31.577	29.788	29.498	30.999	31.756	31.212	29.776
.765 103 0	12.408	12.859	11.921	19.215	20.938	25.552	28.649	28.155	29.238	31.399	31.572	30.383	29.265
.624 75 0	16.009	14.519	12.023	24.142	23.043	25.109	27.190	26.691	28.175	30.191	29.909	28.847	27.792
.904 107 0	12.295	8.805	18.551	30.168	26.543	25.948	26.416	25.432	28.525	29.934	28.888	28.043	27.011
.940 79 0	11.918	8.346	18.677	28.470	25.527	25.080	25.569	24.693	27.364	28.927	28.011	26.883	25.664
.999 111 0	2.562	7.268	23.143	28.368	26.589	26.018	25.548	24.425	27.373	28.785	27.754	26.747	25.770
1.027 79 0	3.293	6.692	21.098	27.116	25.743	25.550	25.021	23.913	25.193	28.872	27.498	25.872	24.246
1.161 75 0	1.190	10.233	22.119	24.091	24.084	25.236	24.112	22.910	24.035	27.027	25.632	24.309	22.944
1.263 39 0	5.080	12.880	19.738	22.446	22.705	24.495	23.731	22.886	23.729	25.650	24.549	23.721	22.539
1.432 35 0	9.563	12.237	16.984	19.771	21.291	22.827	23.525	22.809	23.330	24.804	23.986	23.077	22.280
1.538 99 0	9.792	13.058	15.882	18.486	20.304	22.147	22.346	22.651	23.847	23.733	23.047	22.004	21.482
1.680 103 0	11.010	13.106	15.903	18.153	19.826	21.409	21.893	22.288	23.032	22.928	22.394	21.754	20.792
1.798 107 0	11.574	13.559	15.701	17.820	19.521	21.195	21.127	21.281	21.894	21.921	21.555	21.065	20.577
1.923 111 0	12.417	13.567	15.426	17.105	18.597	20.228	20.391	20.298	21.097	21.823	21.556	21.162	20.962

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.961 RE = 9.80x10 FT ALPHA = 20.250 X/D = 3.500 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 3 1	180.0	-139.1	-103.4	-70.9	-39.0	-30.7	-79.8	156.8	68.7	77.7	73.6	66.4	73.9
.395 15 0	180.0	-155.3	-137.1	-57.5	1.4	18.8	53.6	63.3	61.7	67.9	73.3	79.6	86.4
.438 3 1	180.0	-168.7	-148.3	-129.9	35.9	32.5	44.0	51.1	56.1	64.3	70.6	75.9	81.3
.495 15 0	180.0	-176.5	-158.9	-56.3	46.4	43.9	46.3	50.9	58.3	64.2	71.3	77.6	81.8
.564 19 1	180.0	-155.6	-107.3	61.7	49.4	47.6	48.3	52.1	57.2	64.9	73.3	79.6	83.8
.685 55 0	.0	41.7	57.2	54.9	54.8	54.8	54.2	55.7	59.7	66.0	74.3	79.5	83.5
.824 59 0	.0	20.0	33.2	40.8	45.8	48.9	51.6	54.7	59.1	67.0	73.4	77.9	83.7
.940 95 0	.0	15.0	27.0	34.5	40.5	46.0	49.9	53.5	58.4	67.2	73.2	78.2	84.2
1.027 95 0	.0	12.2	24.1	34.2	41.2	47.8	53.0	57.5	65.0	72.4	76.1	80.4	86.0
1.161 99 0	.0	10.6	21.0	30.2	38.0	45.1	50.4	56.5	64.5	70.4	74.8	79.9	85.4
1.283 95 0	.0	10.6	19.8	29.1	36.8	44.1	50.5	57.8	66.0	71.1	75.2	80.4	85.3
1.432 19 1	.0	10.9	18.5	27.3	34.9	42.9	50.1	57.8	65.4	70.8	75.1	80.0	86.4

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.062 RE = 0.75X10 FT ALPHA = 20.250 X/D = 4.100 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 11 0	.0	-30.7	-36.3	-14.9	-11.2	-15.6	8.8	33.4	49.9	79.9	71.8	52.1	60.1
.438 7 0	.0	67.8	-53.1	2.1	8.9	16.6	30.0	54.2	64.8	50.9	44.0	47.9	64.0
.495 11 0	180.0	-169.4	83.2	35.0	38.9	40.1	37.3	36.9	34.8	38.2	46.9	62.7	74.0
.564 23 0	180.0	-167.3	79.6	38.4	39.1	41.0	40.7	39.9	43.8	55.5	71.0	78.4	82.0
.685 51 0	-180.0	129.1	71.7	48.3	47.0	49.1	51.0	55.1	59.8	65.0	71.3	77.4	83.1
.824 63 0	.0	34.9	45.7	46.0	46.6	49.6	52.5	55.9	59.8	63.4	70.3	77.5	84.0
.940 91 0	.0	19.3	32.3	38.8	43.4	47.4	51.1	55.2	59.7	63.6	70.6	78.0	84.7
1.027 91 0	.0	16.4	29.0	37.4	44.0	50.5	54.9	59.0	63.1	68.6	75.5	80.7	86.1
1.161 63 0	.0	12.0	23.1	32.4	39.6	47.0	52.0	56.7	61.0	67.2	75.4	79.8	85.7
1.283 51 0	.0	11.9	21.4	30.8	38.8	46.3	52.1	56.7	62.4	70.0	75.7	80.6	85.7
1.432 23 0	.0	9.1	18.3	27.1	34.9	43.0	48.9	53.7	61.2	70.1	74.2	79.0	84.7

LOCAL FLOW FIELD DATA

MACH = 1.956 RE = 9.81x10⁶ FT ALPHA = 20.250 X/D = 4.400 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 27 1	-180.0	-83.7	-46.2	-18.6	-6.0	2.7	22.3	40.3	44.9	46.4	51.1	54.6	57.1
.685 47 0	-180.0	153.2	48.5	31.8	30.3	34.0	36.7	39.1	42.4	45.1	48.0	52.1	55.6
.824 67 0	.0	45.9	44.0	35.2	32.6	36.2	39.5	41.2	43.4	44.7	49.6	56.3	62.7
.940 87 0	.0	30.9	32.2	30.7	30.5	34.3	39.0	40.3	46.7	57.3	68.5	76.9	83.6
1.027 87 0	.0	20.8	24.2	25.9	27.6	36.7	48.5	58.2	63.6	67.9	73.8	81.2	85.5
1.161 67 0	.0	13.1	24.3	33.1	40.2	47.8	52.9	57.4	61.5	67.1	74.7	80.1	85.5
1.283 47 0	.0	11.0	21.7	31.1	39.0	46.5	52.1	57.7	62.4	69.0	76.7	81.5	86.7
1.432 27 1	.0	6.6	18.8	27.4	35.4	42.8	48.9	53.9	59.4	66.9	73.9	78.5	84.3

LOCAL FLOW FIELD DATA

MACH = 1.957 RE = 9.81X10 FT ALPHA = 20.250 X/D = 4.800 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 31 0	180.0	-128.4	-101.1	-75.4	-58.2	-58.6	76.2	73.3	77.5	79.8	80.5	82.5	84.2
.685 43 0	180.0	-132.6	-101.5	-75.6	-38.0	5.5	39.8	62.1	71.7	74.8	78.1	80.4	82.7
.824 71 0	180.0	-164.2	60.5	38.0	34.4	39.5	44.7	49.2	54.7	58.9	61.9	65.1	68.2
.940 83 0	.0	38.6	49.8	46.7	42.3	38.3	42.1	45.9	49.0	52.1	54.9	58.6	61.9
1.027 83 0	.0	24.1	38.5	44.6	40.5	40.4	43.3	48.1	51.3	53.7	56.5	60.0	65.5
1.161 71 0	.0	13.5	26.5	34.5	34.2	35.9	39.8	44.7	47.6	50.0	52.8	56.7	61.8
1.283 43 0	.0	11.8	22.4	30.2	31.8	34.4	38.6	44.3	47.5	49.4	52.4	57.2	60.1
1.432 31 0	.0	10.4	19.6	25.9	28.7	32.6	38.0	42.7	44.9	54.8	72.8	82.2	85.5

LOCAL FLOW FIELD DATA

MACH = 1.960 RE = 9.78x10⁴ FT ALPHA = 20.250 X/D = 6.500 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D / RUN NO.													
.364 35 0	180.0	-119.2	3.4	122.1	-138.0	-93.6	-41.5	-2.4	75.0	84.9	79.3	78.9	84.5
.633 99 0	180.0	-105.0	-52.8	-41.3	155.7	91.3	74.1	68.6	68.6	73.3	80.5	84.1	85.1
.685 39 0	-180.0	-119.5	-63.4	-19.0	75.2	79.4	72.9	67.3	68.7	73.6	80.2	83.4	84.6
.765 103 0	-180.0	-142.3	-47.6	13.8	45.3	63.9	68.8	67.7	68.2	75.4	79.6	81.3	83.4
.824 75 0	180.0	-149.2	-14.2	22.9	40.0	59.4	65.6	65.2	67.2	74.8	79.3	81.4	83.8
.904 107 0	180.0	-154.7	29.6	33.5	41.9	56.6	62.1	62.4	69.5	74.4	76.8	79.5	82.6
.940 79 0	-180.0	-175.9	39.9	35.1	40.6	54.3	60.5	61.0	69.1	74.5	76.9	79.6	82.8
.999 111 0	-180.0	92.8	50.5	41.2	46.3	55.9	60.1	61.2	69.6	74.1	76.4	79.4	82.7
1.027 79 0	180.0	129.1	47.8	39.2	45.8	56.0	61.4	62.9	68.8	76.5	78.8	81.7	84.8
1.161 75 0	.0	68.0	41.6	41.3	47.6	55.6	57.6	59.0	65.0	73.3	75.4	78.4	82.9
1.283 39 0	.0	56.8	53.0	44.8	51.4	55.5	57.4	59.2	65.2	73.3	76.0	79.4	83.8
1.432 35 0	.0	34.1	45.8	46.4	48.4	52.2	55.3	57.7	64.2	70.9	74.0	77.9	81.4
1.538 99 0	.0	29.4	40.9	44.3	47.7	52.8	54.3	59.5	68.0	70.8	74.2	78.5	83.5
1.680 103 0	.0	22.7	33.7	38.9	43.2	49.7	52.3	57.0	65.8	69.3	73.7	78.9	86.4
1.798 107 0	.0	17.4	28.0	34.5	40.6	49.0	53.7	61.2	64.8	69.8	74.6	79.0	83.5
1.923 111 0	.0	14.6	25.3	32.8	39.9	49.3	55.9	62.2	66.2	70.9	74.2	77.8	81.7

LOCAL FLOW FIELD DATA

+8 -1

MACH = 1.961 RE = 9.60x10 FT ALPHA = 20.250 X/D = 3.500 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	160.00	172.50	185.00	197.50	210.00	222.50	235.00	247.50	260.00	272.50	285.00	297.50	310.00
R/D RUN NO.													
.315 3 1	-.143	-.148	-.147	-.157	-.117	-.044	-.071	-.082	-.025	.030	-.113	.054	.006
.395 15 0	-.246	-.232	-.194	-.199	-.143	-.106	-.052	-.081	-.134	-.132	-.117	-.120	-.133
.438 3 1	-.230	-.237	-.235	-.245	-.176	-.169	-.124	-.091	-.084	-.105	-.116	-.110	-.103
.495 15 0	-.136	-.151	-.180	-.191	-.184	-.192	-.133	-.078	-.079	-.088	-.089	-.091	-.076
.564 19 1	-.048	-.086	-.133	-.162	-.189	-.184	-.135	-.091	-.063	-.083	-.108	-.111	-.090
.685 55 0	.019	.010	-.011	-.028	-.058	-.080	-.075	-.058	-.045	-.055	-.076	-.066	-.035
.824 59 0	.024	.019	.013	.004	-.022	-.040	-.046	-.040	-.032	-.052	-.057	-.034	-.011
.940 95 0	.021	.022	.015	.000	-.015	-.029	-.035	-.038	-.036	-.061	-.053	-.034	-.023
1.027 95 0	.005	.009	-.000	-.005	-.008	-.019	-.021	-.012	-.030	-.055	-.041	-.027	.002
1.161 59 0	.004	.010	-.005	-.004	.004	-.009	-.014	-.006	-.025	-.040	-.023	-.010	.009
1.283 55 0	-.001	.008	-.005	-.005	.007	-.002	-.009	-.014	-.031	-.031	-.017	-.001	.013
1.432 19 1	.006	.014	.006	.009	.015	.005	-.005	-.020	-.035	-.029	-.017	-.000	.017

LOCAL FLOW FIELD DATA

MACH = 1.962 RE = 9.79X10 FT ALPHA = 20.250 X/D = 4.100 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA		180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D	RUN NO.													
.395	11 0	.636	.618	.652	.606	.080	.012	.125	.280	.332	.321	.041	.320	.381
.438	7 0	.477	.503	.401	.362	.282	.138	.008	-.059	-.089	-.003	.308	1.003	1.492
.495	11 0	-.180	-.153	.117	.251	.260	.149	.149	.156	.253	.343	.325	.140	.014
.564	23 0	-.190	-.195	-.019	.022	.046	.024	.111	.182	.178	.078	-.067	-.110	-.081
.685	51 0	-.015	-.027	-.049	-.055	-.059	-.077	-.088	-.077	-.058	-.052	-.057	-.054	-.041
.824	63 0	.040	.026	.010	-.013	-.038	-.064	-.071	-.066	-.052	-.032	-.037	-.038	-.021
.940	91 0	.036	.029	.012	-.008	-.030	-.050	-.067	-.073	-.062	-.043	-.054	-.049	-.024
1.027	91 0	.012	.016	.001	-.007	-.017	-.035	-.038	-.037	-.028	-.027	-.041	-.034	-.011
1.161	63 0	.014	.017	.000	-.002	-.001	-.023	-.029	-.015	-.002	-.013	-.037	-.018	-.001
1.283	51 0	.005	.013	-.003	-.005	-.002	-.018	-.022	-.006	-.005	-.026	-.027	-.008	-.001
1.432	23 0	.009	.018	.010	.008	.010	-.002	-.006	-.003	-.014	-.038	-.029	-.010	.002

LOCAL FLOW FIELD DATA

*6 -1

MACH = 1.956 RE = 9.81x10 FT ALPHA = 20.250 X/D = 4.400 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 27 1	.230	.268	.198	.124	.090	.137	.480	.354	.090	.158	.187	.204	.244
.685 47 0	.261	.088	-.037	.042	.083	.051	.038	.104	.190	.241	.297	.318	.349
.824 67 0	.329	.206	.176	.208	.219	.181	.150	.184	.234	.243	.892	.739	.306
.940 87 0	.196	.197	.219	.221	.223	.188	.224	.293	.216	.063	-.034	-.044	-.023
1.027 87 0	.004	.170	.372	.393	.359	.173	.068	-.034	-.041	-.020	-.027	-.049	-.014
1.161 67 0	.018	.022	.003	-.001	-.003	-.029	-.037	-.024	-.012	-.015	-.031	-.027	-.003
1.283 47 0	.009	.019	.004	-.003	-.004	-.021	-.030	-.019	-.013	-.026	-.040	-.016	-.007
1.432 27 1	.001	.020	.007	.004	.000	-.008	-.010	-.010	-.005	-.018	-.034	-.011	-.007

LOCAL FLOW FIELD DATA

MACH = 1.957 RE = 9.81x10 FT ALPHA = 20.250 X/D = 4.800 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 31 0	-.213	-.224	-.261	-.210	-.155	-.135	-.155	-.199	-.213	-.213	-.196	-.180	-.163
.685 43 0	-.129	-.165	-.222	-.245	-.173	-.127	-.145	-.216	-.218	-.201	-.184	-.173	-.159
.824 71 0	-.043	-.053	-.139	-.164	-.122	-.063	-.108	-.124	-.093	-.065	-.029	.003	.034
.940 83 0	.110	.050	-.042	-.098	-.091	-.023	-.015	-.010	.022	.060	.102	.136	.160
1.027 83 0	.159	.129	.038	-.031	.010	.061	.079	.051	.079	.128	.169	.206	.219
1.161 71 0	.214	.179	.109	.064	.103	.137	.148	.140	.159	.200	.247	.277	.283
1.283 43 0	.213	.200	.164	.126	.178	.204	.203	.184	.202	.245	.305	.363	.442
1.432 31 0	.237	.224	.195	.190	.227	.237	.224	.239	.313	.213	-.002	-.027	.009

LOCAL FLOW FIELD DATA

+8 -1

MACH = 1.960 RE = 9.78X10 FT ALPHA = 20.250 X/D = 6.500 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 35 0	-.033	-.024	-.009	-.047	-.125	-.167	-.164	-.127	-.189	-.104	-.235	-.167	-.129
.633 99 0	-.065	-.063	-.062	-.026	-.083	-.120	-.146	-.174	-.186	-.179	-.210	-.215	-.179
.685 39 0	-.090	-.083	-.074	-.030	-.046	-.174	-.203	-.161	-.169	-.182	-.195	-.193	-.162
.765 103 0	-.145	-.112	-.096	-.048	-.057	-.132	-.165	-.139	-.140	-.171	-.174	-.149	-.110
.824 75 0	-.172	-.115	-.110	-.069	-.101	-.145	-.155	-.123	-.125	-.161	-.156	-.124	-.088
.904 107 0	-.073	-.050	-.102	-.084	-.132	-.151	-.141	-.094	-.134	-.160	-.134	-.093	-.060
.940 79 0	-.034	-.022	-.095	-.099	-.140	-.136	-.148	-.106	-.137	-.157	-.131	-.095	-.062
.999 111 0	.103	-.002	-.065	-.102	-.137	-.151	-.128	-.076	-.123	-.141	-.111	-.078	-.049
1.027 79 0	.081	-.084	-.084	-.115	-.119	-.127	-.114	-.067	-.072	-.123	-.092	-.070	-.047
1.161 75 0	.036	-.024	-.041	-.072	-.098	-.131	-.089	-.051	-.055	-.093	-.069	-.051	-.020
1.283 39 0	-.009	.003	-.048	-.071	-.105	-.114	-.084	-.047	-.047	-.089	-.061	-.042	-.015
1.432 35 0	-.043	-.027	-.067	-.079	-.075	-.076	-.073	-.032	-.029	-.070	-.044	-.020	-.012
1.538 99 0	-.078	-.058	-.081	-.076	-.081	-.090	-.060	-.050	-.067	-.049	-.036	-.019	-.004
1.680 103 0	-.092	-.079	-.076	-.067	-.061	-.060	-.052	-.039	-.061	-.054	-.038	-.016	-.004
1.798 107 0	-.106	-.083	-.077	-.057	-.053	-.064	-.059	-.067	-.057	-.056	-.045	-.020	.008
1.923 111 0	-.108	-.087	-.082	-.065	-.057	-.070	-.078	-.077	-.058	-.043	-.020	.008	.035

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.961 RE = 9.80x10 FT ALPHA = 20.250 X/D = 3.500 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 3 1	.929	.901	.874	.872	.832	.848	.399	.372	.355	.625	.932	.743	.783
.395 15 0	.817	.681	.393	.321	.519	.770	.601	.753	.951	.976	.957	.938	.960
.438 3 1 1.133	.962	.510	.218	.400	.726	.867	.972	.967	.962	.999	1.003	1.003	
.495 15 0 1.034	.745	.335	.265	.622	.995	1.054	1.008	.947	.949	.949	.981	1.017	
.564 19 1	.987	.970	.645	.480	.669	.922	1.008	1.007	.994	.990	.979	1.003	1.022
.685 55 0	.963	.966	.968	.958	.906	.903	.936	.959	.965	.942	.937	.948	.959
.824 59 0	.978	.975	.979	.975	.974	.970	.971	.971	.967	.931	.934	.947	.957
.940 95 0	.984	.982	.991	1.000	.998	1.007	1.014	1.021	1.003	.995	.998	1.008	1.017
1.027 95 0 1.003	.994	.991	.996	.999	1.002	1.003	.997	.987	.996	1.003	1.003	1.004	
1.161 59 0 1.014	1.003	1.002	1.007	.999	1.001	1.007	.984	.971	.994	.997	.998	1.000	
1.283 55 0 1.016	1.010	1.007	1.014	1.009	1.012	1.004	.993	.987	.994	1.002	1.003	1.001	
1.432 19 1	.997	1.005	1.002	.998	.994	1.001	1.000	.993	1.003	1.008	1.006	1.008	1.002

LOCAL FLOW FIELD DATA

MACH = 1.962 RE = 9.79X10 FT ALPHA = 20.250 X/D = 4.100 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 11 0	.590	.568	.522	.670	.813	.558	.406	.325	.351	.507	.900	1.072	.905
.438 7 0	.404	.416	.370	.362	.627	.635	.628	.506	.687	1.076	1.008	.893	.947
.495 11 0	.783	.585	.312	.381	.532	.744	.940	1.051	.977	.842	.707	.731	.834
.564 23 0	1.089	.816	.377	.389	.630	.879	.909	.914	.837	.787	.936	1.006	.990
.685 51 0	.981	.851	.723	.796	.754	.811	.920	.947	.953	.942	.943	.942	.948
.824 63 0	.962	.972	.966	.957	.963	.943	.942	.956	.965	.951	.931	.939	.961
.940 91 0	.965	.972	.986	.995	1.004	1.003	1.004	1.013	1.022	1.002	.984	.992	1.011
1.027 91 0	.982	.976	.982	.994	.993	.992	.990	.990	.996	.990	.985	1.011	1.003
1.161 63 0	1.007	.986	.992	1.001	.995	.994	1.005	.997	.984	.982	.998	.998	1.001
1.283 51 0	1.012	1.003	1.001	1.010	1.009	1.011	1.006	1.003	.984	.967	1.004	1.002	.995
1.432 23 0	.998	.997	.997	.994	.992	1.003	1.007	1.004	.997	1.001	1.004	1.001	1.004

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.956 RE = 9.81x10 FT ALPHA = 20.250 X/D = 4.400 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.364 27 1	.728	.659	.480	.396	.566	.468	.477	.701	1.007	1.061	1.018	1.014	1.003
.665 47 0	.993	.608	.388	.516	.700	.921	1.058	1.059	.989	.967	.946	.955	.964
.824 67 0	.869	.897	.808	.888	.983	.963	.972	.978	.974	.973	.889	.765	.734
.940 67 0	.826	.944	.999	1.001	1.003	.995	.935	.792	.785	.904	.970	.990	1.005
1.027 67 0	.990	.866	.834	.853	.808	.812	.879	.971	1.005	.997	.993	1.017	1.007
1.161 67 0	.993	.978	.986	.996	.991	.994	1.002	.992	.991	.991	.984	1.004	.998
1.283 47 0	1.002	.983	.988	.998	.997	1.003	1.004	1.002	.999	.998	1.001	1.001	1.005
1.432 27 1	1.000	.988	.992	.994	.987	.992	1.001	1.004	.991	.984	1.006	1.006	1.005

LOCAL FLOW FIELD DATA

+8 -1

MACH = 1.937 RE = 9.61X10 FT ALPHA = 20.250 X/D = 4.000 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.364 31 0	.828	.798	.696	.464	.529	.602	.703	.831	.825	.905	.842	.777	.809
.685 43 0	1.125	.847	.425	.311	.456	.474	.816	1.043	1.073	1.059	1.022	1.023	1.037
.824 71 0	1.053	.785	.421	.426	.526	.704	.982	1.057	1.027	1.027	1.026	1.009	.994
.940 83 0	1.023	.979	.757	.636	1.021	1.085	1.027	1.003	1.012	1.002	1.003	1.000	.999
1.027 83 0	.991	1.002	1.010	1.029	1.043	1.022	.996	1.008	1.002	1.000	.991	.995	.982
1.161 71 0	.977	.997	1.001	1.034	1.032	1.022	1.018	1.021	1.014	1.002	.987	.982	.990
1.283 43 0	.981	.977	.961	1.015	1.009	.996	.995	1.006	1.008	.996	.957	.860	.691
1.432 31 0	.995	.997	.975	1.001	1.001	.994	.996	.989	.874	.817	.949	1.016	.980

LOCAL FLOW FIELD DATA

MACH = 1.960 RE = 9.78X10 FT ALPHA = 20.250 X/D = 6.500 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 35 0	.671	.659	.534	.495	.594	.584	.545	.279	.145	1.519	1.406	.715	.721
.633 99 0	.673	.718	.658	.546	.544	.313	.390	.714	.874	.847	.890	.988	1.012
.685 39 0	.817	.723	.612	.570	.769	.794	.844	.861	.873	.834	.883	.956	.961
.765 103 0	.828	.578	.410	.553	.825	.865	.888	.925	.898	.883	.931	.955	.940
.824 75 0	.910	.559	.303	.625	.886	.896	.905	.925	.852	.872	.913	.912	.905
.904 107 0	.902	.516	.285	.697	.910	.908	.926	.937	.879	.917	.952	.939	.935
.940 79 0	.973	.564	.330	.729	.912	.923	.954	.965	.895	.912	.941	.936	.941
.999 111 0	.810	.570	.548	.801	.861	.901	.939	.936	.916	.926	.942	.943	.949
1.027 79 0	.933	.469	.517	.821	.879	.887	.931	.933	.927	.916	.934	.949	.951
1.161 75 0	.976	.652	.635	.839	.879	.930	.940	.938	.932	.932	.946	.957	.961
1.283 39 0	.933	.902	.824	.887	.905	.925	.952	.916	.870	.956	.958	.968	.980
1.432 35 0	.934	.933	.950	.949	.920	.899	.954	.916	.870	.962	.971	.978	.988
1.538 99 0	.935	.947	.971	.971	.958	.937	.962	.958	.948	.961	.972	.978	.980
1.680 103 0	.940	.953	.969	.984	.962	.933	.967	.953	.959	.971	.972	.969	.983
1.798 107 0	.949	.956	.966	.977	.966	.959	.967	.949	.959	.972	.986	.999	1.018
1.923 111 0	.959	.964	.970	.982	.977	.946	.950	.977	.970	.992	.997	.998	1.007

LOCAL FLOW FIELD DATA

MACH = 1.961 RE = 9.80x10⁶ FT ALPHA = 20.250 X/D = 3.500 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 3 1	-.152	-.126	-.047	.086	.225	.234	.024	-.032	.093	.111	.155	.202	.143
.395 15 0	-.410	-.369	-.209	.100	.297	.240	.150	.208	.251	.197	.146	.092	.033
.438 3 1	-.413	-.420	-.310	-.090	.249	.389	.341	.305	.263	.214	.166	.120	.073
.495 15 0	-.257	-.292	-.111	.205	.414	.443	.376	.302	.247	.206	.153	.103	.065
.564 19 1	-.129	-.172	-.071	.179	.367	.399	.354	.295	.241	.195	.138	.086	.049
.665 55 0	.099	.109	.144	.211	.252	.277	.282	.259	.221	.179	.125	.082	.047
.824 59 0	.216	.218	.233	.249	.259	.265	.262	.243	.214	.168	.125	.087	.043
.940 95 0	.257	.264	.266	.270	.270	.263	.252	.236	.208	.161	.121	.082	.038
1.027 95 0	.267	.268	.269	.264	.257	.244	.225	.205	.170	.127	.097	.065	.026
1.161 59 0	.284	.288	.285	.278	.267	.251	.233	.204	.167	.134	.100	.064	.028
1.283 55 0	.302	.295	.291	.284	.270	.251	.228	.195	.155	.126	.096	.060	.029
1.432 19 1	.321	.310	.304	.298	.288	.264	.234	.200	.160	.125	.096	.062	.022

LOCAL FLOW FIELD DATA

MACH = 1.962 RE = 9.79x10⁶ FT ALPHA = 20.250 X/D = 4.100 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 11 0	.127	.122	.201	.383	.372	.252	.245	.261	.231	.074	.169	.331	.253
.438 7 0	.060	.002	.075	.239	.465	.464	.354	.217	.197	.349	.389	.291	.173
.495 11 0	-.325	-.312	.008	.305	.395	.461	.489	.482	.451	.381	.293	.198	.126
.564 23 0	-.341	-.350	.020	.353	.453	.479	.453	.424	.342	.246	.150	.094	.063
.685 51 0	-.084	-.097	.092	.283	.348	.359	.325	.273	.226	.183	.141	.096	.050
.824 63 0	.141	.156	.204	.252	.276	.283	.276	.252	.218	.185	.143	.092	.042
.940 91 0	.215	.224	.246	.265	.271	.266	.259	.240	.209	.178	.137	.086	.036
1.027 91 0	.244	.250	.255	.257	.253	.242	.228	.208	.182	.146	.104	.065	.026
1.161 63 0	.267	.276	.277	.272	.264	.250	.232	.209	.186	.151	.100	.066	.027
1.283 51 0	.288	.287	.286	.280	.266	.246	.227	.205	.174	.133	.096	.060	.027
1.432 23 0	.310	.304	.300	.297	.289	.267	.243	.222	.184	.134	.105	.070	.033

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.956 RE = 9.61x10 FT ALPHA = 20.250 X/D = 4.400 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	160.00	172.50	185.00	197.50	210.00	222.50	235.00	247.50	260.00	272.50	285.00	297.50	310.00
R/D RUN NO.													
.564 27 1	-.061	.028	.304	.463	.504	.405	.414	.407	.387	.372	.348	.322	.292
.683 47 0	-.091	-.085	.183	.414	.493	.513	.491	.438	.392	.357	.325	.297	.268
.824 67 0	.156	.174	.288	.404	.439	.431	.424	.403	.370	.350	.259	.205	.177
.940 87 0	.237	.275	.336	.387	.409	.399	.397	.350	.286	.218	.149	.093	.044
1.027 87 0	.219	.291	.369	.385	.376	.328	.284	.222	.184	.152	.114	.063	.029
1.161 67 0	.260	.268	.273	.272	.264	.250	.232	.210	.187	.153	.105	.066	.028
1.283 47 0	.280	.283	.280	.275	.263	.247	.228	.201	.174	.138	.090	.055	.021
1.432 27 1	.304	.299	.298	.297	.287	.268	.246	.225	.195	.152	.109	.074	.035

LOCAL FLOW FIELD DATA

MACH = 1.957 $Re = 9.81 \times 10^6$ FT $\alpha = 20.250$ $X/D = 4.800$ TEST NO. = 35

RADIAL VELOCITY RATIO -- (V_R / V_{INF}) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 31 0	-.204	-.157	-.082	.104	.148	.050	.046	.109	.099	.085	.079	.063	.048
.685 43 0	-.221	-.189	-.076	.088	.208	.212	.227	.184	.136	.116	.090	.074	.056
.824 71 0	-.108	-.084	.033	.275	.329	.318	.329	.305	.267	.237	.210	.183	.157
.940 83 0	.135	.126	.196	.297	.347	.361	.350	.334	.309	.281	.256	.226	.197
1.027 83 0	.227	.235	.267	.304	.339	.336	.327	.320	.294	.270	.247	.216	.177
1.161 71 0	.302	.317	.322	.342	.355	.356	.346	.331	.311	.286	.259	.231	.193
1.283 43 0	.341	.353	.350	.356	.362	.358	.351	.328	.307	.285	.260	.224	.159
1.432 31 0	.387	.377	.367	.373	.374	.364	.345	.330	.304	.222	.116	.051	.028

LOCAL FLOW FIELD DATA

MACH = 1.960 RE = 9.76x10⁶ FT ALPHA = 20.250 X/D = 6.500 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/O RUN NO.													
.564 35 0	-.047	-.025	.066	-.028	-.129	-.016	.168	.138	.077	.054	.126	.118	.054
.633 99 0	-.049	-.020	.096	.052	-.114	-.006	.148	.218	.210	.165	.101	.064	.050
.685 39 0	-.134	-.070	.083	.095	.053	.083	.170	.205	.193	.157	.099	.066	.051
.765 103 0	-.226	-.169	.121	.289	.250	.199	.187	.191	.192	.142	.104	.083	.059
.824 75 0	-.300	-.206	.161	.357	.310	.230	.203	.199	.191	.142	.100	.076	.052
.904 107 0	-.218	-.123	.213	.411	.352	.258	.222	.207	.176	.145	.118	.089	.060
.940 79 0	-.209	-.129	.198	.389	.349	.267	.229	.213	.173	.140	.113	.085	.055
.999 111 0	-.040	-.005	.228	.364	.326	.263	.228	.205	.169	.141	.115	.085	.056
1.027 79 0	-.054	-.066	.222	.365	.317	.254	.212	.189	.158	.119	.093	.065	.038
1.161 75 0	.020	.062	.262	.309	.284	.256	.227	.204	.175	.135	.112	.084	.049
1.283 39 0	.088	.120	.201	.276	.251	.246	.225	.201	.169	.129	.103	.075	.041
1.432 35 0	.168	.176	.209	.241	.247	.243	.234	.207	.170	.141	.114	.083	.057
1.538 99 0	.175	.201	.215	.235	.242	.237	.227	.199	.156	.135	.108	.075	.042
1.660 103 0	.198	.216	.236	.250	.253	.241	.233	.209	.165	.141	.109	.071	.022
1.798 107 0	.211	.232	.247	.259	.259	.243	.219	.180	.162	.132	.100	.069	.040
1.923 111 0	.226	.236	.250	.255	.251	.231	.202	.168	.149	.124	.101	.076	.051

LOCAL FLOW FIELD DATA

MACH = 1.961 RE = 9.80x10 FT ALPHA = 20.250 X/D = 3.500 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (V_{THETA}/V_{INF})

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 3 1	.000	-.109	-.198	-.248	-.182	-.139	-.135	.014	.239	.507	.526	.462	.497
.395 15 0	.000	-.170	-.195	-.157	.007	.082	.203	.414	.466	.487	.486	.500	.524
.438 3 1	.000	-.084	-.190	-.108	.180	.248	.329	.378	.391	.443	.471	.477	.480
.495 15 0	.000	-.018	.043	.307	.434	.426	.394	.372	.400	.426	.452	.468	.452
.564 19 1	.000	.078	.227	.332	.428	.437	.397	.379	.374	.414	.459	.468	.449
.685 55 0	-.000	.097	.223	.300	.357	.392	.391	.380	.378	.403	.443	.440	.411
.824 59 0	-.000	.079	.153	.214	.266	.304	.330	.344	.357	.396	.418	.407	.389
.940 95 0	-.000	.071	.136	.186	.231	.272	.299	.319	.339	.383	.400	.392	.379
1.027 95 0	.000	.058	.120	.180	.226	.269	.299	.321	.365	.401	.392	.383	.372
1.161 59 0	-.000	.054	.110	.162	.208	.253	.283	.308	.349	.377	.369	.361	.350
1.283 55 0	.000	.055	.105	.158	.202	.243	.277	.310	.348	.366	.366	.355	.351
1.432 19 1	.000	.060	.102	.154	.201	.246	.280	.317	.350	.359	.360	.354	.343

LOCAL FLOW FIELD DATA

MACH = 1.962 RE = 9.79x10 FT ALPHA = 20.250 X/D = 4.100 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 11 0	.000	-.072	-.148	-.102	-.073	-.070	.038	.172	.275	.415	.513	.425	.441
.438 7 0	.000	.006	-.100	.009	.072	.139	.204	.301	.418	.429	.375	.322	.354
.495 11 0	.000	-.058	.070	.213	.319	.389	.372	.361	.313	.300	.313	.384	.439
.564 23 0	.000	-.079	.106	.280	.369	.416	.390	.354	.328	.359	.436	.459	.444
.685 51 0	-.000	.119	.280	.318	.373	.414	.401	.390	.387	.393	.418	.429	.418
.824 63 0	-.000	.109	.209	.260	.292	.332	.359	.372	.376	.369	.399	.415	.400
.940 91 0	-.000	.079	.156	.213	.256	.290	.321	.346	.358	.359	.388	.402	.387
1.027 91 0	.000	.074	.142	.197	.244	.293	.324	.346	.360	.377	.403	.396	.375
1.161 63 0	-.000	.059	.118	.173	.219	.268	.298	.317	.335	.359	.385	.371	.358
1.283 51 0	.000	.060	.112	.167	.214	.257	.291	.312	.333	.367	.378	.365	.359
1.432 23 0	-.000	.049	.099	.152	.201	.249	.279	.302	.335	.369	.370	.361	.352

LOCAL FLOW FIELD DATA

MACH = 1.956 $RE = 9.81 \times 10^6$ FT $\alpha = 20.250$ $X/D = 4.400$ TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (V_{θ}/V_{∞})

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 27 1	-.000	-.249	-.316	-.156	-.053	.019	.170	.346	.385	.391	.432	.453	.452
.685 47 0	-.000	.043	.207	.256	.289	.346	.366	.356	.357	.358	.361	.382	.392
.824 67 0	-.000	.180	.278	.285	.280	.315	.350	.352	.350	.346	.305	.306	.343
.940 87 0	-.000	.164	.211	.230	.241	.272	.322	.296	.304	.340	.379	.401	.393
1.027 87 0	.000	.110	.166	.187	.196	.263	.321	.358	.371	.374	.392	.409	.371
1.161 67 0	.000	.062	.123	.178	.223	.275	.307	.328	.344	.362	.382	.379	.360
1.283 47 0	.000	.055	.111	.166	.213	.259	.294	.318	.334	.360	.383	.370	.361
1.432 27 1	-.000	.045	.101	.153	.204	.249	.283	.308	.330	.355	.376	.365	.357

LOCAL FLOW FIELD DATA

MACH = 1.957 $RE = 9.81 \times 10^6$ FT $\alpha = 20.250$ $X/D = 4.800$ TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (V_{THETA}/V_{INF})

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 31 0	.000	-.197	-.422	-.398	-.238	-.082	.189	.364	.449	.472	.472	.478	.470
.685 43 0	.000	-.205	-.374	-.347	-.162	.020	.190	.347	.412	.425	.428	.435	.434
.824 71 0	.000	-.024	.059	.215	.225	.262	.325	.353	.378	.393	.393	.395	.392
.940 83 0	-.000	.101	.232	.315	.316	.286	.317	.345	.356	.361	.365	.370	.368
1.027 83 0	-.000	.105	.212	.299	.290	.286	.308	.356	.367	.369	.370	.374	.388
1.161 71 0	-.000	.076	.161	.235	.242	.258	.289	.327	.341	.340	.341	.350	.360
1.283 43 0	-.000	.073	.144	.207	.224	.246	.280	.320	.335	.332	.338	.347	.277
1.432 31 0	.000	.069	.131	.181	.205	.233	.269	.304	.303	.316	.376	.375	.361

LOCAL FLOW FIELD DATA

MACH = 1.960 RE = 9.76X10 FT ALPHA = 20.250 X/D = 6.500 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.364 35 0	.000	-.045	.004	.044	-.116	-.249	-.148	-.006	.289	.608	.664	.601	.565
.633 99 0	.000	-.075	-.126	-.046	.051	.255	.520	.556	.537	.549	.602	.615	.578
.685 39 0	-.000	-.123	-.166	-.033	.199	.445	.551	.491	.495	.535	.570	.571	.538
.765 103 0	-.000	-.131	-.132	.071	.253	.407	.482	.465	.482	.545	.562	.539	.510
.824 75 0	.000	-.123	-.041	.151	.261	.389	.447	.431	.454	.520	.527	.503	.478
.904 107 0	.000	-.058	.121	.271	.316	.391	.420	.396	.472	.519	.502	.481	.459
.940 79 0	-.000	-.009	.166	.273	.299	.371	.405	.384	.455	.502	.486	.463	.439
.999 111 0	-.000	.111	.277	.319	.341	.389	.397	.373	.454	.495	.476	.456	.438
1.027 79 0	.000	.081	.244	.297	.325	.376	.391	.369	.406	.495	.470	.444	.415
1.161 75 0	-.000	.152	.233	.271	.311	.374	.358	.339	.375	.452	.430	.411	.388
1.283 39 0	.000	.183	.267	.274	.314	.359	.352	.337	.365	.432	.413	.402	.383
1.432 35 0	-.000	.119	.215	.253	.279	.313	.338	.328	.353	.409	.398	.386	.376
1.538 99 0	.000	.113	.186	.229	.266	.311	.316	.338	.385	.387	.382	.369	.363
1.680 103 0	.000	.091	.157	.202	.238	.284	.301	.322	.366	.373	.371	.365	.354
1.798 107 0	.000	.073	.131	.178	.222	.280	.298	.326	.345	.359	.361	.356	.349
1.923 111 0	-.000	.062	.118	.164	.210	.270	.298	.318	.338	.359	.357	.351	.348

LOCAL FLOW FIELD DATA

MACH = 1.961 RE = 9.80x10 FT ALPHA = 20.250 X/D = 3.500 TEST NO. = 35

(VC / VINP * SIN ALPHAINP)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 3 1	.441	.481	.588	.758	.838	.786	.397	.099	.742	1.499	1.585	1.458	1.496
.395 15 0	1.186	1.175	.826	.538	.859	.732	.728	1.339	1.528	1.518	1.467	1.469	1.517
.458 3 1	1.193	1.236	1.049	.407	.886	1.333	1.367	1.405	1.362	1.421	1.443	1.420	1.402
.495 15 0	.743	.844	.343	1.066	1.733	1.775	1.572	1.383	1.358	1.366	1.379	1.384	1.319
.584 19 1	.372	.546	.686	1.088	1.628	1.709	1.536	1.388	1.286	1.323	1.384	1.376	1.304
.685 55 0	.287	.424	.767	1.060	1.264	1.587	1.392	1.329	1.265	1.274	1.330	1.292	1.196
.824 59 0	.623	.671	.805	.948	1.073	1.165	1.219	1.217	1.203	1.243	1.261	1.203	1.131
.940 95 0	.743	.789	.863	.947	1.028	1.095	1.130	1.147	1.151	1.200	1.209	1.157	1.100
1.027 95 0	.771	.793	.851	.923	.989	1.049	1.082	1.101	1.164	1.216	1.166	1.123	1.077
1.161 59 0	.820	.845	.882	.929	.977	1.030	1.059	1.067	1.119	1.155	1.106	1.059	1.014
1.283 55 0	.872	.866	.895	.941	.976	1.008	1.037	1.059	1.100	1.119	1.094	1.040	1.018
1.432 19 1	.927	.913	.926	.969	1.016	1.043	1.054	1.081	1.111	1.098	1.076	1.039	.992

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.962 RE = 9.79X10 FT ALPHA = 20.250 X/D = 4.100 TEST NO. = 35

(VC / VINP * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 11 0	.366	.410	.721	1.146	1.095	.755	.715	.904	1.038	1.219	1.562	1.556	1.469
.436 7 0	.173	.018	.360	.691	1.359	1.399	1.180	1.071	1.334	1.598	1.561	1.254	1.139
.495 11 0	.938	.918	.205	1.075	1.465	1.744	1.777	1.740	1.586	1.401	1.239	1.249	1.321
.564 23 0	.986	1.037	.311	1.302	1.688	1.834	1.725	1.597	1.369	1.258	1.333	1.354	1.296
.685 51 0	.243	.444	.851	1.230	1.475	1.584	1.491	1.376	1.295	1.253	1.276	1.271	1.218
.824 63 0	.408	.548	.844	1.046	1.161	1.260	1.309	1.297	1.255	1.193	1.224	1.228	1.161
.940 91 0	.621	.686	.841	.982	1.076	1.137	1.192	1.216	1.197	1.158	1.189	1.186	1.123
1.027 91 0	.704	.753	.843	.935	1.015	1.096	1.145	1.167	1.165	1.168	1.203	1.159	1.086
1.161 63 0	.772	.815	.870	.932	.990	1.058	1.091	1.097	1.106	1.125	1.148	1.088	1.037
1.283 51 0	.833	.847	.886	.943	.985	1.027	1.067	1.078	1.085	1.127	1.127	1.069	1.041
1.432 23 0	.896	.890	.911	.965	1.017	1.053	1.068	1.083	1.105	1.133	1.110	1.063	1.022

LOCAL FLOW FIELD DATA

MACH = 1.958 RE = 9.81x10 FT ALPHA = 20.250 X/D = 4.400 TEST NO. = 35

(VC / VINF * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 27 1	.175	.723	1.267	1.413	1.465	1.172	1.292	1.544	1.577	1.557	1.603	1.606	1.554
.685 47 0	.263	.275	.799	1.406	1.652	1.789	1.769	1.632	1.532	1.461	1.405	1.399	1.371
.824 67 0	.451	.723	1.158	1.429	1.504	1.541	1.588	1.546	1.471	1.422	1.156	1.064	1.116
.940 87 0	.685	.925	1.145	1.299	1.372	1.394	1.476	1.325	1.206	1.168	1.177	1.189	1.143
1.027 87 0	.632	.899	1.169	1.236	1.224	1.217	1.238	1.217	1.196	1.168	1.178	1.195	1.076
1.161 67 0	.751	.794	.865	.940	.998	1.074	1.111	1.125	1.131	1.134	1.145	1.113	1.044
1.283 47 0	.809	.833	.870	.927	.977	1.034	1.074	1.085	1.087	1.113	1.136	1.081	1.046
1.432 27 1	.878	.875	.911	.965	1.018	1.057	1.084	1.100	1.107	1.116	1.131	1.075	1.037

LOCAL FLOW FIELD DATA

MACH = 1.957 RE = 9.81X10⁶ FT ALPHA = 20.250 X/D = 4.800 TEST NO. = 35

(VC / VINF * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 31 0	.588	.728	1.243	1.187	.809	.277	.563	1.099	1.328	1.385	1.382	1.393	1.366
.685 43 0	.640	.807	1.103	1.034	.761	.616	.856	1.134	1.253	1.273	1.263	1.274	1.264
.824 71 0	.313	.252	.195	1.007	1.153	1.190	1.336	1.348	1.338	1.327	1.289	1.258	1.221
.940 83 0	.389	.467	.879	1.249	1.355	1.331	1.363	1.389	1.362	1.323	1.289	1.254	1.204
1.027 83 0	.655	.745	.986	1.232	1.289	1.274	1.296	1.383	1.359	1.321	1.285	1.247	1.231
1.161 71 0	.673	.943	1.041	1.198	1.241	1.269	1.303	1.344	1.334	1.284	1.239	1.212	1.179
1.283 43 0	.986	1.041	1.095	1.191	1.229	1.255	1.297	1.324	1.312	1.265	1.232	1.193	.923
1.432 31 0	1.119	1.106	1.127	1.198	1.232	1.249	1.263	1.296	1.240	1.115	1.136	1.093	1.047

LOCAL FLOW FIELD DATA

MACH = 1.960 RE = 9.78x10 FT ALPHA = 20.250 X/D = 6.500 TEST NO. = 35

(VC / VINP * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 35 0	.136	.149	.192	.150	.302	.720	.647	.399	.863	1.764	1.953	1.768	1.641
.633 99 0	.142	.223	.459	.202	.362	.738	1.560	1.725	1.667	1.657	1.764	1.786	1.676
.665 39 0	.387	.409	.536	.290	.593	1.307	1.667	1.537	1.535	1.609	1.673	1.662	1.561
.765 103 0	.654	.619	.518	.861	1.027	1.310	1.494	1.453	1.499	1.628	1.652	1.575	1.484
.824 75 0	.867	.693	.480	1.119	1.171	1.305	1.419	1.370	1.424	1.558	1.551	1.469	1.388
.904 107 0	.629	.394	.708	1.422	1.369	1.355	1.373	1.291	1.455	1.557	1.490	1.412	1.338
.940 79 0	.605	.374	.747	1.375	1.326	1.320	1.344	1.270	1.406	1.505	1.443	1.359	1.279
.999 111 0	.117	.322	1.036	1.399	1.363	1.357	1.323	1.230	1.400	1.487	1.414	1.341	1.277
1.027 79 0	.157	.300	.952	1.359	1.311	1.310	1.285	1.199	1.259	1.471	1.385	1.296	1.205
1.161 75 0	.039	.475	1.013	1.189	1.216	1.308	1.225	1.142	1.195	1.363	1.284	1.211	1.130
1.263 39 0	.254	.631	.965	1.122	1.161	1.258	1.206	1.133	1.161	1.301	1.230	1.181	1.112
1.432 35 0	.485	.613	.867	1.010	1.076	1.145	1.188	1.120	1.131	1.249	1.195	1.140	1.100
1.538 99 0	.506	.666	.821	.948	1.039	1.130	1.126	1.133	1.199	1.184	1.147	1.089	1.056
1.680 103 0	.573	.677	.819	.930	1.005	1.075	1.100	1.108	1.158	1.151	1.117	1.073	1.025
1.798 107 0	.608	.702	.809	.907	.986	1.072	1.067	1.077	1.102	1.105	1.083	1.049	1.014
1.923 111 0	.654	.705	.798	.876	.945	1.027	1.039	1.039	1.066	1.097	1.072	1.039	1.017

LOCAL FLOW FIELD DATA

MACH = 1.961 RE = 9.60x10 FT ALPHA = 20.250 X/D = 3.500 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 3 1	1.059	1.056	1.043	1.037	.993	.896	.831	.833	.718	.708	.696	.760	.793
.395 15 0	1.060	1.019	.918	.903	.921	.981	.891	.879	.927	.932	.928	.925	.930
.436 3 1	1.085	1.065	.991	.897	.886	.946	.931	.925	.926	.929	.939	.940	.938
.495 15 0	1.051	.999	.901	.780	.845	.931	.935	.927	.920	.925	.923	.929	.936
.564 19 1	1.015	1.025	.970	.891	.890	.926	.936	.934	.931	.937	.941	.949	.950
.685 55 0	.978	.977	.964	.938	.914	.906	.909	.914	.918	.918	.920	.923	.922
.824 59 0	.980	.938	.950	.937	.935	.932	.928	.924	.921	.919	.920	.917	.917
.940 95 0	.952	.947	.944	.945	.942	.943	.943	.943	.938	.943	.938	.937	.940
1.027 95 0	.962	.956	.954	.949	.944	.943	.939	.931	.929	.938	.939	.937	.928
1.161 59 0	.960	.952	.955	.950	.939	.939	.939	.929	.930	.938	.936	.936	.932
1.283 55 0	.957	.952	.955	.951	.939	.941	.939	.936	.940	.938	.935	.934	.929
1.432 19 1	.944	.943	.944	.937	.927	.930	.934	.937	.943	.943	.938	.935	.931

LOCAL FLOW FIELD DATA

MACH = 1.962 RE = 9.79X10 FT ALPHA = 20.250 X/D = 4.100 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 11 0	.524	.508	.383	.459	.839	.828	.635	.312	.259	.475	.795	.699	.635
.438 7 0	.409	.412	.398	.367	.572	.669	.798	.811	.865	.850	.683	.398	.233
.495 11 0	1.020	.953	.566	.422	.481	.613	.682	.721	.692	.647	.631	.743	.844
.564 23 0	1.073	1.035	.754	.610	.652	.724	.710	.707	.739	.800	.913	.953	.939
.685 51 0	1.001	.972	.915	.891	.835	.841	.895	.915	.919	.919	.919	.918	.920
.824 63 0	.962	.963	.944	.930	.930	.926	.922	.924	.924	.919	.913	.915	.919
.940 91 0	.952	.951	.948	.944	.945	.948	.950	.952	.949	.941	.939	.938	.937
1.027 91 0	.960	.953	.952	.949	.944	.943	.938	.933	.930	.927	.930	.937	.933
1.161 63 0	.958	.948	.952	.948	.939	.942	.943	.933	.922	.924	.938	.936	.934
1.283 51 0	.958	.950	.953	.950	.943	.946	.943	.932	.926	.929	.937	.934	.932
1.432 23 0	.946	.941	.943	.938	.929	.933	.934	.930	.931	.941	.940	.935	.935

LOCAL FLOW FIELD DATA

MACH = 1.956 RE = 9.81X10⁶ FT ALPHA = 20.250 X/D = 4.400 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 27 1	.815	.722	.542	.472	.643	.607	.251	.506	.793	.771	.734	.723	.714
.685 47 0	.681	.637	.748	.667	.669	.732	.781	.780	.742	.728	.708	.703	.698
.624 67 0	.609	.644	.771	.727	.733	.737	.744	.739	.731	.741	.476	.494	.685
.940 67 0	.632	.641	.811	.783	.767	.777	.723	.670	.733	.858	.927	.935	.932
1.027 67 0	.972	.832	.684	.667	.666	.765	.837	.921	.934	.925	.927	.941	.937
1.161 67 0	.955	.946	.950	.946	.938	.943	.944	.933	.925	.926	.932	.939	.934
1.283 47 0	.956	.944	.949	.948	.942	.946	.945	.938	.933	.937	.942	.936	.937
1.432 27 1	.952	.941	.944	.939	.933	.933	.933	.931	.925	.929	.941	.935	.938

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.937 RE = 9.81x10 FT ALPHA = 20.250 X/D = 4.800 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 31 0	1.088	1.080	1.047	.919	.941	.985	1.011	1.028	1.006	1.011	.984	.955	.951
.685 43 0	1.068	1.032	.934	.917	.933	.910	1.006	1.070	1.060	1.040	1.023	1.013	1.006
.824 71 0	1.026	.979	.915	.876	.864	.876	.949	.971	.948	.932	.917	.900	.886
.940 83 0	.944	.958	.920	.927	.942	.917	.895	.883	.872	.857	.842	.831	.828
1.027 83 0	.898	.905	.922	.928	.898	.870	.850	.852	.840	.823	.807	.798	.791
1.181 71 0	.847	.859	.878	.884	.857	.833	.820	.817	.808	.796	.779	.769	.775
1.283 43 0	.834	.831	.834	.850	.818	.798	.790	.796	.791	.778	.746	.684	.627
1.432 31 0	.807	.815	.819	.816	.793	.783	.787	.772	.713	.761	.910	.943	.923

LOCAL FLOW FIELD DATA

MACH = 1.960 RE = 9.76x10 FT ALPHA = 20.250 X/D = 6.500 TEST NO. = 35

AXIAL VELOCITY RATIO -- (VX / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 35 0	.937	.928	.866	.875	.962	.891	.870	.787	.609	.908	.980	.848	.844
.633 99 0	.959	.969	.940	.884	.921	.780	.731	.865	.928	.918	.932	.948	.943
.685 39 0	1.005	.976	.929	.894	.952	.966	.939	.929	.939	.927	.935	.949	.944
.765 103 0	1.029	.938	.849	.855	.929	.948	.946	.940	.927	.923	.931	.930	.916
.824 75 0	1.046	.927	.780	.864	.953	.964	.956	.943	.920	.927	.933	.923	.911
.904 107 0	.999	.880	.730	.847	.948	.964	.956	.940	.927	.936	.935	.918	.908
.940 79 0	.992	.882	.764	.877	.961	.976	.972	.956	.941	.943	.939	.928	.921
.999 111 0	.905	.874	.839	.897	.942	.962	.958	.937	.936	.936	.930	.921	.915
1.027 79 0	.946	.885	.854	.918	.941	.949	.953	.936	.927	.923	.921	.925	.926
1.161 75 0	.977	.910	.863	.920	.941	.961	.947	.935	.928	.925	.926	.928	.924
1.283 39 0	.988	.955	.931	.940	.960	.956	.949	.929	.914	.938	.932	.930	.927
1.432 35 0	.996	.978	.982	.972	.956	.942	.945	.922	.908	.936	.930	.926	.929
1.538 99 0	1.015	.994	.999	.982	.972	.961	.948	.940	.939	.932	.933	.932	.929
1.680 103 0	1.020	1.007	.995	.981	.964	.949	.947	.936	.943	.942	.938	.931	.934
1.798 107 0	1.028	1.008	.997	.977	.962	.957	.956	.957	.949	.950	.949	.942	.935
1.923 111 0	1.027	1.012	1.001	.986	.972	.964	.968	.973	.957	.948	.939	.929	.919

LOCAL VORTICITY X 100.

MACH = 1.961 RE = 9.80x10 FT ALPHA = 20.250 X/D = 3.500 TEST NO. = 35

THETA	178.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.3550	3.738	43.230	119.637	124.181	46.908	6.709	124.802	163.015	52.469	24.113	32.630	13.111
.4165	29.170	78.975	127.233	186.197	125.521	66.200	51.398	-7.189	-31.155	-11.560	-5.005	-14.411
.4865	4.718	121.742	252.123	269.837	146.617	48.365	10.155	1.187	1.685	-4.636	-.673	-.166
.5295	4.044	105.464	150.382	92.678	32.115	1.852	-3.866	-4.858	-3.409	.095	4.634	7.577
.6245	-1.310	28.624	55.573	38.771	12.970	4.836	2.468	1.535	1.522	-2.595	-.948	-.220
.7545	1.437	2.858	3.735	.044	-1.252	-1.385	-2.026	-1.642	-.755	-1.538	-1.205	-1.308
.8820	1.152	2.232	2.059	.632	.386	.258	-.678	-1.151	-2.925	-1.058	-.417	-1.081
.9835	-.230	-1.311	.721	2.934	3.061	3.871	4.562	6.483	7.019	4.601	.447	-.569
1.0940	.703	.430	-.401	-.457	-.255	.051	-.201	-1.308	-1.868	-1.163	-1.526	-2.371
1.2220	.398	.839	.833	.819	.360	.689	.858	.769	1.279	1.248	.841	1.497
1.3575	-.305	.943	.791	1.114	1.192	1.555	1.464	1.186	1.575	1.386	1.059	.641

LOCAL VORTICITY X 100.

MACH = 1.962 RE = 9.79x10 FT ALPHA = 20.250 X/D = 4.100 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.4165	7.438	66.798	120.378	122.157	76.441	86.769	68.607	84.881	67.477	20.735	-30.870	-76.891
.4665	-24.025	102.661	179.112	171.713	134.793	89.910	37.144	-1.557	-14.783	-32.781	-20.676	13.470
.5295	-4.664	127.695	139.993	69.168	48.374	26.849	12.877	-3.014	-1.109	16.336	27.512	16.153
.6245	17.575	128.152	111.977	43.039	21.598	7.855	8.028	4.727	3.252	-3.360	-2.980	.014
.7545	1.116	28.709	27.508	9.179	-.777	-3.879	-2.413	-.318	-.181	-1.464	-1.457	-1.315
.8820	.687	2.559	2.279	1.487	.028	-.960	-1.693	-1.431	.370	-.625	-2.295	-2.237
.9835	1.810	2.736	2.030	1.873	4.094	6.677	5.209	3.835	5.636	6.341	2.578	-1.253
1.0940	.676	-.800	-1.097	-.951	-1.040	-.778	-1.662	-1.527	-2.045	-2.756	-1.554	-2.252
1.2220	1.336	1.329	.984	1.091	.645	1.159	1.481	1.675	1.856	.826	.963	1.335
1.3575	-.978	-.983	-.478	-.615	-.478	.194	.506	.408	.394	1.642	.800	.738

LOCAL VORTICITY X 100.

MACH = 1.956 RE = 9.81x10⁶ FT ALPHA = 20.250 X/D = 4.400 TEST NO. = 35

THETA 176.25 168.75 161.25 153.75 146.25 138.75 131.25 123.75 116.25 108.75 101.25 93.75

R/D

.6245	42.446	164.327	156.294	99.722	62.982	60.933	24.799	2.349	1.038	-3.557	-6.524	-5.852
.7545	17.149	72.942	61.323	25.548	8.046	3.341	.650	.633	3.021	-10.279	-11.124	-6.616
.8620	6.785	15.968	11.880	3.336	-3.024	.419	-7.016	-12.264	-5.644	-.200	16.061	17.519
.9635	4.648	3.411	-1.098	-5.912	-7.141	1.671	6.449	16.979	13.733	5.757	2.674	-.127
1.0940	3.504	1.448	.238	4.598	3.776	.966	-3.959	-2.651	-1.228	-1.015	-2.469	-1.408
1.2220	.672	-.044	.087	.066	-.074	.019	.084	.784	.410	.021	1.122	1.021
1.3575	-.448	-.522	.135	.142	.179	.348	.326	.827	.042	-.519	.995	.687

LOCAL VORTICITY X 100.

MACH = 1.957 RE = 9.81X10 FT ALPHA = 20.250 X/D = 4.800 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.6245	7.278	20.762	48.306	26.602	-.478	15.535	12.114	1.290	3.614	3.694	4.212	4.857
.7545	21.645	79.879	137.048	106.855	58.589	43.809	14.273	-.894	1.008	.934	1.530	.812
.8620	15.736	54.970	72.317	39.446	20.338	10.006	3.440	.082	-1.608	-1.384	-1.122	-.615
.9635	1.965	11.739	14.963	10.137	4.883	4.331	6.552	7.337	6.875	6.369	4.756	6.258
1.0940	.356	-1.174	-.782	-.149	-1.247	.521	.835	-1.123	-1.237	-1.587	-1.849	-3.106
1.2220	2.585	.635	1.285	1.492	1.659	2.077	1.606	2.240	1.805	1.749	1.189	-9.999
1.3575	.349	-.353	.530	.363	.545	.878	.460	-1.554	-5.438	-1.135	4.932	9.532

LOCAL VORTICITY X 100.

MACH = 1.960 RE = 9.78X10 FT ALPHA = 20.250 X/D = 6.500 TEST NO. = 35

THETA 176.25 168.75 161.25 153.75 146.25 138.75 131.25 123.75 116.25 108.75 101.25 93.75

R/D

.5985	1.537	1.601	-63.178	-29.420	156.408	270.024	238.828	159.220	44.190	4.699	10.065	17.092
.6590	-.024	13.137	-14.341	9.938	110.020	104.759	27.426	-9.063	-5.331	-7.461	-5.851	-2.634
.7250	12.571	57.609	42.921	16.131	11.230	9.347	7.601	9.140	6.065	6.772	6.009	4.036
.7945	17.905	96.830	80.488	14.080	-7.655	-2.359	-.409	.411	-7.326	-5.434	-3.686	-4.373
.8640	29.593	112.350	91.223	23.209	-.445	1.118	.459	5.693	7.845	3.157	1.374	1.635
.9220	34.653	102.712	62.113	-7.862	-22.328	-9.371	-1.665	-5.607	-5.342	-3.299	-4.530	-6.741
.9695	37.584	107.855	72.118	18.780	7.609	5.129	2.099	.728	4.580	3.744	2.752	4.293
1.0130	-10.285	25.047	8.925	-17.015	-15.861	-6.288	.469	-19.444	-16.075	4.743	-2.142	-10.283
1.0940	10.648	52.287	19.093	-3.259	-1.510	-.834	-1.725	-2.483	-3.960	-1.475	-1.712	-1.646
1.2220	10.526	32.935	18.498	2.564	3.263	1.324	2.521	1.233	-1.040	1.107	1.503	1.152
1.3575	-1.161	2.028	6.054	-.851	-1.579	-.821	.810	-.250	-.561	.623	.607	1.009
1.4850	2.471	1.650	.887	.874	2.613	1.399	.601	5.700	4.466	-1.247	-1.466	-1.067
1.6090	1.361	-.425	.155	-.624	-1.669	-.062	-.872	-2.832	.278	.163	.242	-.505
1.7390	.862	-1.063	-1.507	-1.100	.024	1.600	1.137	-.153	-1.384	-.737	-.384	-.603
1.8605	.938	.319	.187	-.181	-.809	.044	-.389	1.016	1.134	1.506	.981	1.395

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = 1.961 RE = 9.80x10 FT ALPHA = 20.250 X/D = 3.500 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.3550	.016	.205	.566	.588	.222	.032	.591	.772	.248	.114	.154	.062	3.5716
.4165	.087	.236	.380	.556	.375	.198	.153	-.021	-.093	-.035	-.015	-.043	1.7771
.4665	.021	.540	1.117	1.196	.650	.214	.045	.005	.007	-.021	-.003	-.001	3.7712
.5295	.025	.642	.916	.564	.196	.011	-.024	-.030	-.021	.001	.028	.046	2.3548
.6245	-.016	.360	.700	.488	.163	.061	.031	.019	.019	-.033	-.012	-.003	1.7786
.7545	.025	.050	.065	.001	-.022	-.024	-.035	-.029	-.013	-.027	-.021	-.023	-.0531
.8820	.020	.038	.035	.011	.007	.004	-.012	-.020	-.050	-.018	-.007	-.018	-.0101
.9835	-.003	-.019	.010	.042	.044	.055	.065	.092	.100	.066	.006	-.008	.4505
1.0940	.017	.011	-.010	-.011	-.006	.001	-.005	-.032	-.046	-.028	-.037	-.058	-.2044
1.2220	.010	.021	.021	.020	.009	.017	.021	.019	.032	.031	.021	.037	.2592
1.3575	-.010	.032	.027	.038	.040	.052	.049	.040	.053	.047	.036	.022	.4248
R SUM	.192	2.115	3.827	3.492	1.677	.622	.881	.816	.237	.097	.150	.013	14.1202

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = 1.962 RE = 9.79X10 FT ALPHA = 20.250 X/D = 4.100 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.4165	.022	.199	.359	.565	.228	.259	.205	.253	.201	.062	-.092	-.230	1.8325
.4665	-.106	.455	.794	.761	.597	.398	.165	-.007	-.066	-.145	-.092	.060	2.8141
.5295	-.028	.778	.852	.421	.295	.163	.078	-.018	-.007	.099	.168	.098	2.8995
.6245	.221	1.614	1.410	.542	.272	.099	.101	.060	.041	-.042	-.038	.000	4.2805
.7545	.020	.502	.481	.160	-.014	-.068	-.042	-.006	-.003	-.026	-.025	-.023	.9562
.8820	.012	.044	.039	.025	.000	-.016	-.029	-.024	.006	-.011	-.039	-.038	-.0313
.9835	.026	.039	.029	.027	.058	.095	.074	.055	.080	.090	.037	-.018	.5927
1.0940	.017	-.020	-.027	-.023	-.025	-.019	-.041	-.037	-.050	-.067	-.038	-.055	-.3857
1.2220	.033	.033	.024	.027	.016	.029	.037	.042	.046	.021	.024	.033	.3648
1.3575	-.033	-.033	-.016	-.021	-.016	.007	.017	.014	.013	.055	.027	.025	.0388
RSUM	.182	3.611	3.946	2.284	1.412	.947	.565	.330	.263	.036	-.069	-.147	13.3621

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = 1.956 RE = 9.81X10 FT ALPHA = 20.250 X/D = 4.400 TEST NO. = 35

THETA	176.25	166.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.6245	.535	2.070	1.968	1.256	.793	.767	.312	.030	.013	-.045	-.082	-.074	7.5433
.7545	.300	1.275	1.072	.447	.141	.058	.011	.011	.053	-.180	-.194	-.116	2.6777
.8820	.116	.272	.203	.057	-.052	.007	-.120	-.209	-.096	-.003	.274	.299	.7472
.9835	.066	.049	-.016	-.084	-.102	.024	.092	.242	.196	.082	.038	-.002	.5853
1.0940	.066	.035	.006	.112	.092	.024	-.097	-.065	-.030	-.025	-.060	-.034	.0440
1.2220	.017	-.001	.002	.002	-.002	.000	.002	.019	.010	.001	.028	.025	.1036
1.3575	-.015	-.018	.005	.005	.006	.012	.011	.028	.001	-.017	.034	.023	.0739
RSUM	1.103	3.682	3.240	1.794	.877	.893	.212	.056	.147	-.188	.036	.122	11.9750

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = 1.957 RE = 9.81X10 FT ALPHA = 20.250 X/D = 4.800 TEST NO. = 35

THETA	178.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.6245	.092	.261	.608	.335	-.006	.196	.153	.016	.046	.047	.053	.061	1.8613
.7545	.378	1.396	2.395	1.868	1.024	.766	.249	-.016	.018	.016	.027	.014	8.1364
.8820	.268	.937	1.233	.673	.347	.171	.059	.001	-.027	-.024	-.019	-.010	3.6083
.9835	.028	.167	.213	.145	.070	.062	.093	.105	.098	.091	.068	.089	1.2288
1.0940	.009	-.029	-.019	-.004	-.030	.013	.020	-.027	-.030	-.039	-.045	-.076	-.2575
1.2220	.064	.016	.032	.037	.041	.052	.040	.056	.045	.043	.030	-.248	.2068
1.3575	.012	-.012	.018	.012	.018	.030	.016	-.052	-.183	-.038	.166	.321	.3071
RSUM	.851	2.738	4.481	3.066	1.464	1.288	.630	.082	-.035	.096	.279	.151	15.0911

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = 1.960 RE = 9.78x10 FT ALPHA = 20.250 X/D = 6.500 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.5985	.011	.011	-.435	-.202	1.077	1.859	1.644	1.034	.304	.032	.069	.118	5.5204
.6590	-.000	.075	-.082	.057	.628	.598	.157	-.052	-.030	-.043	-.033	-.015	1.2598
.7250	.122	.557	.415	.175	.109	.090	.073	.088	.059	.065	.058	.039	1.8505
.7945	.140	.756	.629	.110	-.060	-.018	-.003	.003	-.057	-.042	-.029	-.034	1.3943
.8640	.341	1.294	1.051	.267	-.005	.013	.005	.066	.090	.036	.016	.019	3.1935
.9220	.192	.568	.344	-.043	-.124	-.052	-.009	-.031	-.030	-.018	-.025	-.037	.7343
.9695	.358	1.028	.688	.179	.073	.049	.020	.007	.044	.036	.026	.041	2.5480
1.0130	-.049	.118	.042	-.080	-.075	-.030	.002	-.092	-.076	.022	-.010	-.049	-.2752
1.0940	.260	1.278	.466	-.080	-.037	-.020	-.042	-.061	-.097	-.036	-.042	-.040	1.5496
1.2220	.262	.818	.460	.064	.081	.033	.063	.031	-.026	.028	.037	.029	1.8781
1.3575	-.039	.068	.204	-.029	-.053	-.028	.027	-.008	-.019	.021	.020	.034	.1991
1.4850	.063	.043	.023	.023	.069	.037	.016	.150	.117	-.033	-.038	-.028	.4429
1.6090	.052	-.016	.006	-.024	-.064	-.002	-.033	-.108	.011	.006	.009	-.019	-.1824
1.7390	.029	-.036	-.052	-.038	.001	.055	.039	-.005	-.047	-.025	-.013	-.021	-.1132
1.8605	.036	.012	.007	-.007	-.031	.002	-.015	.039	.044	.058	.038	.054	.2381
R SUM	1.779	6.576	3.766	.372	1.588	2.585	1.943	1.061	.286	.108	.084	.090	20.2378

SECTION VIII $M_{\infty} = 1.96, \alpha = 24.8^{\circ}, Re = 9.8 \times 10^6 ft^{-1},$ $X/D = 3.5, 4.1, 4.4, 4.8, 6.5$

LOCAL FLOW FIELD DATA

MACH = 1.982 RE = 9.60x10 FT ALPHA = 24.820 X/D = 3.500 TEST NO. = 35

LOCAL MACH NO. -- (H) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 4 0	2.172	2.182	2.179	2.119	2.028	1.919	1.740	1.470	1.278	1.892	2.244	1.786	1.690
.395 16 0	2.184	2.013	1.804	1.676	1.948	1.960	1.733	2.497	2.356	2.340	2.290	2.268	2.292
.438 4 0	2.786	2.560	1.985	1.677	2.086	2.000	2.229	2.362	2.339	2.336	2.342	2.355	2.271
.495 16 0	2.787	2.188	1.707	1.756	2.285	2.525	2.371	2.290	2.254	2.238	2.203	2.135	2.038
.564 20 0	2.760	2.209	1.745	1.596	2.172	2.615	2.489	2.354	2.283	2.231	2.224	2.181	2.077
.685 56 0	2.108	1.851	1.876	1.934	2.319	2.428	2.249	2.184	2.137	2.144	2.089	2.007	1.935
.824 60 0	1.864	1.848	1.895	1.966	2.062	2.184	2.104	2.083	2.119	2.096	2.031	1.948	1.927
.940 96 0	1.834	1.847	1.895	1.975	2.038	2.104	2.110	2.126	2.169	2.139	2.049	1.977	1.932
1.027 96 0	1.873	1.897	1.922	1.957	1.999	2.063	2.042	2.021	2.082	2.030	1.969	1.912	1.902
1.161 60 1	1.912	1.930	1.938	1.946	1.958	1.980	1.964	1.964	1.981	1.933	1.885	1.866	1.880
1.283 56 0	1.908	1.932	1.940	1.955	1.974	2.007	1.997	2.003	2.017	1.948	1.913	1.905	1.878
1.432 20 0	1.945	1.952	1.939	1.934	1.955	1.978	1.990	2.015	2.015	1.956	1.928	1.907	1.871

LOCAL FLOW FIELD DATA

MACH = 1.960 RE = 9.79X10 FT ALPHA = 24.620 X/D = 4.100 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 12 0	.861	.635	.641	.879	1.412	1.627	1.677	1.602	.585	1.111	1.482	.849	1.060
.438 8 0	.698	.700	.684	.665	1.385	1.144	.849	.757	1.625	1.828	1.523	1.564	1.645
.495 12 0	2.238	1.712	.929	.874	.932	1.256	1.414	1.400	1.399	1.234	1.321	1.481	1.462
.564 24 0	2.488	2.110	1.526	1.208	.985	1.280	1.622	1.634	1.509	1.607	2.042	2.214	2.080
.685 52 0	2.511	1.998	1.670	1.424	1.343	1.672	1.949	2.047	2.106	2.106	2.065	2.017	1.955
.824 64 0	1.888	1.804	1.938	1.597	1.878	2.265	2.186	2.079	2.039	2.058	2.028	1.955	1.895
.940 92 0	1.854	1.837	1.899	2.008	2.059	2.192	2.221	2.176	2.154	2.155	2.102	2.024	1.934
1.027 92 0	1.880	1.876	1.935	1.980	2.032	2.136	2.125	2.099	2.096	2.051	1.983	1.943	1.926
1.161 64 0	1.842	1.905	1.916	1.942	1.975	2.050	2.077	2.035	2.040	2.002	1.946	1.906	1.901
1.263 52 0	1.888	1.910	1.932	1.953	1.979	2.038	2.038	2.032	2.051	1.997	1.943	1.906	1.903
1.432 24 0	1.890	1.919	1.923	1.926	1.965	1.999	2.001	2.021	2.059	1.991	1.939	1.919	1.898

LOCAL FLOW FIELD DATA

MACH = 1.963 RE = 9.81X10 FT ALPHA = 24.820 X/D = 4.400 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.964 28 0	1.633	1.379	1.166	1.117	1.519	1.418	.852	1.538	1.958	1.726	1.655	1.691	1.692
.685 48 0	1.401	1.419	1.604	1.285	1.147	1.349	1.677	1.808	1.718	1.690	1.660	1.614	1.544
.824 68 0	1.631	1.478	1.741	1.100	.974	1.387	1.602	1.650	1.602	1.550	1.521	1.479	1.418
.940 88 0	1.462	1.647	1.786	1.790	1.530	1.683	1.879	1.851	1.334	1.346	1.594	1.654	1.704
1.027 88 0	1.430	1.667	1.649	1.666	1.742	1.938	1.873	1.677	1.674	1.992	2.018	1.954	1.931
1.161 68 0	1.896	1.552	1.404	1.430	1.460	1.637	1.885	2.050	2.056	2.024	1.957	1.910	1.914
1.283 48 0	1.857	1.915	1.904	1.922	1.981	2.053	2.069	2.062	2.065	2.022	1.952	1.911	1.916
1.432 28 0	1.883	1.910	1.922	1.933	1.970	1.997	2.019	2.040	2.059	2.002	1.952	1.928	1.903

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.61×10 FT ALPHA = 24.620 X/D = 4.800 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.364 32 0	2.287	2.289	2.301	1.929	1.779	1.760	2.171	2.567	2.652	2.648	2.444	2.324	2.276
.685 44 0	2.097	2.126	2.127	1.970	1.776	1.973	2.460	2.681	2.679	2.648	2.592	2.520	2.416
.824 72 0	2.478	2.102	1.737	1.775	1.902	2.287	2.486	2.404	2.327	2.256	2.178	2.079	1.964
.940 84 0	2.037	1.793	1.723	1.492	1.724	2.271	2.340	2.207	2.107	2.030	1.940	1.859	1.834
1.027 84 1	1.691	1.909	1.988	2.045	2.003	1.945	1.912	1.859	1.804	1.750	1.708	1.646	1.577
1.161 72 0	1.657	1.724	1.800	2.014	1.925	1.869	1.967	1.920	1.874	1.837	1.757	1.666	1.592
1.283 44 0	1.666	1.697	1.776	1.902	1.840	1.816	1.884	1.853	1.796	1.784	1.707	1.618	1.549
1.432 32 0	1.665	1.665	1.689	1.771	1.735	1.742	1.810	1.777	1.709	1.720	1.552	1.279	1.886

LOCAL FLOW FIELD DATA

MACH = 1.964 RE = 9.78X10⁴ FT ALPHA = 24.820 X/D = 6.500 TEST NO. = 35

LOCAL MACH NO. -- (M) --

THETA	160.00	172.50	185.00	197.50	210.00	222.50	235.00	247.50	260.00	272.50	285.00	297.50	310.00
R/D RUN NO.													
.564 36 0	1.853	1.877	1.887	1.875	1.956	1.833	1.693	1.476	.761	2.278	2.722	2.212	2.352
.633 100 0	1.783	1.774	1.810	1.920	1.880	1.404	1.213	2.029	2.454	2.336	2.597	2.632	2.414
.685 40 0	1.982	1.809	1.732	1.917	1.536	1.079	1.993	2.473	2.398	2.553	2.559	2.466	2.338
.765 104 0	2.029	1.700	1.544	1.837	1.824	2.001	2.352	2.417	2.425	2.515	2.446	2.318	2.174
.824 76 0	2.196	1.647	1.524	2.022	2.256	2.308	2.337	2.363	2.468	2.435	2.327	2.209	2.077
.904 108 0	2.222	1.589	1.517	2.080	2.314	2.354	2.258	2.289	2.395	2.375	2.273	2.139	2.030
.940 80 0	2.190	1.554	1.539	2.095	2.274	2.306	2.273	2.335	2.456	2.407	2.346	2.344	2.279
.999 112 0	1.882	1.431	1.547	2.076	2.355	2.384	2.217	2.268	2.364	2.303	2.178	2.086	2.009
1.027 80 1	1.837	1.283	1.729	2.214	2.191	2.180	2.128	2.119	2.172	2.095	2.010	1.938	1.960
1.161 76 0	2.030	1.317	1.739	2.241	2.303	2.272	2.246	2.281	2.237	2.111	2.024	1.982	1.921
1.283 40 0	2.009	1.445	1.743	2.206	2.253	2.214	2.214	2.191	2.168	2.098	2.021	1.950	1.896
1.432 36 0	1.885	1.860	1.963	2.147	2.180	2.136	2.104	2.200	2.121	2.064	2.001	1.930	1.890
1.538 100 0	1.865	2.004	2.057	2.114	2.118	2.123	2.124	2.185	2.102	2.042	1.980	1.927	1.878
1.680 104 0	1.915	1.999	2.048	2.059	2.087	2.094	2.077	2.144	2.076	2.019	1.953	1.888	1.868
1.798 108 0	1.988	2.024	2.041	2.035	2.034	2.064	2.050	2.086	2.043	1.983	1.935	1.904	1.975
1.923 112 0	2.086	2.061	2.065	2.041	2.017	2.065	2.071	2.037	2.008	1.989	1.992	1.954	1.881

LOCAL FLOW FIELD DATA

MACH = 1.962 RE = 9.60x10 FT ALPHA = 24.820 X/D = 3.500 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315	4 0 9.156	9.454	13.030	16.330	17.140	14.368	8.868	4.474	34.161	45.547	35.805	37.485	36.701
.395	16 0 14.136	16.049	14.386	8.235	15.635	16.790	24.623	34.091	34.903	34.131	33.706	34.413	32.103
.436	4 0 26.899	26.319	19.359	1.954	17.677	29.424	34.755	34.805	34.416	33.444	33.840	33.319	31.420
.495	16 0 23.840	20.355	3.218	24.932	36.281	36.887	34.828	34.016	33.383	33.087	32.406	30.910	29.207
.564	20 0 22.754	19.509	5.456	30.240	38.199	36.905	34.244	33.578	33.019	32.463	32.348	30.884	28.784
.685	56 0 11.475	8.404	21.867	36.779	38.536	36.036	34.584	33.878	33.386	32.838	31.951	30.201	28.340
.824	60 0 7.918	14.194	21.675	25.300	31.415	33.992	32.283	32.018	32.306	31.434	30.238	28.667	28.277
.940	96 0 15.094	17.391	21.204	23.839	26.217	28.742	29.311	29.506	29.663	29.065	28.236	27.189	25.808
1.027	96 0 17.272	18.180	20.563	22.953	25.006	27.698	28.444	28.931	30.741	29.988	28.917	27.355	25.859
1.161	60 1 21.670	21.676	22.583	24.243	25.904	27.458	28.560	29.274	30.095	29.367	28.309	26.559	25.004
1.283	56 0 20.628	20.559	21.485	23.154	24.419	25.776	26.810	27.919	28.909	28.413	27.639	25.994	24.164
1.432	20 0 22.372	22.040	22.963	24.540	25.343	26.320	27.246	28.197	28.523	27.907	27.018	25.799	24.217

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.960 RE = 9.79X10 FT ALPHA = 24.820 X/D = 4.100 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395	12 0 8.153	23.822	34.393	41.912	31.254	25.395	14.591	2.186	43.577	49.706	41.407	50.271	45.252
.438	8 0 9.334	6.177	15.846	39.177	38.507	40.663	36.045	42.800	43.200	40.849	43.186	44.993	43.979
.495	12 0 22.318	17.399	12.690	41.313	54.215	55.449	51.880	48.355	45.380	43.794	40.619	37.431	34.786
.564	24 0 23.987	19.910	7.657	34.890	48.497	48.631	44.762	42.663	39.408	36.356	33.318	31.176	29.290
.685	52 0 21.198	11.220	17.759	40.413	47.999	43.246	38.055	34.413	32.894	32.669	32.288	30.621	28.456
.824	64 0 5.587	13.743	27.073	30.917	35.434	35.871	33.935	32.740	32.029	31.727	30.948	29.346	27.609
.940	92 0 8.012	14.021	21.821	25.108	29.967	32.200	30.834	30.298	29.916	29.375	28.483	27.291	26.078
1.027	92 0 13.106	17.448	21.175	23.787	26.545	29.921	30.018	29.642	30.813	30.509	29.569	27.995	25.833
1.161	64 0 17.645	18.899	21.162	23.489	25.252	27.518	28.745	29.075	30.213	29.836	28.594	26.647	24.952
1.283	52 0 19.492	19.948	21.334	23.332	24.818	26.485	28.033	28.683	29.471	28.970	28.111	26.529	24.839
1.432	24 0 21.543	21.488	22.681	24.415	25.427	26.806	27.850	28.635	29.294	28.532	27.671	26.441	24.635

LOCAL FLOW FIELD DATA

MACH = 1.963 RE = 9.61x10 FT ALPHA = 24.820 X/D = 4.400 TEST NO. = 35

LOCAL ANGLE OF ATTACK -- (ALPHA) -- DEG.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.964 28 0 17.787	14.173	32.927	43.803	36.295	39.423	48.596	42.457	39.716	41.891	43.595	43.225	41.370	
.685 48 0 21.170	3.709	21.764	40.316	46.904	46.657	44.159	41.403	40.888	40.758	40.502	39.830	38.482	
.824 68 0 16.578	7.987	31.771	46.059	51.623	46.091	43.320	41.471	40.947	40.958	40.420	39.151	37.419	
.940 88 0 7.741	20.352	32.019	35.525	41.496	42.777	39.783	38.632	43.383	38.136	32.617	30.400	28.040	
1.027 88 0 16.396	22.922	29.122	32.838	35.516	38.168	38.432	37.724	34.017	31.463	29.897	28.568	26.141	
1.161 68 0 15.006	26.568	34.257	35.978	36.233	34.433	31.922	29.472	30.338	30.091	28.855	27.027	25.143	
1.283 48 0 18.624	19.456	21.612	23.945	25.278	26.982	28.645	29.136	29.808	29.382	28.574	26.916	24.814	
1.432 28 0 20.876	21.268	22.495	24.289	25.426	27.040	28.294	29.096	29.622	28.807	27.813	26.425	24.958	

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.81x10 FT ALPHA = 24.820 X/D = 4.800 TEST NO. = 35

LOCAL ANGLE OF ATTACK		-- (ALPHA) --												
DEG.														
THETA		180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.														
.564	32 0 12.299	14.481	24.142	30.123	18.947	3.010	18.619	26.312	28.857	30.636	31.756	31.234	30.014	
.685	44 0 16.971	15.929	21.006	20.337	19.566	22.082	21.193	23.956	26.265	27.612	28.192	27.808	26.815	
.824	72 0 19.465	12.973	13.379	20.607	30.149	31.954	29.903	29.571	30.186	30.631	30.692	30.207	29.245	
.940	84 0 11.300	1.517	18.077	26.855	37.108	36.908	33.552	32.707	32.569	32.572	32.210	31.154	30.481	
1.027	84 1 9.596	17.584	27.046	30.758	35.166	39.382	37.552	36.502	36.224	35.845	35.074	33.710	31.688	
1.161	72 0 15.332	19.762	24.357	28.509	30.874	33.937	35.859	34.669	34.579	34.450	33.533	32.109	30.374	
1.283	44 0 19.377	23.455	25.742	28.837	31.181	33.511	35.967	35.071	34.902	34.888	33.767	32.077	30.304	
1.432	32 0 25.716	26.427	28.438	29.896	32.097	33.681	34.775	35.268	35.334	35.364	34.467	32.064	28.246	

LOCAL FLOW FIELD DATA

MACH = 1.964 RE = 9.76X10 FT ALPHA = 24.820 X/D = 6.900 TEST NO. = 35

LOCAL ANGLE OF ATTACK		-- (ALPHA) --												DEG.	
THETA		180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00	
R/D	RUN NO.														
.564	36 0	5.448	6.897	10.342	15.173	19.418	20.175	17.010	13.177	26.071	39.738	37.996	39.030	37.369	
.633	100 0	6.354	8.866	10.508	13.520	18.414	15.812	32.579	39.578	37.875	39.178	38.025	36.505	35.202	
.685	40 0	12.600	11.974	8.478	9.158	13.046	24.699	40.698	38.122	36.808	37.047	36.563	34.966	33.262	
.765	104 0	15.449	11.822	5.717	13.961	30.869	43.081	41.106	37.993	37.637	37.006	35.802	34.333	32.774	
.824	76 0	19.182	11.931	12.113	22.720	30.623	34.651	36.480	36.611	36.391	36.197	34.824	33.214	31.603	
.904	108 0	17.458	7.977	20.745	29.630	31.913	33.455	35.155	36.481	36.262	34.993	33.563	32.240	30.812	
.940	80 0	17.172	7.081	21.064	29.297	31.190	32.159	32.543	34.223	34.560	33.617	33.218	33.322	32.876	
.999	112 0	11.460	.614	26.344	32.225	32.352	32.383	31.844	34.232	34.930	33.598	32.535	31.184	29.737	
1.027	80 1	8.265	11.546	30.719	31.865	32.919	32.436	32.972	35.215	34.830	33.926	32.965	31.406	28.941	
1.161	76 0	9.427	10.465	30.766	29.457	30.188	31.154	31.318	33.181	32.886	32.450	31.585	29.955	27.758	
1.283	40 0	3.613	10.767	29.820	29.070	29.197	29.116	31.004	32.026	31.989	31.389	30.564	29.171	27.559	
1.432	36 0	6.796	15.069	26.629	26.920	28.796	29.102	30.156	31.296	30.817	30.392	29.511	28.285	26.656	
1.538	100 0	9.572	16.481	23.324	24.567	26.210	27.581	28.120	30.700	30.199	29.959	29.424	28.256	26.027	
1.680	104 0	11.864	17.488	21.409	23.597	25.710	27.341	28.000	30.026	29.674	29.330	28.948	27.936	25.731	
1.798	108 0	12.580	17.864	21.334	23.383	25.372	27.356	28.197	29.251	29.384	28.990	28.333	26.740	24.566	
1.923	112 0	13.526	17.343	20.312	22.563	24.732	26.659	27.476	28.351	28.710	28.029	27.122	25.947	25.102	

LOCAL FLOW FIELD DATA

MACH = 1.962 RE = 9.80x10 FT ALPHA = 24.820 X/D = 3.500 TEST NO. = 35

CROSSFLOW DIRECTION (THETA) MODEL RADIAL L.

	THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D	RUN NO.													
.315	4 0	180.0	-136.2	-101.2	-68.5	-38.7	-33.7	-64.5	12.5	72.3	80.2	69.2	68.0	73.0
.395	16 0	180.0	-147.3	-131.0	-40.3	14.5	23.9	45.8	61.8	62.2	67.4	74.0	82.2	84.5
.438	4 0	180.0	-175.6	-159.9	113.9	41.4	47.5	48.6	50.4	57.6	63.9	72.0	77.7	81.1
.495	16 0	-180.0	-166.5	110.1	43.2	46.8	44.2	44.1	51.7	58.6	66.4	71.9	75.3	79.1
.564	20 0	-180.0	-166.4	60.1	43.8	47.3	47.0	47.3	53.6	60.6	66.7	72.7	77.3	81.6
.685	56 0	180.0	125.0	52.2	48.0	49.1	49.6	50.5	55.9	62.6	68.6	73.0	77.1	82.1
.824	60 0	.0	36.0	39.0	42.1	49.3	51.0	51.3	57.1	64.2	68.4	72.0	77.1	78.4
.940	96 0	.0	22.4	31.5	37.1	44.0	48.6	50.8	56.4	63.2	67.7	72.0	76.7	81.7
1.027	96 0	.0	15.7	26.0	37.5	44.2	49.8	52.8	58.7	66.2	69.7	73.7	77.9	82.9
1.161	60 1	.0	14.9	23.1	32.0	39.6	46.4	51.0	57.4	64.1	68.1	72.5	77.2	82.1
1.283	56 0	.0	11.7	21.5	31.7	39.2	46.3	51.9	58.1	64.9	69.1	73.2	77.7	83.4
1.432	20 0	.0	17.2	22.8	31.8	39.3	46.6	53.1	60.3	65.3	69.2	72.8	77.2	83.0

LOCAL FLOW FIELD DATA

*8 -1

MACH = 1.960 RE = 9.79X10 FT ALPHA = 24.620 X/D = 4.100 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 12 0 180.0	-71.6	-22.1	-2.5	-3.3	-14.2	-17.8	18.4	32.0	75.1	54.8	63.6	69.2	
.438 8 0 -180.0	140.8	-14.1	2.4	11.6	8.3	30.0	51.0	62.9	49.8	47.4	58.3	62.9	
.495 12 0 180.0	177.7	65.1	33.8	43.2	50.2	47.9	40.7	40.0	41.1	53.0	63.7	68.1	
.564 24 0 180.0	-168.6	71.1	41.7	49.6	45.9	39.4	36.9	40.9	53.8	69.4	76.9	80.4	
.695 52 0 180.0	-175.0	35.5	38.6	43.3	42.7	44.3	51.3	60.1	67.0	72.2	76.5	81.2	
.824 64 0 -180.0	74.9	47.0	43.8	47.9	48.8	50.6	55.0	60.9	67.1	71.7	76.3	82.1	
.940 92 0 .0	32.1	36.5	38.3	46.2	49.1	50.1	54.9	60.8	66.5	71.3	75.5	80.9	
1.027 92 0 .0	25.3	33.5	39.5	45.6	51.1	53.0	57.0	63.5	69.2	73.2	77.5	82.9	
1.161 64 0 .0	15.8	26.0	35.2	42.0	48.4	52.2	57.4	64.1	68.6	72.7	77.4	83.0	
1.283 52 0 .0	13.3	23.2	33.0	40.6	47.8	52.6	57.8	65.0	69.0	73.2	78.0	83.3	
1.432 24 0 .0	12.5	20.8	30.2	38.3	45.6	50.7	56.5	64.0	68.1	72.1	76.6	82.7	

LOCAL FLOW FIELD DATA

MACH = 1.963 RE = 9.61x10⁶ ALPHA = 24.620 X/D = 4.400 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 28 0	-180.0	-102.3	-38.5	-18.7	-6.0	-4.0	25.2	42.5	45.4	52.6	58.5	61.6	62.6
.685 48 0	-180.0	-163.6	12.6	20.4	29.4	44.8	41.9	38.8	44.2	50.4	54.7	58.1	60.1
.824 68 0	-180.0	49.9	38.8	39.2	38.8	38.9	38.8	40.6	44.2	48.5	53.9	58.1	60.4
.940 88 0	.0	50.5	40.2	31.4	35.9	39.4	40.3	41.0	44.2	51.0	60.1	66.9	74.7
1.027 88 0	.0	28.9	31.9	32.3	37.3	43.7	43.5	44.7	55.5	67.5	73.1	77.3	82.7
1.161 68 0	.0	21.3	22.6	27.7	32.2	38.7	47.6	56.3	62.9	68.2	72.5	77.1	82.5
1.283 48 0	.0	14.0	24.2	33.5	41.1	48.2	53.0	57.6	64.4	69.3	73.5	78.4	83.9
1.432 28 0	.0	10.9	20.3	29.7	37.6	44.4	49.9	55.4	62.6	67.1	71.2	76.0	81.9

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.81×10^4 FT $\alpha = -1$ ALPHA = 24.820 X/D = 4.800 TEST NO. = 35

CROSSFLOW DIRECTION (THETA) MODEL RADIAL L.

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 32 0	-180.0	-125.7	-98.5	-66.4	-76.5	156.0	76.1	76.0	77.3	78.1	80.5	82.5	84.4
.685 44 0	180.0	-138.3	-98.5	-75.7	-16.4	22.8	52.1	65.8	71.9	76.5	79.6	82.0	84.3
.824 72 0	180.0	-133.7	-52.6	3.0	23.7	34.9	44.4	52.2	58.4	63.0	66.5	69.3	71.6
.940 84 0	-180.0	110.7	37.8	36.6	40.2	39.1	41.6	47.7	52.5	57.2	60.8	63.5	64.6
1.027 84 1	.0	45.1	44.2	42.7	40.4	41.3	44.1	48.1	52.4	56.2	59.8	63.0	66.1
1.161 72 0	.0	18.5	31.7	38.8	37.8	39.0	43.0	47.1	50.9	54.9	58.4	61.6	64.2
1.283 44 0	.0	15.7	27.3	35.3	35.0	37.6	43.8	46.9	50.3	54.8	58.3	61.3	64.0
1.432 32 0	.0	12.0	21.8	30.0	31.8	36.3	42.6	44.9	48.0	53.9	55.5	59.2	79.3

LOCAL FLOW FIELD DATA

MACH = 1.964 RE = 9.78x10 FT ALPHA = 24.820 X/D = 6.500 TEST NO. = 35

CROSSFLOW DIRECTION (THETA VC) MODEL RADIAL L.

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 36 0	180.0	-129.0	-103.7	-94.8	-92.9	-84.0	-70.2	-72.2	67.0	81.3	78.6	81.0	86.7
.633 100 0	-180.0	-138.3	-98.8	-95.6	-89.2	-44.5	49.9	61.1	64.5	73.4	79.9	82.3	83.8
.685 40 0	180.0	-143.1	-99.7	-103.0	-73.9	47.0	60.1	59.1	65.1	74.6	79.1	81.0	83.2
.763 104 0	-180.0	-160.7	9.0	53.1	70.2	62.0	55.2	58.3	68.2	73.8	76.0	78.4	81.1
.824 76 0	180.0	-164.3	27.0	44.5	56.9	59.2	56.8	59.9	68.6	73.0	75.2	77.9	81.3
.904 108 0	-180.0	-157.0	28.9	40.2	51.0	55.8	58.0	63.2	68.2	70.9	73.4	76.2	79.6
.940 80 0	180.0	-155.4	25.1	36.3	49.0	55.5	58.0	63.3	68.2	71.0	71.8	71.5	72.9
.999 112 0	180.0	-9.1	27.1	36.3	48.5	54.6	56.4	64.1	68.4	70.3	72.9	75.9	79.8
1.027 80 1	-180.0	23.8	27.1	38.5	48.5	53.2	57.8	65.6	69.1	71.6	74.8	78.1	81.4
1.161 76 0	-180.0	25.7	28.4	40.1	50.7	51.5	56.5	64.1	66.8	69.9	73.2	76.5	80.2
1.283 40 0	-180.0	53.8	34.0	41.4	50.2	51.9	56.4	64.1	66.9	69.9	73.4	77.2	81.1
1.432 36 0	.0	54.0	41.3	43.8	48.1	49.9	54.9	61.9	64.7	67.9	71.4	75.5	79.6
1.538 100 0	.0	47.3	42.2	43.8	47.3	50.1	54.9	61.5	64.8	68.5	72.3	76.3	80.9
1.680 104 0	.0	28.6	36.8	40.6	44.9	49.0	53.8	60.4	63.4	67.2	71.7	76.5	81.2
1.798 108 0	.0	22.7	32.5	37.3	42.4	48.3	54.8	59.3	62.6	67.2	71.6	76.6	83.7
1.923 112 0	.0	20.9	30.2	35.9	41.1	48.6	55.5	59.6	63.8	69.0	74.3	78.3	82.5

LOCAL FLOW FIELD DATA

*6 -1

MACH = 1.962 RE = 9.60x10 FT ALPHA = 24.620 X/D = 3.500 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 4 0	-.158	-.162	-.177	-.178	-.143	-.115	-.125	-.099	.001	-.068	-.147	-.004	.007
.395 16 0	-.190	-.179	-.201	-.210	-.167	-.144	-.084	-.214	-.176	-.170	-.162	-.156	-.137
.438 4 0	-.286	-.274	-.238	-.227	-.220	-.163	-.157	-.170	-.163	-.160	-.164	-.158	-.124
.495 16 0	-.273	-.222	-.207	-.193	-.212	-.213	-.167	-.152	-.145	-.143	-.122	-.087	-.041
.564 20 0	-.254	-.202	-.182	-.167	-.192	-.231	-.188	-.164	-.151	-.137	-.126	-.102	-.060
.685 56 0	-.078	-.072	-.102	-.137	-.193	-.191	-.134	-.119	-.117	-.113	-.081	-.043	-.006
.824 60 0	.039	.027	.000	-.026	-.099	-.131	-.086	-.085	-.104	-.089	-.055	-.012	-.001
.940 96 0	.051	.046	.023	-.017	-.058	-.088	-.082	-.092	-.108	-.092	-.049	-.011	.018
1.027 96 0	.032	.022	.008	-.010	-.032	-.066	-.053	-.047	-.075	-.045	-.010	.022	.033
1.161 60 1	.014	.008	-.000	-.004	-.012	-.025	-.022	-.026	-.032	-.003	.028	.046	.046
1.283 56 0	.019	.009	.003	-.003	-.011	-.029	-.029	-.035	-.040	-.002	.021	.032	.050
1.432 20 0	.007	.007	.011	.012	-.000	-.011	-.019	-.037	-.032	-.000	.016	.036	.057

LOCAL FLOW FIELD DATA

MACH = 1.960 RE = 9.79X10 FT ALPHA = 24.820 X/D = 4.100 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 12 0	.417	.418	.345	.349	.151	.042	-.178	-.380	.133	.633	.349	1.077	.877
.438 8 0	.354	.301	.221	.239	.163	.271	.143	.114	.132	.089	.289	.260	.218
.495 12 0	-.220	-.144	.028	.250	.460	.325	.267	.315	.340	.420	.274	.175	.225
.564 24 0	-.239	-.208	-.138	-.013	.315	.270	.126	.156	.180	.078	-.072	-.112	-.057
.685 52 0	-.212	-.151	-.137	-.010	.082	.017	-.051	-.078	-.099	-.100	-.078	-.050	-.015
.824 64 0	.002	-.020	-.062	.017	-.088	-.158	-.117	-.087	-.077	-.079	-.058	-.019	.016
.940 92 0	.046	.040	.004	-.034	-.095	-.134	-.120	-.105	-.100	-.095	-.068	-.031	.006
1.027 92 0	.032	.030	.002	-.019	-.052	-.102	-.090	-.077	-.079	-.054	-.017	.009	.025
1.161 64 0	.043	.021	.013	-.000	-.020	-.061	-.066	-.047	-.055	-.030	.002	.027	.035
1.283 92 0	.025	.020	.010	-.001	-.015	-.043	-.046	-.043	-.056	-.026	.005	.031	.040
1.432 24 0	.025	.013	.015	.012	-.008	-.024	-.026	-.036	-.054	-.020	.009	.025	.045

LOCAL FLOW FIELD DATA

MACH = 1.963 RE = 9.61X10 FT ALPHA = 24.620 X/D = 4.400 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.364 28 0	.020	.059	.001	-.005	-.026	.036	.528	.292	.032	.140	.171	.183	.213
.685 48 0	.201	.036	-.129	.046	.158	.049	.072	.088	.142	.173	.206	.246	.310
.824 68 0	.145	.073	-.079	.457	.634	.291	.157	.162	.203	.257	.296	.346	.421
.940 88 0	.270	.156	.090	.116	.205	.116	.055	.085	.466	.331	.148	.137	.125
1.027 88 0	.262	.174	.193	.199	.135	.014	.071	.154	.086	-.033	-.031	.004	.022
1.161 68 0	.019	.212	.356	.333	.273	.116	.003	-.055	-.060	-.039	-.003	.025	.028
1.283 48 0	.037	.017	.019	.009	-.019	-.054	-.064	-.059	-.064	-.041	-.003	.023	.028
1.432 28 0	.025	.018	.015	.007	-.011	-.025	-.035	-.044	-.057	-.025	.003	.021	.039

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.81x10⁶ FT ALPHA = 24.820 X/D = 4.000 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 32 0	-.232	-.241	-.267	-.232	-.192	-.140	-.187	-.250	-.257	-.254	-.234	-.212	-.184
.665 44 0	-.188	-.206	-.254	-.269	-.204	-.167	-.216	-.246	-.244	-.238	-.226	-.208	-.179
.824 72 0	-.205	-.183	-.221	-.227	-.199	-.178	-.193	-.173	-.151	-.128	-.100	-.057	-.000
.940 84 0	-.044	-.067	-.155	-.115	-.093	-.155	-.144	-.101	-.063	-.028	.019	.068	.087
1.027 84 1	.134	.016	-.050	-.056	-.034	-.031	.008	.044	.082	.122	.158	.208	.268
1.161 72 0	.170	.118	.063	-.024	.016	.028	.004	.033	.064	.092	.147	.214	.276
1.283 44 0	.182	.149	.103	.040	.087	.099	.048	.076	.112	.129	.187	.257	.318
1.432 32 0	.197	.192	.173	.126	.157	.152	.103	.130	.183	.180	.280	.383	.333

LOCAL FLOW FIELD DATA

*6 -1

MACH = 1.964 RE = 9.78X10 FT ALPHA = 24.820 X/D = 6.500 TEST NO. = 35

LOCAL PRESSURE COEFFICIENT ** (CP) **

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.964 36 0	-.118	-.126	-.147	-.181	-.219	-.206	-.171	-.167	-.240	.070	-.203	-.201	-.180
.633 100 0	-.118	-.122	-.133	-.169	-.210	-.192	-.117	-.140	-.221	-.215	-.235	-.226	-.181
.685 40 0	-.143	-.132	-.138	-.168	-.169	-.168	-.136	-.229	-.219	-.239	-.228	-.200	-.164
.765 104 0	-.162	-.121	-.093	-.104	-.145	-.176	-.200	-.209	-.221	-.226	-.199	-.163	-.114
.824 76 0	-.197	-.112	-.080	-.106	-.165	-.194	-.199	-.203	-.220	-.205	-.172	-.134	-.084
.904 108 0	-.174	-.067	-.054	-.126	-.180	-.186	-.173	-.194	-.204	-.187	-.152	-.103	-.052
.940 80 0	-.149	-.042	-.056	-.131	-.171	-.171	-.172	-.198	-.210	-.188	-.171	-.174	-.154
.999 112 0	-.014	.022	-.037	-.126	-.191	-.188	-.151	-.176	-.189	-.163	-.119	-.079	-.036
1.027 80 1	.030	-.119	-.067	-.165	-.184	-.145	-.129	-.148	-.144	-.109	-.068	-.026	-.018
1.161 76 0	-.043	-.083	-.043	-.157	-.178	-.160	-.149	-.170	-.143	-.097	-.056	-.028	.008
1.283 40 0	-.029	-.029	-.045	-.148	-.155	-.133	-.137	-.139	-.120	-.087	-.052	-.011	.028
1.432 36 0	.019	-.022	-.073	-.116	-.130	-.104	-.102	-.129	-.096	-.067	-.034	.009	.039
1.558 100 0	-.003	-.046	-.082	-.096	-.101	-.091	-.093	-.119	-.082	-.053	-.020	.014	.047
1.660 104 0	-.027	-.049	-.070	-.077	-.081	-.081	-.074	-.104	-.071	-.044	-.008	.032	.051
1.798 108 0	-.062	-.059	-.062	-.060	-.057	-.070	-.071	-.079	-.055	-.026	.001	.020	-.001
1.923 112 0	-.093	-.072	-.068	-.057	-.044	-.065	-.074	-.059	-.043	-.029	-.022	.006	.050

LOCAL FLOW FIELD DATA

MACH = 1.962 RE = 9.80x10⁶ FT ALPHA = 24.820 X/D = 3.500 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA		180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D	RUN NO.													
.315	4 0	.796	.795	.733	.668	.681	.645	.472	.350	.366	.731	.936	.757	.676
.395	16 0	.692	.560	.360	.280	.484	.609	.545	.982	.970	.983	.951	.944	1.065
.438	4 0	.825	.662	.371	.250	.493	.540	.878	1.019	1.010	1.016	1.008	1.059	1.083
.495	16 0	.965	.577	.301	.352	.715	1.029	1.048	.992	.970	.956	.987	1.015	1.012
.564	20 0	1.102	.672	.366	.316	.669	1.043	1.121	1.030	.980	.957	.992	1.016	.998
.685	56 0	1.003	.686	.642	.613	.850	1.021	1.014	.972	.910	.932	.957	.955	.951
.824	60 0	.954	.903	.907	.943	.865	.922	.965	.935	.922	.940	.953	.949	.947
.940	96 0	.944	.950	.967	.986	.963	.966	.993	.983	.991	1.006	1.002	1.003	1.011
1.027	96 0	.955	.965	.968	.978	.977	.973	.983	.970	.975	.992	.995	.989	1.007
1.161	60 1	.962	.971	.962	.969	.967	.963	.949	.939	.945	.952	.957	.974	.993
1.283	56 0	.976	.985	.983	.990	1.000	.997	.985	.973	.983	.982	.989	1.004	1.003
1.432	20 0	.990	.999	.990	.988	.989	.995	.987	.978	.993	.993	.998	1.008	1.007

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.960 RE = 9.79x10 FT ALPHA = 24.820 X/D = 4.100 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 12 0	.469	.378	.346	.436	.619	.671	.338	-.012	.233	.798	.946	.851	.931
.436 8 0	.367	.340	.295	.300	.609	.528	.300	.259	.611	1.008	.917	.931	.961
.495 12 0	.631	.420	.255	.375	.534	.666	.758	.600	.830	.737	.676	.718	.761
.564 24 0	.809	.558	.325	.322	.467	.633	.802	.865	.752	.707	.913	1.033	1.016
.685 52 0	1.004	.627	.404	.434	.487	.674	.847	.901	.920	.914	.927	.944	.948
.824 64 0	.902	.749	.813	.606	.679	.933	.984	.930	.904	.923	.942	.945	.948
.940 92 0	.951	.912	.916	.975	.866	.916	1.011	.995	.978	1.001	1.011	1.006	1.003
1.027 92 0	.956	.944	.961	.973	.955	.947	.973	.982	.972	.980	.984	.992	1.007
1.161 64 0	.936	.972	.971	.977	.975	.969	.993	.988	.974	.988	.991	.992	1.003
1.283 52 0	.951	.972	.980	.982	.987	.996	.988	.989	.977	.980	.985	.995	1.007
1.432 24 0	.952	.969	.979	.980	.988	.996	.993	.993	.996	.995	.991	1.001	1.015

LOCAL FLOW FIELD DATA

MACH = 1.963 RE = 9.81x10 FT ALPHA = 24.620 X/D = 4.400 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 28 0	.637	.485	.314	.292	.478	.485	.527	.940	1.077	.957	.911	.981	1.036
.665 48 0	.670	.490	.383	.416	.440	.459	.777	.982	.954	.970	.984	.983	.977
.824 68 0	.843	.580	.565	.648	.676	.759	.827	.895	.896	.910	.925	.936	.949
.940 88 0	.814	.883	.951	1.009	.811	.860	1.013	1.038	.888	.757	.800	.858	.903
1.027 88 0	.769	.939	.944	.978	.974	1.004	1.043	.918	.795	.957	1.006	1.001	1.011
1.161 68 0	.954	.847	.853	.857	.818	.803	.901	.985	.974	.992	.991	.988	1.006
1.283 48 0	.936	.979	.966	.968	.983	.990	.987	.993	.978	.984	.982	.990	1.008
1.432 28 0	.939	.963	.973	.972	.979	.983	.989	.991	.988	.992	.991	1.002	1.007

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.61x10 FT ALPHA = 24.820 X/D = 4.800 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 32 0	.630	.588	.477	.358	.366	.459	.691	.844	.906	.920	.786	.752	.815
.685 44 0	.607	.574	.411	.282	.341	.563	.915	1.030	1.044	1.042	1.039	1.052	1.054
.824 72 0	1.015	.639	.291	.296	.427	.874	1.100	1.074	1.062	1.048	1.036	1.024	1.008
.940 84 0	.997	.636	.406	.342	.524	.953	1.109	1.073	1.046	1.036	1.023	1.016	1.020
1.027 84 1	.901	.967	.908	.975	.976	.902	.954	.961	.966	.967	.972	.969	.967
1.161 72 0	.921	.919	.919	1.024	.992	.936	1.025	1.027	1.030	1.035	1.024	1.008	.997
1.283 44 0	.950	.933	.958	1.009	1.022	1.011	1.004	1.020	1.012	1.028	1.018	1.002	.989
1.432 32 0	.967	.963	.965	.999	1.007	1.008	1.012	1.017	1.014	1.026	.944	.742	.975

LOCAL FLOW FIELD DATA

MACH = 1.964 RE = 9.78X10 FT ALPHA = 24.820 X/D = 6.500 TEST NO. = 35

LOCAL TOTAL PRESSURE RATIO (PT/PTINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 36 0	.573	.577	.538	.451	.411	.369	.359	.265	.071	1.943	1.473	.673	.947
.633 100 0	.516	.501	.507	.509	.380	.209	.229	.685	.865	.749	.971	1.086	1.025
.685 40 0	.637	.514	.448	.515	.288	.156	.667	.862	.816	.912	.993	1.019	1.007
.765 104 0	.635	.454	.402	.601	.500	.570	.868	.908	.850	.947	1.002	.993	.976
.824 76 0	.684	.433	.407	.792	.884	.829	.840	.854	.907	.946	.959	.947	.930
.904 108 0	.805	.467	.439	.800	.905	.937	.861	.807	.897	.960	.969	.959	.960
.940 80 0	.863	.480	.450	.803	.886	.930	.880	.843	.950	1.001	.987	.974	.974
.999 112 0	.855	.480	.483	.795	.908	.966	.893	.857	.926	.959	.954	.957	.972
1.027 80 1	.897	.250	.574	.824	.800	.862	.851	.775	.855	.875	.890	.904	.955
1.161 76 0	.991	.300	.631	.900	.892	.931	.938	.901	.951	.939	.942	.957	.967
1.283 40 0	.995	.426	.631	.889	.924	.959	.940	.902	.940	.951	.955	.959	.975
1.432 36 0	.938	.799	.804	.917	.916	.946	.907	.954	.957	.962	.965	.971	.987
1.538 100 0	.850	.922	.897	.928	.923	.963	.963	.959	.967	.970	.974	.981	.987
1.680 104 0	.871	.930	.939	.933	.959	.975	.971	.969	.975	.973	.974	.973	.992
1.798 108 0	.873	.932	.949	.946	.957	.962	.938	.965	.973	.968	.966	.967	1.027
1.923 112 0	.909	.940	.963	.961	.966	.975	.956	.952	.957	.967	.990	1.006	1.008

Case 10-11111-1111

*6 -1

MACH = 1.962 RE = 9.60x10 FT ALPHA = 24.820 X/D = 3.500 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 4 0	-.168	-.123	-.047	.107	.234	.204	.062	.063	.127	.119	.223	.216	.160
.395 16 0	-.239	-.236	-.155	.099	.260	.263	.267	.300	.293	.237	.166	.083	.056
.438 4 0	-.535	-.505	-.313	-.013	.235	.335	.403	.401	.332	.266	.189	.128	.087
.495 16 0	-.479	-.359	-.018	.288	.439	.488	.452	.376	.309	.235	.177	.137	.095
.564 20 0	-.457	-.346	.044	.321	.441	.472	.430	.361	.290	.227	.170	.120	.073
.685 56 0	-.207	-.081	.222	.398	.446	.426	.389	.332	.265	.208	.160	.114	.065
.824 60 0	.134	.192	.282	.318	.349	.374	.347	.298	.243	.199	.158	.106	.094
.940 96 0	.251	.267	.303	.324	.325	.331	.323	.286	.236	.194	.150	.106	.062
1.027 96 0	.290	.295	.307	.310	.307	.309	.295	.256	.214	.177	.136	.095	.053
1.161 60 1	.364	.354	.351	.347	.337	.320	.301	.264	.221	.181	.139	.096	.057
1.283 56 0	.347	.341	.339	.334	.322	.305	.281	.251	.209	.169	.132	.092	.046
1.432 20 0	.379	.357	.357	.350	.331	.306	.277	.238	.202	.166	.133	.095	.049

LOCAL FLOW FIELD DATA

MACH = 1.960 RE = 9.79X10 FT ALPHA = 24.620 X/D = 4.100 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 12 0	-.078	.053	.219	.370	.418	.372	.215	.031	.225	.131	.319	.186	.163
.438 8 0	-.073	-.038	.117	.274	.482	.441	.274	.209	.273	.404	.396	.323	.285
.495 12 0	-.408	-.275	.053	.304	.345	.391	.428	.456	.439	.382	.302	.226	.177
.564 24 0	-.459	-.348	.037	.309	.297	.392	.485	.485	.407	.310	.197	.125	.084
.685 52 0	-.410	-.195	.224	.413	.423	.457	.440	.362	.282	.219	.168	.121	.073
.824 64 0	-.096	.059	.309	.327	.378	.417	.376	.321	.264	.211	.165	.116	.063
.940 92 0	.135	.197	.293	.337	.355	.370	.351	.307	.255	.206	.158	.116	.069
1.027 92 0	.221	.264	.299	.313	.318	.328	.315	.280	.237	.185	.143	.101	.053
1.161 64 0	.293	.307	.320	.324	.319	.315	.305	.268	.225	.184	.142	.096	.051
1.283 52 0	.326	.327	.332	.331	.320	.306	.292	.261	.213	.175	.136	.091	.048
1.432 24 0	.359	.353	.356	.354	.338	.319	.300	.269	.221	.180	.142	.102	.052

LOCAL FLOW FIELD DATA

MACH = 1.000 RE = 9.81X10⁶ ALPHA = 24.820 X/D = 4.400 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 28 0	-.274	-.041	.298	.445	.500	.514	.365	.421	.449	.376	.324	.298	.278
.685 48 0	-.292	-.050	.320	.457	.442	.405	.472	.492	.434	.381	.339	.301	.268
.824 68 0	-.256	.074	.385	.369	.371	.448	.473	.453	.415	.375	.326	.279	.244
.940 88 0	.112	.199	.383	.470	.459	.478	.476	.456	.381	.304	.237	.179	.114
1.027 88 0	.230	.310	.372	.415	.430	.444	.439	.396	.288	.202	.147	.105	.055
1.161 68 0	.254	.361	.420	.425	.415	.396	.349	.280	.236	.189	.145	.100	.055
1.283 48 0	.310	.319	.331	.335	.324	.310	.297	.268	.221	.176	.136	.089	.044
1.432 28 0	.348	.350	.354	.354	.341	.328	.310	.282	.234	.190	.150	.106	.058

LOCAL FLOW FIELD DATA

MACH = 1.959 $RE = 9.61 \times 10^6$ FT $\alpha = 24.820$ $X/D = 4.800$ TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 32 0	-.231	-.158	-.066	.199	.071	-.045	.081	.123	.123	.122	.098	.074	.053
.685 44 0	-.303	-.213	-.055	.086	.302	.348	.249	.194	.160	.125	.098	.074	.050
.824 72 0	-.376	-.161	.131	.331	.453	.471	.402	.336	.288	.250	.215	.184	.153
.940 84 0	-.201	-.009	.227	.306	.426	.504	.454	.388	.341	.298	.258	.224	.209
1.027 84 1	.153	.210	.329	.385	.444	.475	.432	.386	.344	.305	.266	.227	.187
1.161 72 0	.239	.297	.334	.378	.402	.422	.429	.383	.349	.313	.272	.229	.194
1.283 44 0	.301	.351	.364	.387	.409	.418	.415	.380	.347	.312	.269	.227	.191
1.432 32 0	.392	.394	.404	.406	.420	.417	.401	.386	.356	.316	.277	.205	.087

LOCAL FLOW FIELD DATA

MACH = 1.964 RE = 9.78x10 FT ALPHA = 24.820 X/D = 6.500 TEST NO. = 35

RADIAL VELOCITY RATIO -- (VR / VIN) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 36 0	-.092	-.074	-.042	-.021	-.017	.034	.091	.059	.083	.100	.143	.105	.039
.633 100 0	-.137	-.108	-.027	-.022	.004	.156	.250	.311	.297	.197	.124	.092	.069
.685 40 0	-.220	-.158	-.023	-.035	.054	.186	.326	.357	.280	.182	.128	.100	.071
.765 104 0	-.272	-.177	.085	.140	.166	.325	.413	.361	.253	.190	.158	.124	.089
.824 76 0	-.330	-.176	.159	.281	.300	.317	.357	.330	.243	.193	.160	.122	.082
.904 108 0	-.322	-.112	.263	.391	.363	.341	.330	.291	.244	.207	.171	.133	.095
.940 80 0	-.314	-.096	.279	.410	.368	.328	.309	.277	.237	.200	.188	.191	.173
.999 112 0	-.195	.009	.340	.444	.390	.344	.312	.265	.232	.203	.167	.130	.089
1.027 80 1	-.139	.138	.421	.441	.383	.341	.304	.249	.216	.183	.145	.107	.072
1.161 76 0	-.168	.126	.419	.405	.347	.348	.309	.259	.230	.192	.154	.117	.079
1.283 40 0	-.064	.091	.385	.389	.337	.321	.304	.246	.220	.186	.148	.108	.070
1.432 36 0	.116	.148	.337	.343	.341	.328	.300	.261	.229	.196	.159	.118	.079
1.538 100 0	.161	.194	.301	.312	.312	.310	.283	.258	.223	.187	.150	.111	.068
1.680 104 0	.200	.267	.300	.313	.318	.313	.286	.260	.229	.193	.152	.107	.065
1.798 108 0	.220	.288	.314	.323	.323	.315	.279	.259	.231	.189	.149	.103	.046
1.923 112 0	.242	.286	.309	.318	.320	.306	.269	.246	.215	.170	.124	.088	.054

LOCAL FLOW FIELD DATA

MACH = 1.962 RE = 9.60x10 FT ALPHA = 24.820 X/D = 3.500 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 4 0	.000	-.120	-.234	-.273	-.188	-.136	-.130	.014	.400	.686	.588	.534	.522
.395 16 0	.000	-.152	-.178	-.084	.067	.117	.275	.560	.556	.568	.579	.605	.575
.438 4 0	.000	-.039	-.115	.028	.208	.366	.457	.485	.523	.542	.580	.590	.556
.495 16 0	-.000	-.086	.048	.271	.467	.476	.439	.477	.506	.537	.543	.521	.490
.564 20 0	-.000	-.084	.076	.308	.478	.507	.466	.489	.514	.528	.546	.530	.491
.685 56 0	.000	.116	.286	.443	.514	.500	.472	.490	.513	.531	.524	.497	.467
.824 60 0	-.000	.139	.228	.287	.407	.461	.434	.460	.502	.503	.489	.466	.460
.940 96 0	-.000	.110	.185	.245	.314	.376	.396	.429	.467	.472	.462	.447	.428
1.027 96 0	-.000	.083	.163	.238	.298	.366	.389	.421	.485	.479	.466	.443	.426
1.161 60 1	.000	.094	.150	.217	.278	.336	.372	.413	.454	.452	.442	.424	.409
1.283 56 0	-.000	.071	.133	.207	.263	.319	.359	.403	.445	.444	.439	.422	.397
1.432 20 0	.000	.110	.150	.217	.270	.324	.369	.416	.440	.437	.430	.418	.397

LOCAL FLOW FIELD DATA

MACH = 1.960 RE = 9.79x10 FT ALPHA = 24.820 X/D = 4.100 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 12 0	.000	-.159	-.089	-.016	-.024	-.094	-.069	.010	.140	.493	.452	.374	.430
.438 8 0	-.000	.031	-.029	.011	.099	.064	.158	.258	.532	.478	.430	.523	.556
.495 12 0	.000	.011	.115	.204	.324	.469	.473	.393	.368	.334	.401	.457	.439
.564 24 0	.000	-.070	.107	.275	.349	.405	.399	.365	.353	.424	.525	.538	.498
.685 52 0	.000	-.017	.160	.329	.399	.421	.429	.451	.489	.517	.523	.503	.470
.824 64 0	-.000	.218	.332	.313	.419	.477	.458	.458	.474	.498	.498	.476	.451
.940 92 0	-.000	.124	.217	.267	.370	.428	.420	.436	.458	.473	.469	.452	.433
1.027 92 0	.000	.125	.197	.258	.325	.406	.417	.430	.475	.486	.475	.456	.428
1.161 64 0	-.000	.087	.157	.229	.287	.355	.393	.418	.463	.469	.456	.431	.412
1.283 52 0	.000	.077	.142	.215	.275	.337	.381	.414	.457	.457	.449	.430	.410
1.432 24 0	.000	.079	.135	.206	.267	.326	.366	.407	.452	.447	.439	.428	.406

LOCAL FLOW FIELD DATA

MACH = 1.963 RE = 9.81×10^6 FT ALPHA = 24.620 X/D = 4.400 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (V_{THETA}/V_{INF})

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 28 0	-.000	-.189	-.237	-.151	-.053	-.036	.172	.386	.456	.491	.530	.550	.536
.685 48 0	-.000	-.015	.072	.170	.249	.401	.423	.396	.422	.460	.480	.483	.465
.824 68 0	-.000	.088	.309	.301	.298	.361	.380	.388	.404	.425	.447	.449	.430
.940 88 0	-.000	.241	.324	.287	.332	.393	.404	.397	.371	.375	.411	.420	.417
1.027 88 0	-.000	.171	.231	.263	.328	.425	.417	.392	.419	.487	.485	.466	.433
1.161 68 0	.000	.140	.175	.223	.261	.317	.382	.420	.462	.474	.460	.437	.416
1.283 48 0	-.000	.079	.149	.222	.282	.347	.395	.423	.462	.468	.458	.438	.412
1.432 28 0	-.000	.068	.131	.202	.263	.321	.368	.409	.451	.449	.440	.428	.410

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.61X10⁶ FT ALPHA = 24.820 X/D = 4.800 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.364 32 0	-.000	-.220	-.441	-.454	-.297	.020	.327	.492	.546	.578	.580	.562	.538
.695 44 0	.000	-.190	-.371	-.338	-.089	.146	.320	.432	.490	.522	.533	.524	.500
.824 72 0	.000	-.168	-.171	.017	.199	.328	.394	.434	.469	.490	.496	.486	.465
.940 84 0	-.000	.025	.176	.227	.359	.409	.402	.426	.444	.462	.463	.449	.441
1.027 84 1	.000	.211	.320	.355	.378	.418	.418	.430	.446	.456	.458	.445	.420
1.161 72 0	.000	.100	.206	.304	.311	.342	.401	.412	.430	.446	.441	.424	.401
1.283 44 0	.000	.099	.187	.274	.286	.322	.397	.406	.418	.443	.435	.414	.391
1.432 32 0	.000	.084	.162	.235	.260	.306	.368	.384	.396	.432	.403	.343	.459

C5

LOCAL FLOW FIELD DATA

*6 -1

MACH = 1.964 RE = 9.78x10 FT ALPHA = 24.820 X/D = 6.500 TEST NO. = 35

CIRCUMFERENTIAL VELOCITY RATIO - (VTHETA/VINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.584 36 0	.000	-.091	-.171	-.254	-.332	-.330	-.252	-.182	.196	.654	.708	.664	.665
.633 100 0	-.000	-.096	-.172	-.230	-.309	-.154	.296	.565	.622	.663	.696	.680	.637
.685 40 0	.000	-.119	-.135	-.153	-.186	.200	.566	.598	.603	.663	.669	.636	.597
.765 104 0	-.000	-.062	.013	.186	.461	.612	.595	.584	.633	.656	.636	.604	.566
.824 76 0	.000	-.050	.081	.276	.460	.533	.545	.569	.621	.631	.604	.571	.535
.904 108 0	-.000	-.047	.145	.330	.449	.503	.527	.577	.610	.599	.573	.543	.514
.940 80 0	.000	-.044	.131	.301	.423	.478	.494	.551	.591	.582	.572	.572	.562
.999 112 0	.000	-.001	.174	.326	.441	.483	.470	.547	.587	.567	.544	.520	.495
1.027 80 1	-.000	.061	.216	.351	.432	.455	.481	.548	.564	.550	.533	.507	.479
1.161 76 0	-.000	.061	.227	.340	.424	.438	.466	.534	.536	.525	.511	.489	.454
1.283 40 0	-.000	.124	.260	.343	.404	.409	.458	.507	.515	.508	.496	.474	.449
1.432 36 0	.000	.203	.296	.329	.380	.390	.427	.488	.484	.482	.472	.454	.432
1.536 100 0	.000	.211	.273	.300	.338	.370	.402	.475	.472	.475	.470	.455	.422
1.680 104 0	-.000	.146	.224	.268	.317	.360	.392	.457	.457	.460	.459	.446	.418
1.798 108 0	-.000	.121	.200	.246	.295	.354	.397	.435	.446	.450	.447	.430	.416
1.923 112 0	-.000	.109	.180	.230	.280	.346	.392	.419	.437	.443	.443	.428	.411

LOCAL FLOW FIELD DATA

MACH = 1.962 RE = 9.80x10 FT ALPHA = 24.820 X/D = 3.500 TEST NO. = 35

(VC / VINF * SIN ALPHAINF)

THETA	160.00	172.50	185.00	197.50	210.00	222.50	235.00	247.50	260.00	272.50	285.00	297.50	310.00
R/D RUN NO.													
.315 4 0	.401	.414	.568	.698	.716	.583	.343	.154	1.001	1.659	1.498	1.374	1.302
.395 16 0	.617	.669	.563	.310	.639	.686	.913	1.514	1.499	1.466	1.436	1.456	1.375
.438 4 0	1.274	1.206	.794	.074	.748	1.181	1.453	1.498	1.475	1.437	1.454	1.438	1.342
.495 16 0	1.141	.878	.123	.942	1.527	1.624	1.501	1.447	1.413	1.396	1.361	1.284	1.189
.564 20 0	1.088	.648	.210	1.060	1.549	1.651	1.511	1.448	1.406	1.369	1.362	1.294	1.183
.685 56 0	.494	.337	.864	1.418	1.620	1.566	1.457	1.409	1.376	1.357	1.306	1.215	1.124
.824 60 0	.319	.564	.863	1.021	1.277	1.413	1.324	1.306	1.329	1.289	1.224	1.139	1.118
.940 96 0	.598	.689	.847	.969	1.078	1.193	1.216	1.228	1.247	1.216	1.156	1.095	1.030
1.027 96 0	.690	.729	.828	.930	1.019	1.141	1.163	1.174	1.261	1.216	1.157	1.080	1.024
1.161 60 1	.867	.872	.908	.974	1.040	1.105	1.141	1.167	1.202	1.159	1.105	1.036	.983
1.283 56 0	.827	.830	.868	.936	.990	1.051	1.087	1.130	1.172	1.131	1.091	1.029	.952
1.432 20 0	.902	.891	.923	.981	1.018	1.061	1.099	1.142	1.154	1.113	1.072	1.020	.952

LOCAL FLOW FIELD DATA

MACH = 1.980 RE = 9.79X10 FT ALPHA = 24.820 X/D = 4.100 TEST NO. = 35

(VC / VINF * SIN ALPHAINF)

THETA	160.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 12 0	.185	.400	.563	.682	.998	.915	.538	.078	.631	1.215	1.318	.995	1.095
.438 8 0	.174	.116	.288	.652	1.172	1.063	.754	.790	1.425	1.492	1.393	1.464	1.488
.495 12 0	.973	.657	.302	.871	1.128	1.455	1.520	1.433	1.366	1.210	1.197	1.215	1.128
.564 24 0	1.093	.846	.269	.984	1.093	1.343	1.496	1.446	1.284	1.250	1.336	1.317	1.203
.685 92 0	.977	.467	.656	1.257	1.385	1.480	1.464	1.378	1.345	1.337	1.309	1.232	1.132
.824 64 0	.228	.537	1.080	1.080	1.344	1.510	1.412	1.333	1.293	1.288	1.250	1.167	1.084
.940 92 0	.321	.555	.869	1.024	1.221	1.348	1.304	1.270	1.249	1.229	1.179	1.111	1.045
1.027 92 0	.527	.696	.853	.965	1.084	1.244	1.244	1.223	1.265	1.239	1.182	1.112	1.027
1.161 64 0	.697	.760	.850	.946	1.022	1.130	1.184	1.183	1.227	1.201	1.137	1.053	.988
1.283 92 0	.777	.801	.859	.941	1.005	1.085	1.144	1.166	1.202	1.165	1.117	1.047	.983
1.432 24 0	.856	.862	.908	.975	1.025	1.087	1.127	1.161	1.198	1.148	1.099	1.048	.974

LOCAL FLOW FIELD DATA

MACH = 1.963 RE = 9.81×10^6 FT $\alpha = -1$ ALPHA = 24.820 X/D = 4.400 TEST NO. = 33

(VC / VINP * SIN ALPHAINP)

THEYA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 28 0	.652	.461	.906	1.120	1.197	1.228	.961	1.361	1.524	1.473	1.481	1.491	1.439
.685 48 0	.695	.125	.782	1.162	1.207	1.358	1.510	1.505	1.442	1.423	1.400	1.356	1.278
.824 68 0	.610	.274	1.176	1.136	1.134	1.372	1.446	1.422	1.380	1.350	1.318	1.259	1.177
.940 88 0	.266	.744	1.196	1.313	1.351	1.475	1.488	1.440	1.266	1.149	1.131	1.088	1.030
1.027 88 0	.549	.642	1.044	1.171	1.289	1.463	1.443	1.327	1.210	1.255	1.207	1.137	1.040
1.161 68 0	.606	.923	1.083	1.145	1.168	1.207	1.232	1.203	1.236	1.217	1.150	1.067	.999
1.283 48 0	.738	.784	.863	.957	1.024	1.110	1.178	1.194	1.220	1.191	1.138	1.064	.988
1.432 28 0	.828	.850	.900	.972	1.025	1.094	1.147	1.183	1.210	1.161	1.108	1.049	.988

LOCAL FLOW FIELD DATA

MACH = 1.959 RE = 9.81×10^6 FT ALPHA = 24.820 X/D = 4.800 TEST NO. = 35

(VC / VINF + SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 32 0	.551	.645	1.062	1.180	.727	.117	.802	1.209	1.334	1.407	1.402	1.349	1.287
.685 44 0	.722	.681	.893	.832	.750	.900	.966	1.127	1.227	1.278	1.292	1.260	1.196
.824 72 0	.898	.554	.514	.790	1.178	1.367	1.341	1.306	1.311	1.309	1.289	1.239	1.166
.940 84 0	.478	.060	.684	.907	1.328	1.547	1.445	1.373	1.335	1.309	1.263	1.196	1.153
1.027 84 1	.364	.710	1.093	1.248	1.389	1.507	1.433	1.376	1.343	1.306	1.262	1.190	1.096
1.161 72 0	.570	.747	.935	1.156	1.211	1.294	1.399	1.340	1.318	1.299	1.235	1.149	1.060
1.283 44 0	.716	.869	.975	1.129	1.188	1.257	1.368	1.325	1.295	1.290	1.218	1.125	1.037
1.432 32 0	.935	.960	1.036	1.118	1.177	1.232	1.297	1.298	1.269	1.276	1.164	.952	1.114

LOCAL FLOW FIELD DATA

*6 -1

MACH = 1.964 RE = 9.78x10 FT ALPHA = 24.820 X/D = 6.500 TEST NO. = 35

(VC / VINF * SIN ALPHAINF)

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.864 36 0	.219	.279	.418	.608	.792	.790	.638	.456	.308	1.576	1.720	1.600	1.588
.633 100 0	.327	.346	.414	.550	.735	.522	.923	1.538	1.641	1.647	1.683	1.635	1.525
.685 40 0	.523	.472	.327	.375	.462	.651	1.556	1.660	1.584	1.639	1.622	1.534	1.432
.765 104 0	.648	.448	.204	.555	1.168	1.650	1.724	1.636	1.624	1.628	1.562	1.469	1.365
.824 76 0	.634	.441	.426	.937	1.307	1.477	1.553	1.566	1.589	1.573	1.489	1.392	1.289
.904 108 0	.767	.289	.716	1.219	1.375	1.447	1.480	1.539	1.564	1.510	1.425	1.333	1.245
.940 80 0	.749	.253	.734	1.211	1.335	1.382	1.387	1.468	1.517	1.467	1.434	1.438	1.401
.999 112 0	.463	.021	.911	1.313	1.403	1.413	1.343	1.447	1.504	1.435	1.356	1.276	1.197
1.027 80 1	.331	.360	1.128	1.343	1.375	1.354	1.356	1.434	1.439	1.380	1.316	1.235	1.154
1.161 76 0	.400	.333	1.136	1.259	1.304	1.333	1.331	1.413	1.388	1.332	1.271	1.197	1.098
1.283 40 0	.152	.366	1.106	1.235	1.252	1.238	1.310	1.342	1.334	1.289	1.234	1.158	1.081
1.432 36 0	.276	.599	1.069	1.132	1.215	1.214	1.243	1.317	1.275	1.240	1.186	1.117	1.046
1.538 100 0	.363	.683	.968	1.031	1.096	1.191	1.172	1.289	1.244	1.216	1.176	1.116	1.019
1.680 104 0	.476	.725	.692	.981	1.071	1.137	1.156	1.254	1.219	1.188	1.152	1.093	1.007
1.798 108 0	.523	.744	.687	.966	1.043	1.128	1.155	1.206	1.197	1.163	1.123	1.054	.996
1.923 112 0	.576	.730	.851	.935	1.013	1.100	1.134	1.156	1.161	1.129	1.096	1.041	.988

LOCAL FLOW FIELD DATA

MACH = 1.962 RE = 9.80x10⁶ FT ALPHA = 24.820 X/D = 3.500 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.315 4 0	1.043	1.045	1.031	1.001	.974	.956	.922	.828	.619	.683	.872	.752	.733
.395 16 0	1.028	.976	.921	.899	.959	.934	.836	.939	.902	.908	.903	.892	.920
.438 4 0	1.054	1.024	.948	.907	.985	.879	.879	.905	.904	.914	.910	.919	.922
.495 16 0	1.084	.994	.915	.851	.873	.908	.906	.900	.900	.900	.900	.900	.893
.564 20 0	1.089	1.005	.921	.763	.827	.923	.932	.916	.908	.903	.903	.908	.904
.685 56 0	1.022	.957	.903	.796	.854	.903	.887	.881	.876	.883	.879	.876	.875
.824 60 0	.962	.937	.912	.907	.878	.880	.879	.877	.882	.885	.881	.874	.872
.940 96 0	.930	.923	.916	.920	.919	.913	.909	.911	.919	.918	.904	.895	.894
1.027 96 0	.931	.934	.927	.922	.917	.912	.901	.892	.890	.885	.879	.877	.887
1.161 60 1	.916	.921	.917	.908	.899	.893	.880	.874	.871	.865	.861	.870	.885
1.283 56 0	.922	.929	.925	.919	.915	.913	.903	.895	.891	.878	.875	.886	.891
1.432 20 0	.920	.924	.914	.902	.902	.900	.896	.894	.892	.883	.882	.886	.888

LOCAL FLOW FIELD DATA

+6 -1

MACH = 1.960 RE = 9.79X10 FT ALPHA = 24.820 X/D = 4.100 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.395 12 0	.541	.380	.345	.412	.691	.809	.867	.854	.278	.432	.627	.347	.456
.438 8 0	.446	.450	.426	.336	.618	.519	.435	.358	.637	.725	.623	.615	.647
.495 12 0	.995	.680	.563	.416	.341	.421	.501	.535	.566	.530	.586	.666	.682
.564 24 0	1.032	.981	.839	.592	.406	.497	.633	.659	.656	.713	.853	.913	.900
.685 52 0	1.058	.988	.860	.620	.523	.661	.785	.845	.873	.875	.870	.874	.877
.824 64 0	.977	.922	.887	.757	.793	.877	.881	.870	.868	.875	.875	.871	.870
.940 92 0	.958	.933	.911	.918	.889	.898	.917	.912	.911	.916	.912	.904	.896
1.027 92 0	.950	.930	.925	.919	.911	.907	.904	.902	.891	.883	.875	.878	.890
1.161 64 0	.920	.932	.921	.913	.909	.910	.906	.893	.885	.879	.876	.881	.892
1.263 52 0	.922	.926	.923	.916	.912	.914	.902	.895	.893	.883	.877	.880	.891
1.432 24 0	.910	.919	.912	.901	.905	.903	.895	.893	.896	.887	.880	.885	.892

LOCAL FLOW FIELD DATA

MACH = 1.963 RE = 9.81x10 FT ALPHA = 24.820 X/D = 4.400 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 28 0	.854	.767	.587	.490	.684	.627	.356	.624	.770	.689	.653	.666	.686
.685 48 0	.753	.809	.822	.575	.474	.538	.653	.716	.699	.693	.688	.682	.675
.624 68 0	.860	.819	.797	.459	.377	.554	.644	.675	.667	.653	.650	.649	.646
.940 88 0	.823	.842	.803	.772	.641	.669	.750	.757	.562	.614	.742	.778	.812
1.027 88 0	.783	.836	.786	.761	.758	.781	.763	.720	.753	.861	.882	.877	.890
1.161 68 0	.949	.775	.667	.662	.669	.739	.830	.893	.886	.881	.876	.878	.894
1.283 48 0	.919	.931	.915	.904	.910	.915	.905	.899	.894	.888	.877	.880	.897
1.432 28 0	.911	.917	.912	.904	.905	.899	.895	.892	.893	.886	.882	.886	.891

LOCAL FLOW FIELD DATA

MACH = 1.550 RE = 9.01×10^6 FT ALPHA = 24.820 X/D = 4.800 TEST NO. = 39

AXIAL VELOCITY RATIO -- (V_X / V_{INF}) --

THETA		180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D	RUN NO.													
.964	32 0	1.061	1.048	.994	.854	.889	.936	.999	1.027	1.016	.997	.951	.934	.936
.685	44 0	.993	1.002	.976	.942	.885	.931	1.045	1.065	1.044	1.026	1.011	1.003	.993
.624	72 0	1.064	1.009	.907	.882	.851	.920	.979	.966	.946	.928	.911	.893	.874
.940	84 0	1.004	.946	.860	.752	.737	.865	.914	.897	.877	.860	.842	.831	.830
1.027	84 1	.903	.940	.899	.881	.828	.771	.782	.780	.769	.759	.755	.749	.745
1.161	72 0	.872	.873	.867	.894	.850	.807	.813	.814	.803	.795	.782	.768	.760
1.283	44 0	.855	.841	.849	.860	.824	.797	.791	.792	.779	.776	.765	.753	.745
1.432	32 0	.815	.811	.803	.816	.788	.776	.784	.771	.751	.755	.712	.638	.870

LOCAL FLOW FIELD DATA

MACH = 1.984 RE = 9.78x10 FT ALPHA = 24.820 X/D = 6.500 TEST NO. = 35

AXIAL VELOCITY RATIO -- (Vx / VINF) --

THETA	180.00	172.50	165.00	157.50	150.00	142.50	135.00	127.50	120.00	112.50	105.00	97.50	90.00
R/D RUN NO.													
.564 36 0	.962	.967	.962	.941	.943	.903	.876	.818	.436	.796	.924	.828	.873
.633 100 0	.935	.930	.938	.960	.927	.774	.606	.781	.886	.849	.904	.927	.908
.665 40 0	.983	.934	.920	.976	.838	.594	.759	.888	.889	.911	.918	.921	.917
.765 104 0	.984	.898	.856	.937	.820	.740	.830	.879	.884	.907	.909	.903	.890
.824 76 0	1.007	.877	.833	.939	.927	.897	.882	.885	.905	.902	.899	.892	.880
.904 108 0	1.023	.865	.794	.899	.927	.919	.882	.873	.895	.906	.902	.887	.876
.940 80 0	1.017	.854	.801	.906	.926	.923	.912	.906	.925	.926	.919	.918	.910
.999 112 0	.960	.813	.772	.874	.930	.935	.908	.893	.904	.907	.892	.885	.880
1.027 80 1	.957	.740	.797	.907	.891	.894	.877	.853	.868	.861	.852	.849	.876
1.161 76 0	1.011	.758	.801	.936	.941	.926	.918	.907	.901	.879	.868	.872	.876
1.283 40 0	1.012	.807	.810	.932	.940	.933	.915	.901	.896	.886	.877	.871	.870
1.432 36 0	.971	.933	.895	.936	.928	.915	.898	.910	.897	.887	.880	.872	.874
1.538 100 0	.958	.968	.942	.947	.935	.925	.920	.911	.897	.885	.876	.872	.876
1.680 104 0	.967	.966	.955	.943	.934	.923	.913	.911	.898	.887	.874	.865	.877
1.798 108 0	.984	.969	.953	.938	.923	.915	.905	.904	.892	.881	.874	.878	.915
1.923 112 0	1.005	.981	.965	.944	.923	.920	.915	.900	.889	.890	.898	.898	.885

LOCAL VORTICITY X 100.

+6 -1

MACH = 1.962 RE = 9.80x10 FT ALPHA = 24.820 X/D = 3.500 TEST NO. = 35

THETA 176.25 166.75 161.25 153.75 146.25 138.75 131.25 123.75 116.25 108.75 101.25 93.75

R/D

.3550	7.882	34.870	134.338	136.298	69.578	67.808	170.497	152.116	27.311	32.060	26.233	35.963
.4165	42.116	106.887	173.082	170.457	148.021	160.251	64.847	-17.073	-12.799	-7.116	-1.614	9.525
.4665	18.725	131.850	216.119	204.724	131.853	49.946	2.959	-6.543	-5.104	-7.231	-14.019	-17.767
.5295	40.145	136.766	125.255	75.373	45.089	18.883	3.085	2.133	-.257	3.666	11.070	9.664
.6245	57.177	152.243	116.116	60.582	24.855	7.203	.449	-1.074	2.565	3.339	.672	-.648
.7545	27.546	52.992	17.954	.028	3.009	.409	-4.145	-2.612	.635	.111	-2.033	4.402
.8820	6.674	10.606	3.789	-2.122	-4.800	-5.217	-4.708	-5.214	-2.668	-1.788	-2.129	1.349
.9835	-.587	1.010	3.336	3.366	5.607	5.190	.882	3.899	7.916	5.336	3.323	2.059
1.0940	1.579	3.371	1.092	.921	1.336	1.118	.040	-.981	-1.341	-1.462	-1.270	-.805
1.2220	-2.811	-2.196	.228	.357	.189	.834	.253	.186	1.329	1.722	1.698	.330
1.3575	2.238	6.658	4.694	3.667	3.455	3.811	4.183	3.104	1.840	1.861	1.247	.631

LOCAL VORTICITY X 100.

MACH = 1.960 RE = 9.79x10 FT $\alpha = -1$ ALPHA = 24.820 X/D = 4.100 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.4165	91.362	142.346	93.821	103.748	62.566	38.439	86.227	259.267	143.171	56.535	16.188	94.039
.4665	30.690	128.048	161.111	151.176	152.033	146.946	108.084	24.063	-29.488	-34.094	-26.921	-31.328
.5295	28.551	114.382	113.856	36.473	36.405	18.816	5.671	-7.444	3.105	23.750	32.955	31.849
.6245	54.433	135.752	90.262	24.186	42.343	33.000	16.697	15.447	16.994	4.338	-1.059	-.072
.7545	69.503	127.049	49.592	20.204	30.255	15.071	1.267	-2.609	-1.393	.637	-.254	-1.214
.8820	15.737	21.315	-2.599	6.801	7.387	-3.381	-4.656	-2.868	-2.206	-2.220	-2.190	-2.526
.9835	11.962	14.214	7.515	2.249	2.655	3.939	1.869	4.040	6.625	6.262	5.055	1.828
1.0940	2.632	.073	-.179	.026	-.090	-.156	-.138	.506	.020	.046	-1.435	-2.043
1.2220	1.025	1.293	1.161	1.254	2.011	2.626	1.352	.886	1.340	.952	1.110	1.316
1.3575	.445	2.110	1.645	1.001	1.609	1.648	.923	.102	1.570	1.227	1.128	.706

3

LOCAL VORTICITY X 100.

MACH = 1.963 RE = 9.61x10 FT ALPHA = 24.820 X/D = 4.400 TEST NO. = 35

THETA 176.25 168.75 161.25 153.75 146.25 138.75 131.25 123.75 116.25 108.75 101.25 93.75

R/D

.6245	88.467	154.733	107.086	72.329	76.534	68.210	52.446	9.479	-7.844	-2.925	-1.754	-2.111
.7545	82.165	120.493	55.558	22.930	16.862	17.146	6.623	-1.106	-2.443	-2.535	-1.405	.164
.8820	63.944	78.570	16.571	9.730	27.316	19.424	10.260	-3.847	-10.521	-10.041	-6.016	-3.182
.9835	8.658	6.725	2.815	3.937	16.436	16.162	5.192	-1.589	17.612	26.080	18.655	8.735
1.0940	15.175	6.540	.395	-3.337	-9.200	-9.017	-1.218	3.069	1.838	-1.162	-2.173	-2.586
1.2220	3.946	-.701	1.908	5.441	8.905	7.167	2.330	2.222	1.660	1.990	1.881	1.376
1.3575	.570	.564	.405	-.535	-.139	.025	-.109	-.742	-.355	-.373	-.532	.191

LOCAL VORTICITY X 100.

MACH = 1.959 RE = 9.81X10 FT ALPHA = 24.820 X/D = 4.800 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.6243	23.822	36.379	65.213	35.109	21.665	24.593	6.632	2.296	4.159	3.680	5.953	6.552
.7543	37.612	69.414	86.006	98.703	55.144	11.646	4.482	3.189	2.178	2.909	3.217	2.857
.8820	63.693	114.202	91.988	71.828	45.687	7.694	-2.481	-1.084	-1.345	-1.021	-1.240	1.462
.9833	52.640	86.668	59.061	46.850	24.358	4.907	2.635	3.434	2.911	2.556	3.016	2.159
1.0940	1.493	-2.677	.203	3.866	-.526	-2.789	-1.923	.007	1.146	.848	-.552	-.718
1.2220	9.425	4.874	5.212	3.856	4.151	5.395	.909	1.488	1.839	1.412	.462	.767
1.3575	3.233	.585	.347	1.936	2.331	1.286	-.512	-.713	-.325	-1.413	-9.308	-3.584

LOCAL VORTICITY X 100.

+6 -1

MACH = 1.004 RE = 9.75X10 FT ALPHA = 24.820 X/D = 6.500 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75
R/D												
.5985	4.558	11.377	-.566	1.879	56.873	150.603	244.007	228.666	87.795	22.907	18.245	11.129
.6590	5.621	29.915	19.479	56.164	151.352	192.092	105.480	12.724	-8.811	.824	-.305	-3.342
.7250	27.843	81.788	81.170	172.169	213.299	115.736	19.836	-1.102	4.329	5.153	3.620	2.351
.7945	33.693	88.854	58.829	34.871	20.407	6.196	-5.165	-10.098	-1.270	-.005	-3.363	-4.626
.8640	41.943	90.154	52.059	16.785	7.092	10.807	6.996	1.848	1.408	-.154	-.988	-.696
.9220	44.857	75.048	17.635	-16.208	-11.329	-9.572	-13.230	-8.551	-3.601	4.311	21.214	35.789
.9695	50.229	69.616	43.696	9.429	8.338	3.321	-.447	5.741	4.518	.802	-6.068	-17.585
1.0130	73.475	107.160	48.091	6.033	-13.960	-2.311	8.854	-2.014	-9.856	-6.145	-4.570	-7.325
1.0940	50.534	54.520	6.884	-3.093	4.136	.864	-.283	2.908	1.288	1.147	1.253	.645
1.2220	42.454	59.172	8.767	-2.729	2.354	.880	-1.913	1.528	1.181	1.236	1.069	1.536
1.3575	21.301	47.791	8.242	-.267	1.660	.465	-2.480	.906	-.305	-.423	-.753	-.150
1.4850	6.762	21.332	-.054	-2.826	-1.893	-2.017	-.923	.929	1.386	2.221	2.566	1.131
1.6090	1.614	1.623	-1.471	.425	2.203	.876	1.221	.384	.539	.277	.333	.475
1.7390	5.772	.462	-.366	-.296	.945	1.780	1.623	-.321	-.033	-.243	-1.441	-1.196
1.8605	5.421	1.372	.201	.584	.825	.195	1.190	.326	-.108	.387	.983	.257

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = 1.962 RE = 9.80x10 FT ALPHA = 24.820 X/D = 3.500 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.3550	.037	.165	.636	.655	.329	.321	.807	.720	.129	.152	.124	.170	4.2456
.4165	.126	.319	.517	.509	.442	.478	.194	-.051	-.038	-.021	-.005	.028	2.4971
.4665	.083	.584	.958	.907	.584	.221	.013	-.029	-.023	-.032	-.062	-.079	3.1267
.5295	.244	.833	.763	.459	.275	.115	.019	.013	-.002	.022	.067	.059	2.8673
.6245	.720	1.917	1.462	.763	.313	.091	.006	-.014	.032	.042	.008	-.008	5.3333
.7545	.481	.926	.314	.000	.053	.007	-.072	-.046	.011	.002	-.036	.077	1.7181
.8820	.114	.181	.065	-.036	-.082	-.089	-.080	-.089	-.046	-.030	-.036	.023	-.1062
.9835	-.008	.014	.048	.048	.080	.074	.013	.056	.113	.076	.047	.029	.5895
1.0940	.039	.082	.027	.022	.033	.027	.001	-.024	-.033	-.036	-.031	-.020	.0879
1.2220	-.070	-.055	.006	.014	.005	.021	.006	.005	.033	.043	.042	.008	.0576
1.3575	.075	.224	.158	.124	.116	.128	.141	.105	.062	.063	.042	.021	1.2604
RSUM	1.842	5.192	4.952	3.465	2.148	1.395	1.046	.646	.240	.280	.162	.310	21.6773

LOCAL CIRCULATION STRENGTH X 100.

+6 -1

MACH = 1.960 RE = 9.79x10 FT ALPHA = 24.820 X/D = 4.100 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.4165	.273	.425	.280	.310	.187	.115	.257	.774	.427	.175	.048	.281	3.5512
.4665	.136	.567	.714	.670	.674	.651	.479	.107	-.131	-.151	-.119	-.139	3.4582
.5295	.174	.697	.693	.222	.222	.115	.035	-.045	.019	.145	.201	.194	2.6693
.6245	.686	1.710	1.137	.305	.533	.416	.210	.195	.214	.055	-.013	-.001	5.4447
.7345	1.215	2.221	.867	.353	.529	.263	.022	-.046	-.024	.011	-.004	-.021	5.3855
.8820	.268	.363	-.044	.116	.126	-.058	-.079	-.049	-.038	-.038	-.037	-.043	.4876
.9835	.171	.203	.107	.032	.038	.056	.027	.058	.094	.089	.072	.026	.9728
1.0940	.064	.002	-.004	.001	-.002	-.004	-.003	.012	.000	.001	-.035	-.050	-.0180
1.2220	.025	.032	.029	.031	.050	.065	.034	.022	.033	.024	.028	.033	.4057
1.3575	.015	.071	.055	.034	.054	.062	.031	.003	.053	.041	.038	.024	.4825
RSUM	3.027	6.290	3.834	2.073	2.410	1.682	1.012	1.031	.649	.352	.177	.303	22.8394

LOCAL CIRCULATION STRENGTH X 100.

MACH = 1.963 RE = 9.61x10 FT ALPHA = 24.820 X/D = 4.400 TEST NO. = 35

THETA	176.25	166.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.6245	1.114	1.949	1.349	.911	.989	.859	.661	.119	-.099	-.037	-.022	-.027	7.7661
.7545	1.436	2.106	.971	.401	.295	.300	.151	-.019	-.043	-.044	-.025	.003	5.5313
.8820	1.090	1.340	.283	.166	.466	.331	.175	-.066	-.179	-.171	-.103	-.054	3.2775
.9835	.123	.096	.040	.056	.234	.230	.074	-.023	.251	.372	.266	.125	1.8457
1.0940	.371	.160	.010	-.082	-.225	-.220	-.030	.075	.045	-.028	-.053	-.063	-.0410
1.2220	.098	-.017	.047	.135	.221	.178	.058	.055	.041	.049	.047	.034	.9473
1.3575	.019	.019	.014	-.018	-.005	.001	-.004	-.025	-.012	-.013	-.018	.006	-.0347
RSUM	4.252	5.652	2.713	1.569	1.976	1.679	1.085	.117	.004	.128	.093	.024	19.2923

LOCAL CIRCULATION STRENGTH X 100.

*6 -1

MACH = 1.959 RE = 9.81X10 FT ALPHA = 24.820 X/D = 4.800 TEST NO. = 35

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.6245	.300	.458	.821	.442	.273	.310	.084	.029	.052	.046	.075	.083	2.9729
.7545	.657	1.213	1.503	1.725	.964	.204	.078	.056	.038	.051	.056	.050	6.5959
.8820	1.086	1.947	1.569	1.225	.779	.131	-.042	-.018	-.023	-.017	-.021	.025	6.6398
.9835	.751	1.236	.842	.668	.347	.070	.038	.049	.042	.036	.043	.031	4.1527
1.0940	.036	-.065	.005	.094	-.013	-.068	-.047	.000	.028	.021	-.013	-.018	-.0396
1.2220	.234	.121	.129	.096	.103	.134	.023	.037	.046	.035	.011	.019	.9887
1.3575	.109	.020	.012	.065	.079	.043	-.017	-.024	-.011	-.048	-.314	-.121	-.2069
RSUM	3.174	4.930	4.882	4.316	2.532	.824	.115	.128	.172	.124	-.163	.069	21.1034

LOCAL CIRCULATION STRENGTH X 100.

+8. -1

MACH = 1.964 RE = 9.78X10 FT ALPHA = 24.820 X/D = 6.500 TEST NO. = 33

THETA	176.25	168.75	161.25	153.75	146.25	138.75	131.25	123.75	116.25	108.75	101.25	93.75	TH SUM
R/D													
.5985	.031	.078	-.004	.013	.391	1.037	1.679	1.560	.604	.158	.126	.077	5.7504
.6590	.032	.171	.111	.321	.864	1.097	.602	.073	-.050	.005	-.002	-.019	3.2052
.7250	.269	.791	.785	1.664	2.062	1.119	.192	-.011	.042	.050	.035	.023	7.0199
.7945	.263	.694	.460	.272	.159	.048	-.040	-.079	-.010	-.000	-.026	-.036	1.7057
.8640	.483	1.039	.600	.193	.082	.124	.081	.021	.016	-.002	-.011	-.008	2.6180
.9220	.248	.415	.098	-.090	-.063	-.053	-.073	-.047	-.020	.024	.117	.198	.7544
.9695	.479	.854	.417	.090	.079	.032	-.004	.055	.043	.008	-.058	-.168	1.8265
1.0130	.347	.507	.227	.029	-.066	-.011	.042	-.010	-.047	-.029	-.022	-.035	.9333
1.0940	1.235	1.332	.168	-.076	.101	.021	-.007	.071	.031	.028	.031	.016	2.9515
1.2220	1.055	1.470	.218	-.068	.058	.022	-.048	.038	.029	.031	.027	.038	2.8707
1.3575	.718	1.611	.278	-.009	.056	.016	-.084	.031	-.010	-.014	-.025	-.005	2.5616
1.4850	.177	.560	-.001	-.074	-.050	-.053	-.024	.024	.036	.058	.067	.030	.7507
1.6090	.061	.062	-.056	.016	.084	.033	.046	.015	.013	.011	.013	.018	.3160
1.7390	.197	.016	-.013	-.010	.032	.061	.055	-.011	-.001	-.008	-.049	-.041	.2286
1.8605	.210	.053	.008	.023	.032	.008	.046	.013	-.004	.015	.038	.010	.4509
RSUM	5.807	9.652	3.294	2.295	3.824	3.501	2.464	1.743	.673	.333	.260	.097	33.9433